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DOI

[10.1007/s10854-019-02393-8](https://doi.org/10.1007/s10854-019-02393-8)

Publication date

2019

Document Version

Final published version

Published in

Journal of Materials Science: Materials in Electronics

Citation (APA)

Hoque, M. A., Bradley, R. K., Fan, J., & Fan, X. (2019). Effects of humidity and phosphor on silicone/phosphor composite in white light-emitting diode package. *Journal of Materials Science: Materials in Electronics*, 30(23), 20471–20478. <https://doi.org/10.1007/s10854-019-02393-8>

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Effects of humidity and phosphor on silicone/phosphor composite in white light-emitting diode package

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Received: 25 July 2019 / Accepted: 16 October 2019 / Published online: 4 November 2019
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Abstract

Silicone/phosphor composite, which serve as mechanical protection and light conversion material, is an integral part of white light-emitting diode (LED) package. In this paper, a comprehensive study is conducted to investigate the effect of humidity and phosphor on moisture absorption, hygroscopic swelling, mechanical behavior, as well as thermal properties of silicone/phosphor composite in comparison with the pure silicone. SEM/EDAX and FTIR were performed to identify the phosphor and silicone compositions. Through moisture sorption test, it has been observed that the addition of phosphor significantly lowers the capacity of moisture absorption, but accelerates the diffusivity of moisture absorption. The hygroscopic swelling test showed that the phosphor has little effect on the swelling compared to the pure silicone sample. Both moisture absorption/desorption and hygroscopic swelling/de-swelling are reversible. Strain ramp test revealed that the phosphor enhances the stiffness of the composite. The moisture absorption, however, has negligible impact on mechanical stiffness for both pure and composite samples. Finally, thermal expansion test showed that the coefficient of thermal expansion does not change with the addition of phosphor into pure silicone.

1 Introduction

High power phosphor-converted white light-emitting diodes (pc-WLEDs) have been accepted as an important substitute for traditional lighting sources due to their high luminous efficiency, low power consumption, longer lifetime and their environmental friendliness [1, 2]. In pc-WLEDs system, silicone or silicone-based materials are commonly used as an encapsulant due to good optical properties like high refractive index, good ultraviolet light resistance [3], and high thermal stability [4] and the resistance to discoloration at high temperature [5]. In pc-WLEDs, the silicone encapsulants are

combined with phosphors to form a composite for blue light conversion and chip protection. As shown in Fig. 1, LED packages have evolved from traditional wire-bond-based package to flip-chip package with silicone/phosphor composite used as film to encapsulate LED chip in chip-scale package (CSP) or chip-on-board (COB) package [2].

From the recent study [6–9], it has been observed that most degradation of white LED products is mainly caused by the degradation of encapsulants. Some researchers [10–13] reported that high temperature and high humidity usually contributed to LED's failure. Although silicone encapsulant exhibits better thermal stability than epoxy-based resins, the darkening and carbonization phenomenon were observed under high temperature and high humidity condition [14, 15]. Absorption of moisture from environment causes the change in silicone properties like coefficient of thermal expansion and elasticity modulus [16, 17]. The water trapped inside silicone capsule may cause bubble generation [18], dissolution of the phosphors [19], and light scattering [13]. Fan et al. [20, 21] studied the interaction of silicone and phosphor, and showed that moisture could be the reason behind degradation of silicone/phosphor composite due to pH change. It further causes the degradation of light-conversion efficiency of phosphors and the transmittance of silicone. Due to this reason it suffers a high temperature treatment during operation [22, 23]. Higher temperature at the

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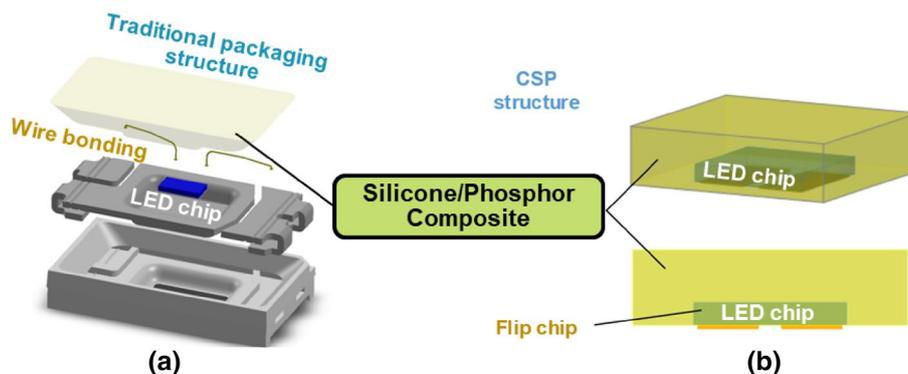
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Fig. 1 The function of silicone/phosphor composite in white LED package **a** traditional packaging structure; **b** chip-scale-package (CSP) or chip-on-board structure [2]



phosphor/binder interface can cause discoloration, decohesion, and cracking of the interface layer [24]. Zhang et al. [25] reported that heat treatment of multicolor phosphor films leads to serious degradation of luminous intensity. According to the study of Wang et al. [26], the introduction of phosphor powder into the silicone matrix shortens the cure rate, while ultraviolet radiation and temperature accelerate the cure of silicone/phosphor composite by increasing the rate of cross-linking. Khalilullah et al. [27] tested the silicone/phosphor composite under high moisture condition and found irreversible swelling despite the reversibility of moisture absorption/desorption. Another study [28] revealed that addition of phosphor with a high temperature aging will stiffen the silicone matrix significantly. Increased Young's modulus of the silicone was observed with aging time which causes severe stress conditions and cracks in the material. Recently, Fan et al. [29] investigated the curing mechanism of phosphor/silicone composites and evaluated their mechanical properties after a high moisture ageing test. Tang et al. studied the reliability of the chip-scale packaged LEDs under overdriving condition [30].

In this paper, a comprehensive study is conducted to investigate the effect of humidity and phosphor on moisture absorption, hygroscopic swelling, mechanical behavior, as well as thermal properties of silicone/phosphor composite in comparison with the pure silicone. Specifically, in situ hygroscopic swelling/de-swelling behavior is restudied for the repeatability and to confirm the non-existence of irreversible swelling observed in the previous study [27]. SEM/EDAX and FTIR were performed to identify the phosphor and silicone compositions. A series of tests, including in situ moisture absorption/desorption, hygroscopic swelling, strain ramp test, as well as thermal expansion measurement, were conducted.

2 Experimental method

2.1 Materials

Silicone and silicone/phosphor composite materials were used in this study. For both samples, a general manufacturing

procedure was provided by a manufacturer company, keeping the chemical composition of the samples unknown. The silicone/phosphor samples were prepared by mixing the phosphor powder with silicone, then a curing process was performed as follows: 1-hour prebake at 100 °C, 2 h curing at 150 °C and then cooling to ambient temperature. The pure silicone sample was prepared similarly but without the addition of phosphor. In this study, the thickness of all test samples is made as ~0.5 mm, which is a typical thickness in actual LED package. The concentration of phosphor in composite is ~9% in mass fraction.

2.2 SEM/EDAX

Identification of the phosphor in the sample was achieved using energy dispersive spectroscopy (EDS). Samples were placed in a Hitachi S-3400 N (SEM) equipped with a backscatter detector and an AMETEK EDAX EDS system. Samples were prepared by securing small pieces cut from the bulk silicone phosphor composite using conductive carbon tape and copper tape to reduce charging of the electrically insulating silicone. To increase the sensitivity of the EDAX analysis the elemental mapping was used to identify subsurface phosphor particles based on threshold X-ray emission at characteristic wavelengths.

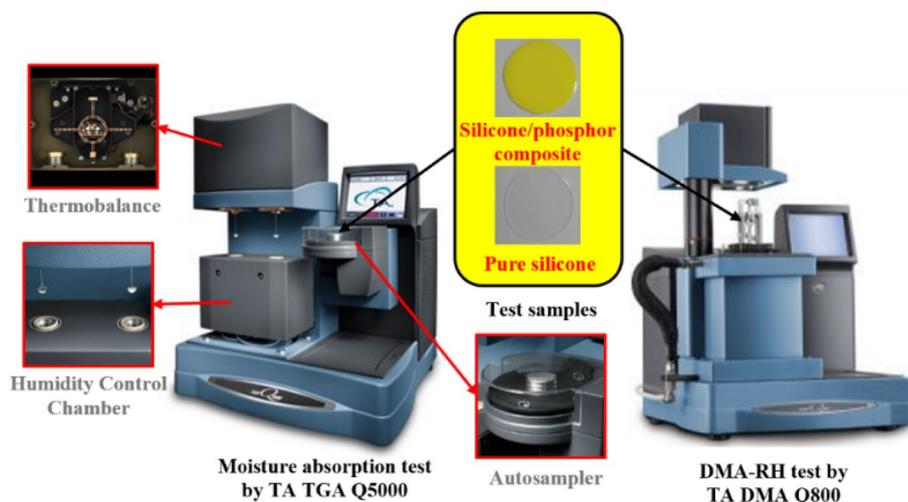
2.3 FTIR

Attenuated total reflectance fourier transform infrared spectroscopy (ATR-FTIR) was used to characterize the silicone composite and pure silicone samples. A perkin elmer spectrum Two FTIR was used. Samples were prepared by cutting small pieces from the bulk. Samples were placed in the ATR accessory and the spectra were captured.

2.4 TGA sorption

As shown in Fig. 2, the moisture absorption test was performed using TA TGA Q5000 instrument equipped with environmental chamber having high accurate temperature and humidity

Fig. 2 The experimental setup of TGA sorption and DMA-RH tests



control (Accuracy: ±1% RH). It measures the amount and rate of change in the weight (Weighing accuracy: ±0.1%) of a material as a function of temperature and time in a controlled environment. The moisture chamber allows in situ weight measurement during moisture diffusion. Dry nitrogen is used to dehumidify the sample chamber and as the moisture carrier to elevate the humidity.

2.5 DMA-RH

Dynamic mechanical analysis (DMA) was performed using at TA DMA Q800 equipped with the humidity control (see Fig. 2). The DMA-RH accessory enables analyzing the hygroscopic swelling behavior by controlling temperature and relative humidity. Dry nitrogen was used to dehumidify the sample chamber. The samples were cut into 10×3 mm size. One of the 3 mm wide ends was held by a fixed clamp and other end was held by movable clamp. Stress–strain curves were measured for pure silicone and silicone/phosphor composite samples with and without the effect of humidity.

2.6 TMA

Thermomechanical analysis (TMA) measures sample displacement as a function of temperature, time and applied force. TMA was used to determine the linear coefficient of thermal expansion (CTE) for pure silicone and silicone/phosphor composite samples were measured from 25 °C to 300 °C.

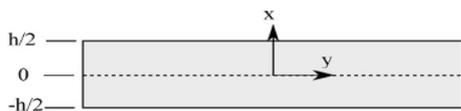


Fig. 3 A schematic representation of an infinite plate

3 Mathematical model for moisture diffusion

In this study 1D-diffusion model was used. In an isotropic medium moisture diffusion can be described by Fick’s diffusion law. The 1-D diffusion equation is expressed by [31, 32] as follows:

$$\frac{\partial C}{\partial t} = D \frac{\partial^2 C}{\partial x^2} \tag{1}$$

Here, C is the concentration of diffusing material in a medium, which changes with position x and time t. D is the diffusivity. Equation 1 can be applied to an infinite plate as shown in Fig. 3 below:

Assume the coordinate of the origin is at the center of the plate, the initial and boundary conditions of moisture absorption can be defined as:

$$C = \begin{cases} C_0, & -\frac{h}{2} \leq x \leq \frac{h}{2}, t = 0 \\ C_s, & x = -\frac{h}{2}, \frac{h}{2}, t \geq 0 \end{cases} \tag{2}$$

Here, C₀ is initial concentration in the material and C_s constant moisture concentration at the surface, and h is thickness of the plate.

The solution of Eqs. 1–2 is given by:

$$\frac{C - C_0}{C_s - C_0} = 1 - \left[\frac{4}{\pi} \sum_{n=0}^{\infty} \frac{(-1)^n}{(2n + 1)} \times \exp \left[-\frac{(2n + 1)^2 \pi^2 D}{h^2} t \right] \times \cos \frac{(2n + 1)\pi}{h} x \right] \tag{3}$$

The total amount of moisture entering the plate at time t can be calculated as:

$$M = M_{\infty} \left[1 - \frac{8}{\pi} \sum_{n=0}^{\infty} \frac{1}{(2n + 1)^2} \exp \left[-\frac{(2n + 1)^2 \pi^2 D}{h^2} t \right] \right] \tag{4}$$

Here, M_{∞} is the final weight gain of the sample. Equation 5 was used to calculate saturated moisture content C_{sat} from the experimental data. If the volume V is known, then one can calculate the saturated moisture content using following equation:

$$C_{\text{sat}} = \frac{M_{\infty}}{V} \quad (5)$$

4 Data regression

Least-square regression method was used to calculate diffusivity D and saturated moisture content C_{sat} . Data regression was done using following equation-

$$\text{SSE} = \min \sum_{i=1}^m (M_{t,i}^{\text{exp}} - M_{t,i}^{\text{cal}})^2 = \min \sum_{i=1}^m e_i^2 \quad (6)$$

Here, $M_{t,i}^{\text{exp}}$ is the i -th number of experimental weight gain value at t time and $M_{t,i}^{\text{cal}}$ is the calculated weight gain value m is the number of total data points in a single experiment. Coefficient of determination (COD) R^2 can be obtained by the following equation-

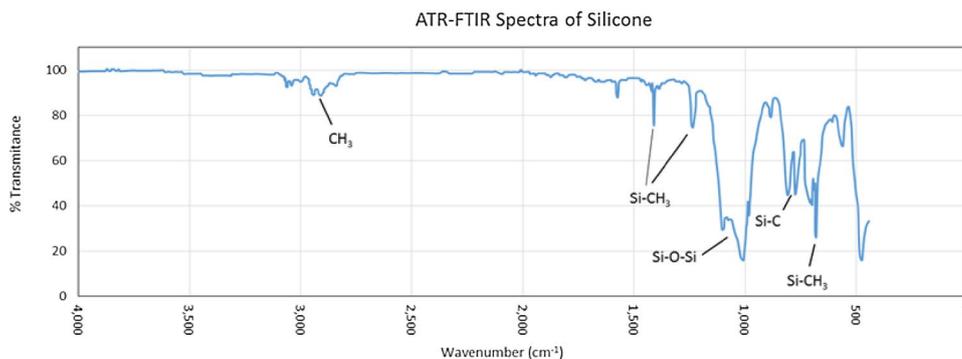
$$R^2 = \frac{1 - \text{SSE}}{\text{SSE}_{\text{Total}}} \quad (7)$$

Here, SS_{Total} is the sum of squared differences between average value and the data points. R^2 is the measure of how much experimental data fits the theoretical model. The values of R^2 ranges between 0 to 1. Value 1 means a perfect association of theoretical model and experimental data, whereas 0 means no association.

5 Results and discussions

ATR-FTIR is used to characterize the functional groups of polymer materials. Figure 4 is a representative ATR-FTIR spectra showing the functional groups of pure silicone

Fig. 4 ATR-FTIR spectra of the pure silicone sample



sample. The spectra for pure silicone and silicone/phosphor composite were found to be identical except minor variations attributed to noise.

From SEM micrograph of silicone/phosphor composite shown in Fig. 5, the particles can be seen embedded in the silicone matrix and extending out of the sample along the cut. Figure 6 shows an elemental map using the signal at the yttrium $L\alpha$ peak as a threshold for locating particles. Yttrium was chosen because of its presence in general EDS analysis of the sample and its colocalization with particles in the SEM image.

Figure 7 shows an EDS spectrum taken from the regions thresholded for yttrium. The spectrum is consistent with the composition of Cerium doped Yttrium Aluminum Garnet (YAG: Ce), a commonly used phosphor in pc-wLEDs that emits the yellow light. The silicon element in the spectra is from the silicone matrix. The carbon is from side functional groups on the silicone as well as residual signal from the carbon tape used to secure the samples.

Figure 8 represents the TGA-sorption analysis results. It can be seen that the addition of phosphor into silicone reduces the significant amount of moisture upon saturation. From Fig. 6, both moisture absorption and desorption are reversible.

Figures 9 and 10 are the mathematical fitting of the moisture absorption and desorption for both pure silicone and

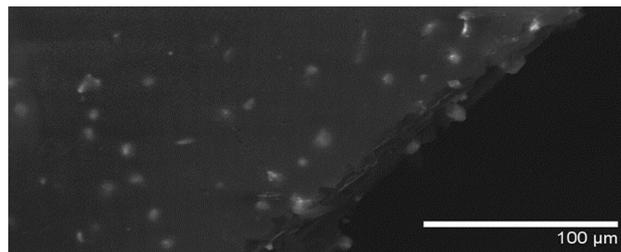


Fig. 5 SEM micrograph of silicone/phosphor composite acquired at 30 kV acceleration voltage and 10 Pa of atmosphere using a back-scatter detector. The sample is on the left and a cut edge can be seen running diagonally across the image

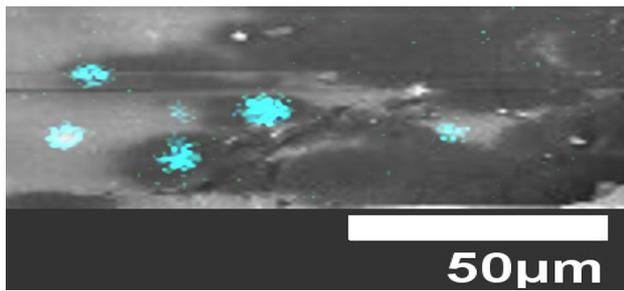


Fig. 6 Elemental map for yttrium (light blue) overlaid on top of an SEM image (grayscale) of the silicone/phosphor composite. The concentrations of yttrium indicate the position of phosphor particles in the silicone

silicone/phosphor composite. It can be seen that both pure silicone and silicone/phosphor composite follows the Fickian diffusion law well. Tables 1 and 2 show the extracted properties from the fit based on the experimental data. We can see that with the addition of phosphor, the diffusivity increases, implying the moisture absorption is accelerated compared to the pure silicone material. The saturated moisture concentration for silicone phosphor is significantly lower than that in pure silicone. For each sample the diffusivity and the saturated moisture concentration are almost same during absorption and desorption phase, which means that the moisture absorption and desorption are reversible.

Figures 11 and 12 describes the hygroscopic swelling and de-swelling during moisture absorption and desorption. The experimental data were taken from a full cycle of moisture absorption and desorption (ramp down–hold–ramp up–hold–ramp down–hold). In these two figures, the dashed line is humidity applied (on the second y-axis on the right). It clearly showed the repeatability and consistency among the seven samples (three pure silicone samples and four silicone/phosphor composite samples). The swelling is reversible for both materials. In the previous study [27], a permanent swelling deformation was observed during the initial

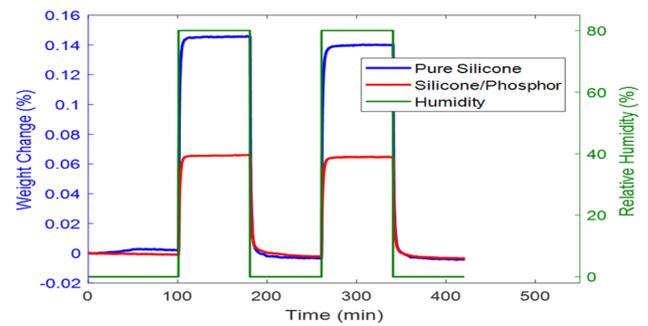


Fig. 8 TGA-sorption analysis of pure silicone and silicone/phosphor samples. Tests were conducted at 60 °C with cycled relative humidity (RH) between 0 and 80% RH

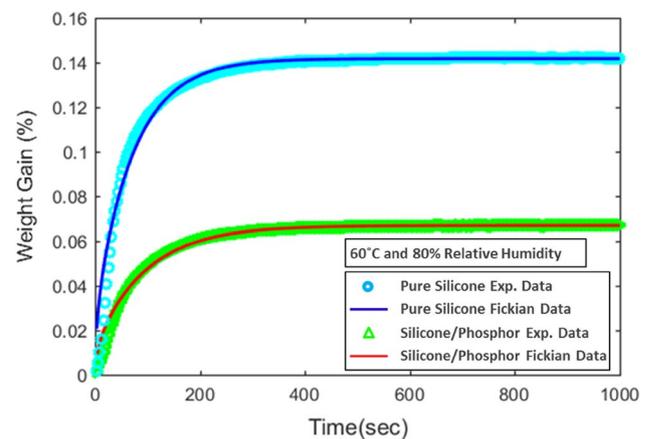
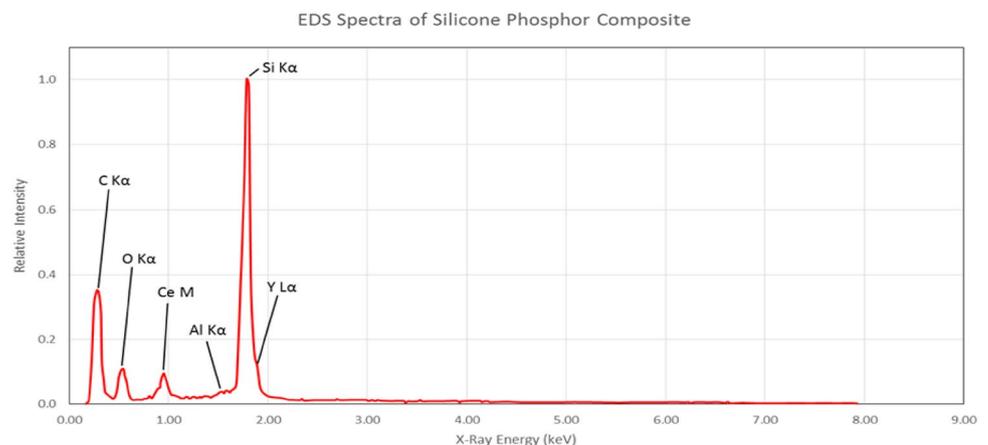


Fig. 9 Fickian diffusion fitting results of pure silicone and silicone/phosphor in moisture absorption. Tests were conducted at 60 °C and 80% RH

humidity ramp up phase. Such a phenomenon occurred in the present testing but it has been attributed to the instrument setup issue. From Figs. 11 and 12, it was also noticed that hygroscopic swelling strain is almost the same for both

Fig. 7 EDS spectra attributed to YAG: Ce



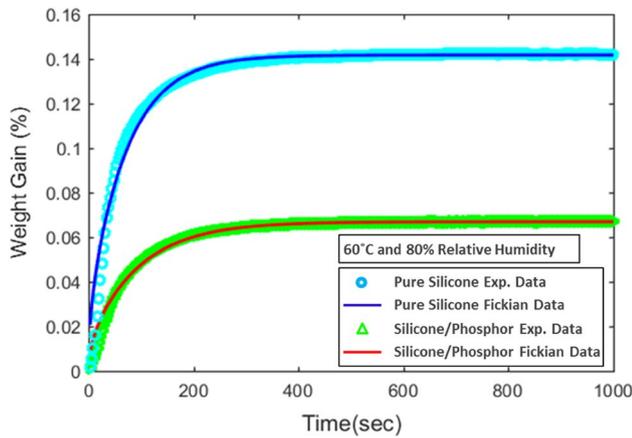


Fig. 10 Fickian diffusion fitting results of pure silicone and silicone/phosphor in moisture desorption. Tests were conducted at 60 °C and 0% RH

Table 1 Extracted diffusivity and saturated moisture concentration from absorption

Diffusion property	Pure silicone	Silicone/phosphor
Diffusivity (cm ² /s)	5.78e-06	3.28e-06
C _{sat} (mg/cm ³)	1.47	1.02
COD (coefficient of determination)	0.97	0.98

Table 2 Extracted diffusivity and saturated moisture concentration from desorption

Diffusion property	Pure silicone	Silicone/phosphor
Diffusivity (cm ² /s)	5.42e-06	2.45e-06
C _{sat} (mg/cm ³)	1.51	1.02
COD (coefficient of determination)	0.97	0.95

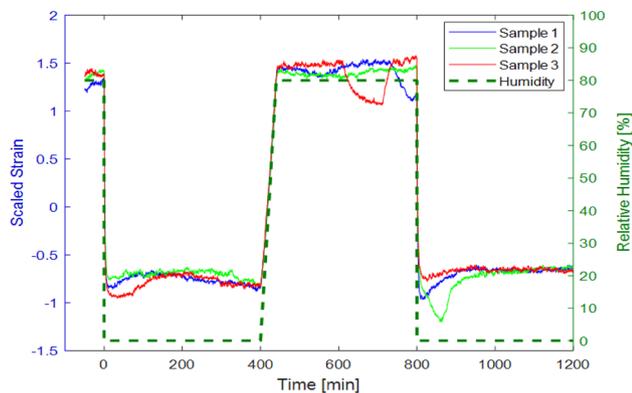


Fig. 11 Hygroscopic strain of pure silicone tested in cycled relative humidity between 0%RH and 80%RH

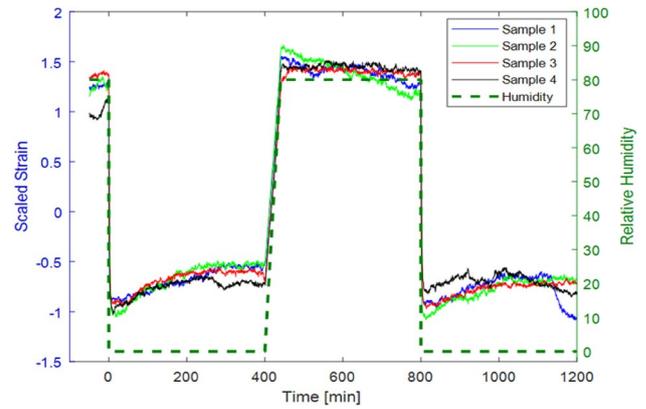


Fig. 12 Hygroscopic strain of silicone/phosphor tested in cycled relative humidity between 0%RH and 80%RH

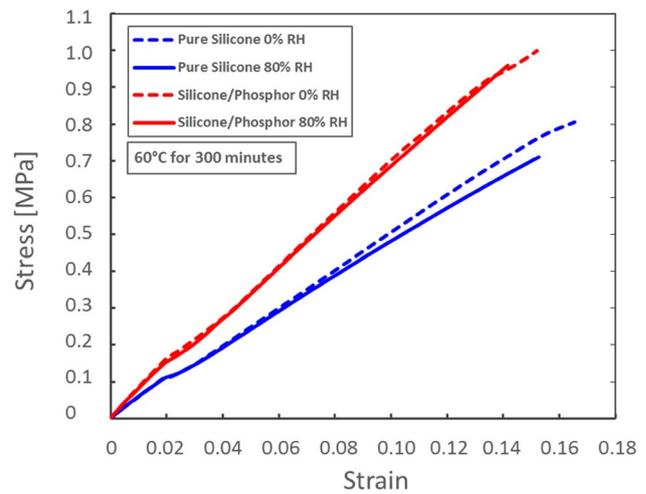


Fig. 13 Comparison of stress–strain curves between pure silicone and silicone/phosphor composite tested at 60 °C under dry and 80% RH conditions

pure silicone and silicone/phosphor. This indicates that the addition of phosphor into silicone has a little effect on the swelling behavior.

Figure 13 plotted the stress–strain curve with and without humidity during strain ramp test for both pure silicone and silicone/phosphor composite. It can be seen that the moisture absorption has almost no effect on the stress–strain behavior for both pure silicone and silicone/phosphor composite. However, it is clearly seen that the silicone/phosphor composite has greater stiffness than pure silicone, but the moisture absorption does not change the material stress–strain behavior.

Figure 14 plots the experimental data of the thermal strain as function of temperature from 50 °C to 300 °C. It shows they have almost the same value of the coefficient of thermal expansion (CTE, the slope of curve). It indicates that

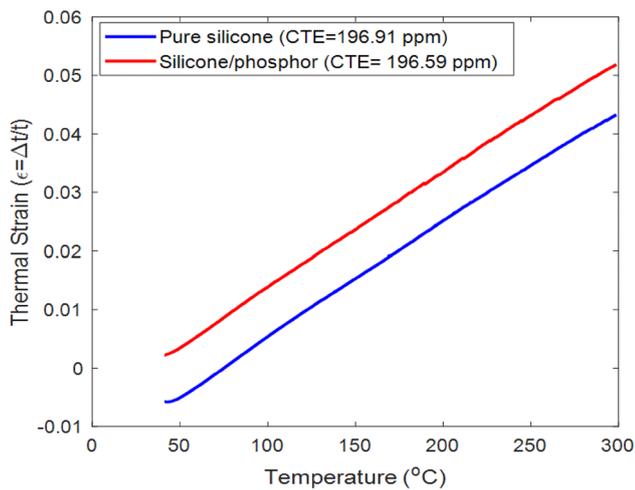


Fig. 14 Thermal expansion of pure silicone and silicone/phosphor composite tested by TMA from 50 °C to 300 °C

the addition of phosphor into silicone does not change the value of CTE.

6 Conclusions

In this paper, the effect of humidity and phosphor addition on silicone/phosphor composite was investigated. We performed an in situ TGA moisture absorption/desorption test for both silicone and silicone/phosphor samples. The results showed both samples follow the Fickian diffusion behavior well. Moisture absorption and desorption are also reversible with the addition of phosphor into silicone. However, the composite reduces the significant amount of moisture absorption compared to the pure silicone, and the diffusion rate increases. In-situ hygroscopic swelling test showed that with and without phosphor, the silicone and composite have almost the same amount of swelling upon moisture absorption. Through the careful experimental analysis, it has confirmed that the previous observation on the permanent swelling for silicone/phosphor composite was false information due to instrument setup issue. The hygroscopic swelling is reversible in absorption/desorption cycle. In strain ramp test, it showed that the moisture has no effect on stress–strain behavior for both silicone and silicone/phosphor samples. But the addition of phosphor enhances the stiffness of material. TMA analysis indicates that the phosphor into silicone does not change the coefficient of thermal expansion in a wide temperature range. In summary, the comprehensive experimental characterization provides a full picture of the effect of humidity and phosphor on the mechanical behavior of silicone/phosphor composite.

Acknowledgement Jiajie Fan would like to acknowledge the support from the National Natural Science Foundation of China (Grant No. 51805147, 61673037).

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