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# Mitigating Electrolyte Flooding for Electrochemical CO<sub>2</sub> Reduction via Infiltration of Hydrophobic Particles in a Gas Diffusion Layer

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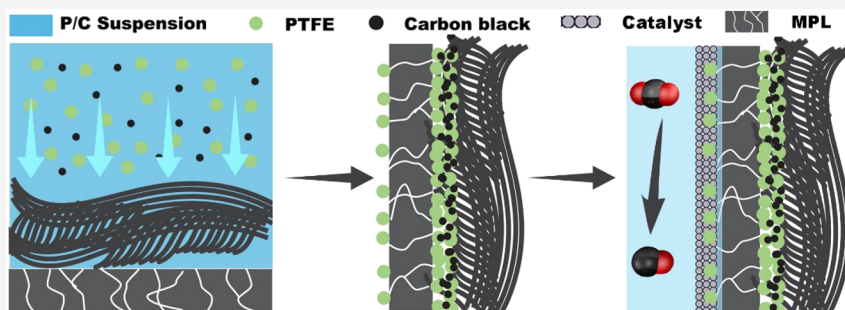
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**ABSTRACT:** Achieving operational stability at high current densities remains a challenge in CO<sub>2</sub> electrolyzers due to flooding of the gas diffusion layer (GDL) that supports the electrocatalyst. We mitigated electrode flooding at high current densities using a vacuum-assisted infiltration method to embed 200–400 nm-sized polytetrafluoroethylene (PTFE) particles at the interface of the microporous layer (MPL) and carbon cloth in a commercial GDL. In CO<sub>2</sub> electrolysis to CO over a silver nanoparticle catalyst on the GDL, the PTFE-embedded GDL not only just exhibited less than 10% of the electrolyte seepage rates observed in untreated GDLs at a current density of 300 mA·cm<sup>-2</sup> but also expanded the electrochemical active area across the testing conditions. The PTFE-embedded GDL also maintained a Faradaic efficiency for CO<sub>2</sub> electrolysis to CO above 80% for more than 100 h at 100 mA·cm<sup>-2</sup>, which was a 50-fold improvement in the stable operation time of the electrolyzer.

The electrochemical CO<sub>2</sub> reduction reaction (CO<sub>2</sub>RR) is a promising technology to reduce CO<sub>2</sub> emissions and produce valuable products,<sup>1</sup> such as CO, formic acid, methane, and ethylene.<sup>2</sup> State-of-the-art continuous CO<sub>2</sub> electrolyzers that use gas diffusion electrodes (GDEs) have been reported to achieve CO<sub>2</sub>RR at industrially relevant current densities, and there are demonstrations at the pilot plant scale.<sup>3</sup> The GDE's porous structure facilitates CO<sub>2</sub> mass transfer from the gas phase to the liquid electrolyte and active catalyst sites at much faster rates than possible with planar electrodes.<sup>4,5</sup> However, managing flooding of liquid electrolytes into the porous structure remains a critical practical challenge for GDEs with operational stability in CO<sub>2</sub> electrolyzers.

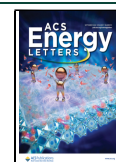
An excellent GDE for CO<sub>2</sub> electrolysis should support a high density of active catalyst sites and facilitate fast transport of gases, ions, and electrons within the electrode.<sup>6</sup> The most

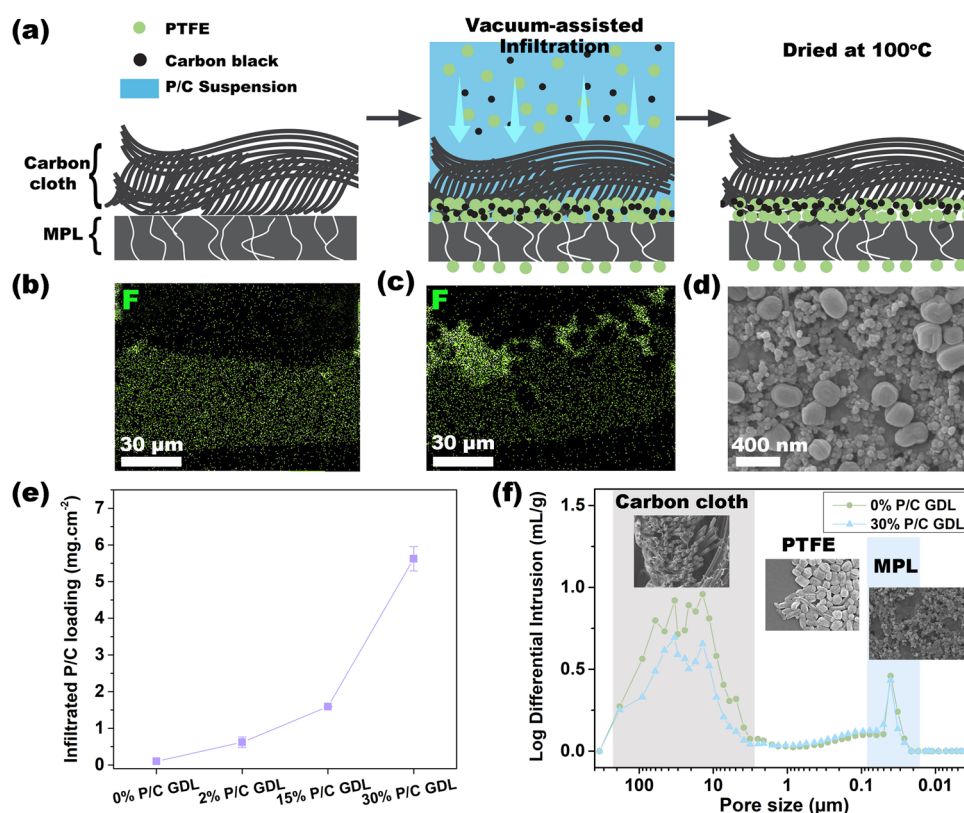
commonly used GDEs in flow-cell CO<sub>2</sub> electrolyzers have a gas diffusion layer (GDL) with carbon fiber support onto which a microporous layer (MPL) and catalyst layer (CL) are deposited.<sup>7</sup> The carbon fiber support (CFS) or macroporous layer is typically a hydrophobic carbon paper or carbon cloth with micron-sized pores<sup>8</sup> that allows fast gas transport and serves as the current collector.<sup>9</sup> The microporous layer is typically made with a mixture of carbon black particles and hydrophobic additives, such as polytetrafluoroethylene

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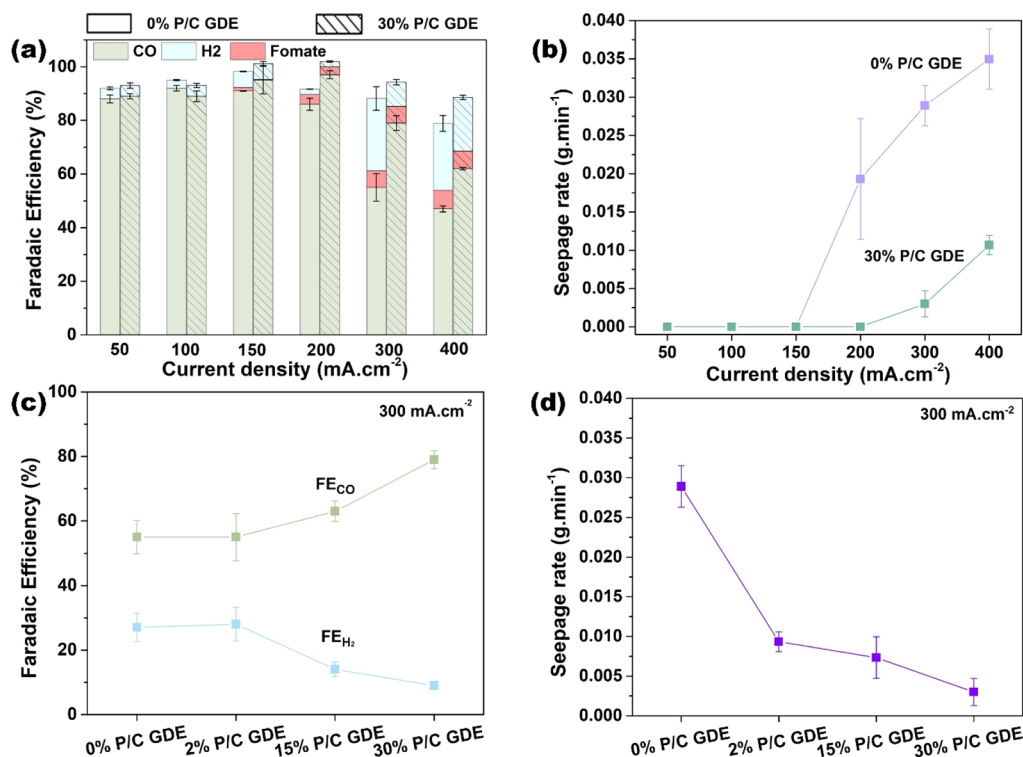
**Figure 1.** Infiltration of polytetrafluoroethylene (PTFE) particles in a commercial gas diffusion layer (GDL). (a) Schematic of the vacuum-assisted infiltration method. (b) Energy-dispersive X-ray spectroscopy (EDS) mapping of fluorine in the cross section of the commercial GDL (F mass% = 4.09%) and (c) in the GDL after 30% P/C infiltration (F mass% = 10.41%). (d) Scanning electron microscope (SEM) image of the surface of the microporous layer (MPL) in the GDL after 30% P/C infiltration. (e) Gravimetric loading of the PTFE and carbon black on GDLs infiltrated with suspensions of different PTFE concentrations. The error bars represent the standard deviation of three independent weightings of three samples. The X% P/C represents constant 10 mg carbon black mixed with the X% PTFE weight ratio in the 10 mL suspension for the infiltration, except 0% P/C represents 10 mL of pure water infiltrated through the GDLs. (f) Pore size distribution of the 0% P/C and 30% P/C GDLs obtained from mercury intrusion porosimetry. The particle size of PTFE in the aqueous suspension (200–400 nm) is between the pore sizes of carbon cloth and MPL.

(PTFE). The MPL plays an essential role in supporting the CL, distributing current, and preventing electrolyte flooding into the gas diffusion layer.<sup>10,11</sup>

Although carbon cloth GDLs are widely used in CO<sub>2</sub> electrolyzers, these GDLs are known to become less hydrophobic during CO<sub>2</sub> electrolyzer operation at highly negative potentials because of electrowetting of carbon sites under an applied electrical field,<sup>12,13</sup> salt precipitation,<sup>14,15</sup> and chemical degradation.<sup>16</sup> When the hydrophobicity of the GDL is reduced, electrolyte penetrates the pores of the GDL, which leads to increased distances for CO<sub>2</sub> diffusion and blocks CO<sub>2</sub> transport to CO<sub>2</sub>RR catalyst sites. In addition, flooding can impact CO<sub>2</sub>RR selectivity as the restriction of CO<sub>2</sub> transport to active sites leads to the promotion of the hydrogen evolution reaction (HER).<sup>16–18</sup> To date, most CO<sub>2</sub> electrolyzer studies used commercial GDLs that were designed and fabricated for polymer electrolyte membrane fuel cells (PEMFC) that experience very different operational conditions to CO<sub>2</sub>RR.<sup>10,19–22</sup> For a PEMFC, the cathode is to convert oxygen gas to water liquid. For CO<sub>2</sub> electrolysis, however, the cathode is driven by the electric potential to convert CO<sub>2</sub> gas into either gas or liquid products, which is drastically different from the reaction scenario for PEMFC.<sup>5,22,23</sup> Furthermore, GDLs for PEMFCs provide the path for the water removed from the catalyst layer to gas flow channel, but electrolyte flow

is desired to be constrained in the liquid channel within the CO<sub>2</sub> electrolyzer.

The development of low-cost, large-scale CO<sub>2</sub> electrolysis technologies is more likely to be successful if CO<sub>2</sub> electrolyzers can take advantage of the supply chain infrastructure already developed for other applications, such as PEM fuel cells and H<sub>2</sub> electrolyzers. Therefore, mitigating flooding in commercial GDLs for the CO<sub>2</sub> electrolyzer is an urgent matter.<sup>6,16,24</sup> Hydrophobic treatments of microporous layers have been reported for GDLs designed for PEM fuel cells,<sup>25,26</sup> and there are a few recent reports on adding hydrophobic agents during fabrication of the catalyst layer on the GDL.<sup>27,28</sup> For example, hydrophobic additives such as fluoroalkyl silane<sup>28</sup> and PTFE<sup>27,29</sup> have been added to catalyst layers in GDEs for CO<sub>2</sub> electrolysis. The addition of the hydrophobic additives to the CL achieved improvements in the CO<sub>2</sub> electrolysis performance at short operating durations, but to date these CO<sub>2</sub> electrolysis improvements and hydrophobicity enhancements have not been reported to be sustained through CO<sub>2</sub>RR stability tests at high current density.<sup>30</sup> Another approach that has achieved stable CO<sub>2</sub>RR performance is replacing the carbon-based GDL with a nonconductive porous hydrophobic membrane (e.g., PTFE membranes<sup>31,32</sup>) coated with a conductive catalyst layer such as sputtered Cu. Electrolyzers with PTFE membranes as GDEs have demonstrated excellent



**Figure 2.** CO<sub>2</sub> reduction reaction performance of silver nanoparticle catalysts on gas diffusion electrodes (GDEs) in a gas-fed flow cell electrolyzer (Figures S10 and S11) with the catholyte of 0.1 M NaHCO<sub>3</sub> flowing at 2 mL/min and the anolyte of 1 M KOH at 10 mL/min. (a) Faradaic efficiency (FE) of the detectable CO, H<sub>2</sub>, and formate of 0% P/C and 30% P/C GDEs. Here, GDE indicates the electrode after the Ag catalyst was sprayed onto the microporous layer of the gas diffusion layers. The X% P/C represents constant 10 mg carbon black mixed with the X% PTFE weight ratio in the 10 mL suspension for the infiltration, except 0% P/C represents 10 mL of pure water infiltrated through the GDLs. (b) Average rate of catholyte seepage through the GDEs measured during the electrolysis tests using the method in Figure S9. (c) FE for detectable CO and H<sub>2</sub> in CO<sub>2</sub> electrolysis tests with 0% P/C, 2% P/C, 15% P/C, and 30% P/C GDEs at 300 mA·cm<sup>-2</sup>. (d) Average rates of catholyte seepage of the four GDEs in part (c) at a current density of 300 mA·cm<sup>-2</sup>. The error bars on FEs in (a) and (c) represent the standard deviation of three measurements of electrolyzer effluent gas compositions. The error bars on seepage rates in (b) and (d) represent the standard deviation of three independent measurements on fresh GDEs for each measured current density.

CO<sub>2</sub>RR performance at current densities of up to 1000 mA·cm<sup>-2</sup>,<sup>32</sup> but there are practical challenges to applying PTFE membranes at a large scale and low cost. Therefore, there remains a need to improve the performance of carbon-based GDLs, including the tailoring of commercial GDLs that are available at low cost for CO<sub>2</sub> electrolyzers.

We report a simple, vacuum-assisted infiltration method (Figure 1a) to deposit PTFE particles and carbon black preferentially at the interface between the microporous layer and the carbon cloth in a commercial GDL. The vacuum-assisted infiltration allows some PTFE particles to be transported through existing cracks in the MPL<sup>33</sup> and protrude into the CL to provide additional protection against electrolyte flooding through the MPL cracks. In our CO<sub>2</sub>RR experiments with a commercial GDL and silver nanoparticle catalyst, the PTFE-embedded GDE achieved a Faradaic efficiency to CO (FE<sub>CO</sub>) of nearly 80% at 300 mA·cm<sup>-2</sup>. Remarkably, at 100 mA·cm<sup>-2</sup> our PTFE-embedded GDE operated stably for more than 100 h with a FE<sub>CO</sub> above 80%, which was more than 50 times longer than for the untreated GDE.

We introduced the PTFE particles to the commercial GDL from a suspension of PTFE and carbon black particles in water that we sucked through the GDL using a vacuum filter, as shown in Figure 1a and Figure S1. The SEM images in Figure S2 show the approximate sizes of these 9PTFE particles in the GDL were determined from the fluorine (F) signal in SEM-

EDS elemental maps of the cross section of the GDL, which was imaged by mounting the GDL in epoxy resin. First, we had to establish a benchmark for the F signal of the PTFE coating in the commercial GDL (Figure 1b). Compared to this benchmark F distribution, we can see in Figure 1c that after infiltration, there is a significantly higher concentration of F at the interface of the carbon cloth layer and the microporous layer, which shows the PTFE particles accumulate at this interface in GDL. We also observed in SEM images of the MPL face of the GDL that some PTFE particles protrude from the MPL's surface (Figure 1d). This observation suggests that some PTFE particles migrated through original cracks, up to 5 μm wide, in the MPL (Figure S4) and lodged at the underside of the MPL that pressed against the glass filter of the vacuum apparatus (illustrated in Figure S1).

We conducted a series of experiments to control the ratio of PTFE to carbon black embedded in the GDLs by modifying the composition of the suspension liquid, as shown in Figure 1e. The loading increases with the weight percentage of PTFE up to  $5.6 \pm \text{mg} \cdot \text{cm}^{-2}$  for the 30% P/C suspension. Along with the weight percentage of PTFE, the density of the PTFE protrusions from MPL can be controlled as well (as shown in Figure S5).

The location of PTFE particles in the modified GDLs was also analyzed by characterizing the pore size distribution (PSD) of the carbon cloth and MPL layers. The PSDs



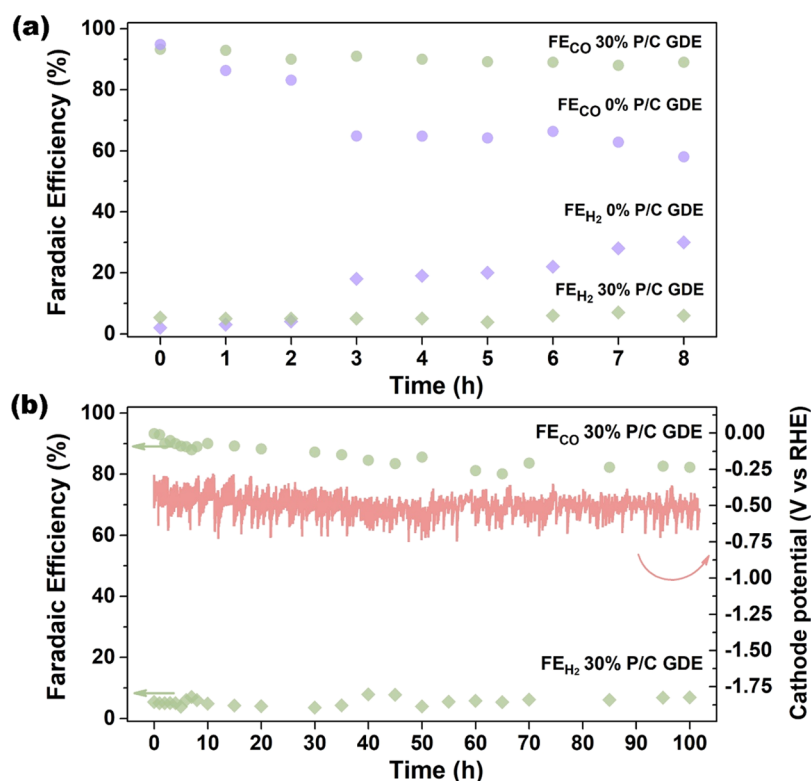


Figure 3. Electrolyzer performance stability tests over 8 and 100 h. (a) Faradaic efficiency for CO and H<sub>2</sub> with the 0% P/C GDE and 30% P/C GDE during an 8 h CO<sub>2</sub> electrolysis experiment at a current density of 100 mA·cm<sup>-2</sup>. (b) Faradaic efficiency for CO and H<sub>2</sub> and cathode potential for the 30% P/C GDE experiment in an additional 100 h test at a current density of 100 mA·cm<sup>-2</sup>. The X% P/C represents constant 10 mg carbon black mixed with the X% PTFE weight ratio in the 10 mL suspension for the infiltration, except 0% P/C represents 10 mL of pure water infiltrated through the gas diffusion layers (GDLs).

obtained from mercury intrusion porosimetry (MIP) in Figure 1f show the PSD of the 0% P/C GDL has the most volume in pores of size ranges 10–100  $\mu\text{m}$  and 20–40 nm (MIP cumulative intrusion plot included in Figure S6), which we expect to be in the carbon cloth and MPL, respectively. The MIP data in Table S1 shows the 30% P/C GDL had 11% less total pore volume than the 0% P/C GDL. The PSDs in Figure 1f show the added PTFE and carbon black particles in 30% P/C sample occupied pores in the micrometer range, primarily in the carbon cloth layer. These MIP results provide additional evidence that the 200–400 nm-sized PTFE particles can move relatively freely through the large carbon cloth pores during the vacuum-assisted infiltration but become lodged at the interface to the MPL (as illustrated in Figure 1a and Figure 1c).

To prepare GDE, we deposited the silver catalyst layer on the GDL samples by air-brushed spray coating an ink of silver nanoparticles (Ag NPs), carbon black, and Nafion ionomer onto the MPL surface. Figure S7a–d shows that this method distributed the Ag NPs evenly on a micrometer-scale across the MPLs of 0% P/C and 30% P/C GDEs. We estimated the thickness of the catalyst layers to be approximately 15  $\mu\text{m}$  from the cross-section SEM images (Figure S7f,h) and the Ag elemental maps from SEM-EDS (Figure S7e,g). There is no apparent difference in the top surface of the catalyst layers of the 0% P/C and 30% P/C GDEs.

The CO<sub>2</sub>RR to CO performance of the control 0% P/C GDE and the PTFE-embedded 30% P/C GDEs was compared in a sandwich-type flow cell electrolyzer with a single-pass 0.1 M KHCO<sub>3</sub> catholyte flow (Figure S8). The cell was completed with an IrO<sub>2</sub> coated titanium plate anode, a 1 M KOH anolyte,

and a Nafion 117 membrane. We measured the catholyte seepage rate through the GDEs using the recently reported method.<sup>34</sup> Briefly, we separated and collected any liquid carried out with gases from the cathode chamber in a two-neck Erlenmeyer flask placed on an analytical balance (Figure S9). An overall schematic of the flow cell electrolyzer and effluent measurements system is provided in Figure S10.

Figure 2 compares the CO<sub>2</sub>RR to CO performance of the 0% P/C GDE and the 30% P/C GDE, with the cathode potentials for these tests summarized in Figure S11. At current densities less than 150 mA·cm<sup>-2</sup>, the CO<sub>2</sub>RR product selectivity (Figure 2a) is similar for the 0% P/C and 30% P/C GDEs, with FEs close to 90% for CO and less than 10% for H<sub>2</sub>. We did not observe electrolyte seepage from the cathodes at current densities below 150 mA·cm<sup>-2</sup> (Figure 2b). However, at current densities above 150 mA·cm<sup>-2</sup>, the 30% P/C GDE was more CO selective than the 0% P/C GDE. For example, at 200 mA·cm<sup>-2</sup>, the  $\text{FE}_{\text{CO}}$  remained  $97.2 \pm 1.5\%$  for 30% P/C GDE but dropped to  $86.3 \pm 2.2\%$  for 0% P/C GDE. At 300 mA·cm<sup>-2</sup>, the  $\text{FE}_{\text{CO}}$  achieved was  $79.5 \pm 2.8\%$  for 30% P/C GDE and only  $55.0 \pm 5.1\%$  for the 0% P/C GDE. We also observed some formate in the liquid products at current densities above 150 mA·cm<sup>-2</sup>, and its selectivity increased with current densities. Formate production during CO<sub>2</sub>RR is common on the Ag-based catalyst.<sup>35</sup>

The main difference in the selectivity of the two GDEs is observed in the H<sub>2</sub> produced at the higher current densities, which is likely due to the electrode flooding that reduces the local CO<sub>2</sub> availability within the catalyst layer.<sup>24</sup> The trend in H<sub>2</sub> production rates is consistent with the seepage rates shown

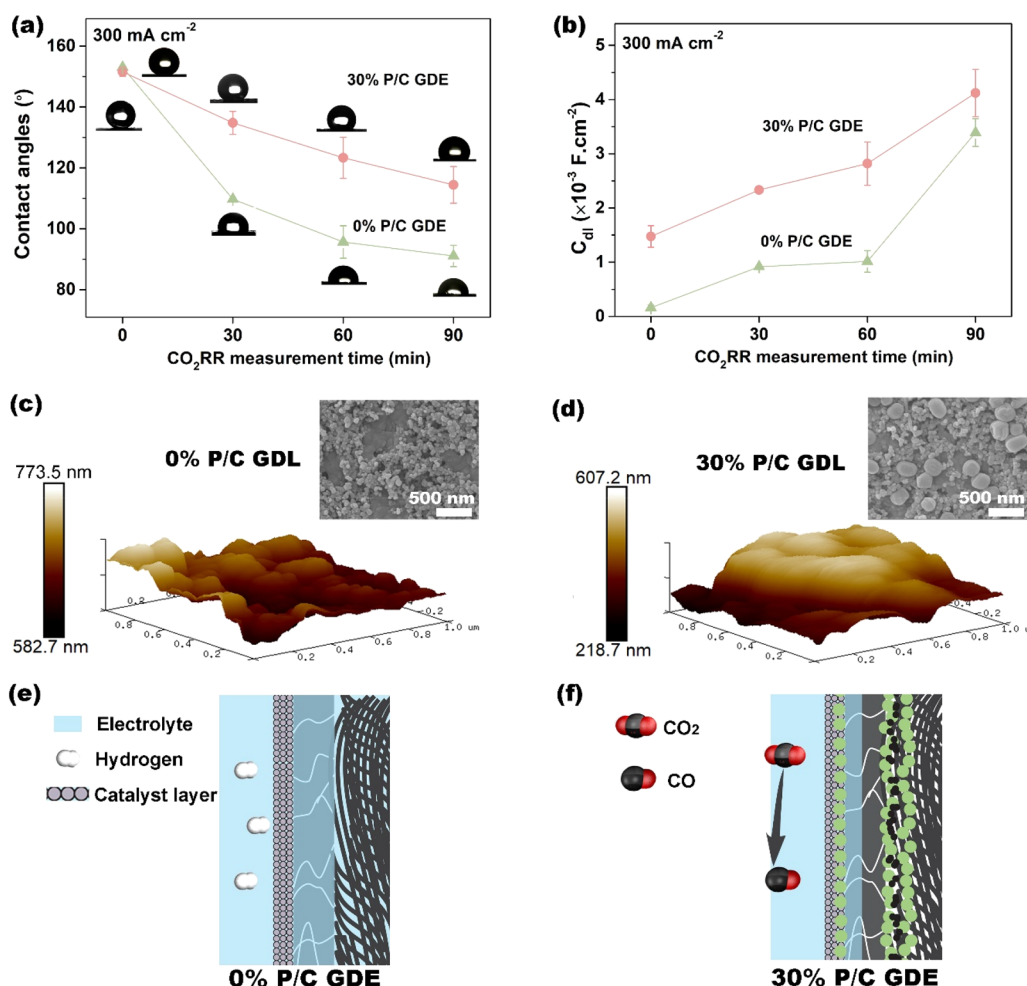


Figure 4. Changes in hydrophobicity and specific double layer capacitance ( $C_{dl}$ ) of the gas diffusion electrodes (GDEs) after exposure to CO<sub>2</sub> electrolysis conditions. (a) Change in wetting contact angles on the catalyst layer of the 0% P/C and 30% P/C GDEs after CO<sub>2</sub> electrolysis at 300 mA·cm<sup>-2</sup> for 30, 60, and 90 min. The 0 min sample is a freshly prepared GDE that has not been used in the electrolyzer. The error bars on contact angle data points represent the standard deviation of nine drop measurements on three areas of three independently prepared GDEs. (b) Specific double layer capacitance of 0% P/C and 30% P/C GDEs before and after CO<sub>2</sub> electrolysis at 300 mA·cm<sup>-2</sup> for 30, 60, and 90 min.  $C_{dl}$  calculated from electrochemical surface area as described in the [Supporting Information](#). Error bars in (b) represent the standard deviation of three independent measurements. (c) and (d) Topographic images from atomic force microscope (AFM) scans of  $1 \times 1 \mu\text{m}^2$  areas of the microporous layer (MPL) of (c) the 0% P/C gas diffusion layer (GDL) and (d) the 30% P/C GDL. (e) and (f) Schematic representations of the interactions of H<sub>2</sub> and CO<sub>2</sub> species with the electrochemically active surface area during CO<sub>2</sub> electrolysis of the gas diffusion electrodes (GDEs) without the hydrophobic particles in (e) 0% P/C GDE and (f) 30% P/C GDE. The X% P/C represents constant 10 mg carbon black mixed with the X% PTFE weight ratio in the 10 mL suspension for the infiltration, except 0% P/C represents 10 mL of pure water infiltrated through the GDLs.

in Figure 2b, with the hydrophobic PTFE-embedded GDE more resistant to electrolyte flooding. For example, at 300 mA·cm<sup>-2</sup>, the 30% P/C GDE exhibited a seepage rate 9.7 times lower than the seepage rate through 30% P/C GDE, which contributed to the falling catholyte mass transfer resistance from the additional layer.

On the other hand, the CO<sub>2</sub> permeance from the carbon cloth to MPL was measured for 30% P/C and 0% P/C, respectively, as shown in Figure S15. The gas permeance of 30% P/C GDL slightly decreased due to the lower porosity in carbon cloth (Figure 1f), which further led to lower CO selectivity than the 0% P/C GDE at 100 mA·cm<sup>-2</sup> (Figure 2a). With the flooding promoted at high current densities, however, the tiny advantage was eliminated by the electrode flooding MPL that substantially increased the resistance of CO<sub>2</sub> transfer to the catalyst and promoted H<sub>2</sub> production. Consequently, the 30% P/C GDE electrode can achieve a FE<sub>CO</sub> nearly 80% at

300 mA cm<sup>-2</sup>, much higher than the 0% P/C GDE with a FE<sub>CO</sub> of  $55.0 \pm 5.1\%$ . Based on the above observations, we postulate that the enhanced CO selectivity results from the hydrophobic PTFE particles embedded at the MPL-GDL interface by the vacuum-assisted infiltration method. These features restrict flooding of the GDE across the MPL layer.

As the largest difference in the FE<sub>CO</sub> between the 0% P/C and the 30% P/C GDEs was at current densities of 300 mA·cm<sup>-2</sup>, we used this condition as an operating point to study the effects of PTFE loadings on the performance. Figure 2c shows that increasing the loading of PTFE led to higher FE<sub>CO</sub> and lower rates of HER. Again, this trend likely arises from the role of the PTFE particles at the catalyst-MPL interface that creates a hydrophobic microenvironment in the catalyst layer for efficient gas transport while maintaining a high electrochemical surface area for CO<sub>2</sub>RR. As shown in Figure 2d, the seepage rate of GDEs dropped with a higher PTFE content. In other

words, more PTFE in the interface between MPL and carbon cloth makes the GDE more resistant to flooding and thus improves the CO<sub>2</sub>RR efficiency.

The orientation of the GDL during the vacuum-assisted infiltration is crucial to depositing the PTFE particles at the optimum location in the GDL. If the GDL is orientated with the microporous layer facing up in the vacuum apparatus (Figure S12), the PTFE particles simply cover the surface of the MPL (Figure S12b). Subsequent deposition of the catalyst layer on this PTFE-coated MPL structure leads to an electrode with poorer electrical conductivity, low CO selectivity (FE<sub>CO</sub> = 38.1 ± 3.5%), and high HER rates (FE<sub>H<sub>2</sub></sub> = 50.2 ± 5.8%). This additional experiment highlights that the excellent flooding resistance and CO<sub>2</sub>RR achieved with the PTFE-embedded GDE are not solely related to the total amount of PTFE added to the electrode but depend on precisely where the PTFE particles deposit.

The electrolyzer stability tests performed at 100 mA cm<sup>-2</sup> reported in Figure 3a show that the control 0% P/C GDE can sustain a FE<sub>CO</sub> above 80% for the first 2 h of operation, but after 3 h, the rate of H<sub>2</sub> production increased significantly. In contrast, the 30% P/C GDE maintained a FE<sub>CO</sub> of 90% for at least 8 h. These results show the enhanced resistance to electrode flooding of the 30% P/C GDE improved the electrode stability remarkably. We repeated the stability test at 100 mA cm<sup>-2</sup> with 30% P/C GDE for an extended period of 100 h (Figure 3b). We found that the FE<sub>CO</sub> remained above 82.2% even after 100 h with no significant degradation in the cathode cell potential (remained around -0.5 V vs RHE). Figure S13 highlights that the performance of 30% P/C GDE is among the most stable Ag-based electrodes achieving a FE<sub>CO</sub> above 70% in the liquid flow cell CO<sub>2</sub> electrolyzer at current densities above 100 mA·cm<sup>-2</sup> reported in the literature.<sup>10,19,31,36–39</sup> We acknowledge that a 100 h operation is well short of the targets of several thousand hours operation required for industrial CO<sub>2</sub> electrolyzers.<sup>40</sup> There are a limited number of reports of CO<sub>2</sub> flow cell electrolyzers for CO production operated for more than 100 h, but the studies that achieved a FE<sub>CO</sub> greater than 80% were conducted at current densities below 100 mA·cm<sup>-2</sup>, for example the 4380 h test at 50 mA·cm<sup>-2</sup> by Kutz et al.<sup>41</sup>

The previous section demonstrated that the PTFE-embedded GDE achieved higher Faradaic efficiencies for much longer durations than the control GDE. Next, we closely examine how the PTFE treatment impacts the hydrophobicity and electrochemically active surface area (ECSA) of GDE. We studied the hydrophobicity using a sessile drop method to measure the water contact angles on the surface of the catalysts layer. As shown in Figure 4a, both the 0% P/C and 30% P/C GDEs were hydrophobic before use in the CO<sub>2</sub> electrolyzer, with water contact angles over 150°. The high hydrophobicity can be attributed to the similar roughness of the catalyst layer (Figures S7 and S16).<sup>42,43</sup> We performed a series of CO<sub>2</sub> electrolysis experiments at 300 mA·cm<sup>-2</sup> with GDEs exposed to the CO<sub>2</sub>RR conditions for 30, 60, and 90 min. After these exposure times, the GDEs were rinsed of excess catholyte off the catalyst layer and then dried. We observed that the contact angles of the catalyst layer for both electrodes decreased with increasing exposure time to CO<sub>2</sub>RR conditioning (Figure 4a). The permanent contact angle loss is likely due to degradation of hydrophobic PTFE and carbon black in the catalyst layer when charged by the negative potential.<sup>5,13,44</sup> This observation is consistent with our previous and others results<sup>29,34</sup> and

linked to the increment of electrolyte flooding.<sup>14,45</sup> Nevertheless, the contact angle of the 0% P/C GDE decreased faster and to a lower angle after 90 min (91.4 ± 3.5°) than the 30% P/C GDE, which remained hydrophobic after 90 min of CO<sub>2</sub> electrolysis (contact angle = 114.4 ± 6.0°). The lower contact angles drop over 30% P/C GDE (Figure 4a) could arise from the experience of more positive cathode potentials (-0.85 V vs RHE) than 0% P/C GDE (-1.04 V vs RHE) at 300 mA·cm<sup>-2</sup> (Figure S11). These experiments confirm that the 30% P/C GDE retains its hydrophobicity for longer than the 0% P/C GDE, but a more detailed study is required to understand better why the PTFE in the carbon cloth layer and protruding into the CL has such a profound impact on the stability of the CL's hydrophobicity.

Many other studies that report an increase in electrode hydrophobicity also report that this hydrophobicity comes with a reduced electrochemically active surface area (ECSA),<sup>24,46</sup> which is generally detrimental to CO<sub>2</sub>RR performance.<sup>47</sup> Figure 4b shows the ECSAs that we estimated from the specific double-layer capacitance (C<sub>dl</sub>) of our 0% P/C and 30% P/C GDEs increase with the duration of CO<sub>2</sub> electrolysis at 300 mA·cm<sup>-2</sup>. Such enhancement of ECSA is ascribed to the hydrophobicity loss (Figure 4a) due to the degradation of Nafion and carbon black in the catalyst layer as stated before and then leads to an increase in electrolyte-catalyst contact within the catalyst layer. Notably, the ECSAs of the hydrophobic 30% P/C GDE are larger than 0% P/C across the testing conditions, which is highly desired for GDE development.<sup>12</sup> The improvement of the ECSA may be explained by the expansion of the surface area at the MPL. PTFE particles (Figure 1d) that passed through the MPL cracks during the infiltration enhance the roughness of the MPL considerably (see Figure 4c,d, Figure S16a,b). After the catalyst is deposited, the particles covered by the catalyst layer hardly change the surface roughness of the catalyst layer (see Figure S16c,d). The higher roughness comes with an enlarged surface area. More impressively, our results provide another possibility to recognize the relationship: the variation trend of ECSA may not always be consistent with the surface hydrophobicity.

As illustrated in Figure 4e,f, these PTFE particles protruding into the catalyst layer increase the active area for the reaction (ECSA) at a constant Ag loading, which improves the CO selectivity (Figure 2a). Most importantly, the 30% P/C GDE can prevent GDE from serious flooding during CO<sub>2</sub> electrolysis. Maintaining both these properties is important to ensure a high local CO<sub>2</sub> availability and active surface for CO<sub>2</sub>RR at industrially applicable current densities.

In conclusion, we used a vacuum-assisted infiltration method to embed PTFE particles in commercial GDLs, and this structure improved the performance of these GDLs as supports for CO<sub>2</sub> electrolysis cathodes. This method embedded the PTFE particles at the interface of the microporous layer and the carbon cloth, and some PTFE particles passed through cracks in the MPL to protrude into the catalyst layer. The protruding PTFE particles led to increased surface areas in the catalyst layer that we subsequently deposited on the GDL. The PTFE-embedded GDEs exhibited excellent selectivity for CO<sub>2</sub> electrolysis to CO at high current densities and outstanding resistance to electrolyte flooding. The PTFE-embedded 30% P/C GDE was able to maintain the FE<sub>CO</sub> above 80% for more than 100 operating hours at 100 mA·cm<sup>-2</sup>. This work provides an avenue to tailor commercially available GDLs to the



requirements of CO<sub>2</sub> electrolyzers and paves the way for the large-scale application of carbon-based GDE.

## ■ ASSOCIATED CONTENT

### SI Supporting Information

The Supporting Information is available free of charge at <https://pubs.acs.org/doi/10.1021/acsenenergylett.2c01555>.

Experimental materials and methods including schematic and photograph of electrolyzer apparatus; additional SEM images and EDS elemental maps of fluorine; cumulative pore size distribution results from mercury intrusion porosimetry; cathode potential of 0% P/C and 30% P/C gas diffusion electrodes vs current density; comparison of FE<sub>CO</sub> observed in our 100 h stability test with other Ag-based GDEs reported in literature; calculation method and results for electrochemical active surface area (ECSA); gas permeance results for CO<sub>2</sub> flow in gas diffusion electrodes; surface roughness contours obtained from optical profiler; additional contact angle measurement data; partial current density for CO of 0% P/C and 30% P/C electrolyzer tests; and supporting references (PDF)

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### Notes

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