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An introduction with exercises

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Introduction to Traffic Flow Theory:
An introduction with exercises

V.L. Knoop

First edition

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Preface

Traffic processes cause several problems in the world. Traffic delay, pollution are some of it. They can be solved with the right road design or traffic management (control) measure. Before implementing these designs of measures, though, their effect could be tested. To this end, knowledge of traffic flow theory is needed.

This book is meant as learning book for students. To learn an engineering discipline, practicing is essential. One of the core qualities of this book, is that more than 250 practice questions (and answers) are available. Therefore, this book can be used as material for courses.

The historical perspective is that the book is an end product of developing, using and continuously improving the lecture notes at Delft University of Technology. I am grateful for the comments by students, and the help of colleagues to this book. It should be mentioned that section 9.4 and 9.5.2 are in majority is written by Femke van Wageningen-Kessels.

I believe that sharing this work can help students, lecturers and possibly practitioners. An online version of the course Traffic Flow Theory and Simulation, including lectures given at Delft University of Technology is freely and openly available via Open Courseware at TU Delft (<https://ocw.tudelft.nl/>, search for traffic and you will find the course on <https://ocw.tudelft.nl/courses/traffic-flow-theory-simulation/>). I believe in open access, and a community where knowledge is shared. The book is hence free to use, and free to distribute to students.

The book is, like science, not finished. By now, it has reached a state of maturity that students highly value the book as it is. Therefore, this is for me the time to share this work. I plan to have regular (yearly) updates to the book. If you have remarks – errors, additional request, things which are unclear – please let me know at v.l.knoop@tudelft.nl.

The book is meant as introduction to the field of traffic flow theory. Only basic calculus is assumed as base knowledge. For more in-depth knowledge, the reader can continue in other books, including:

- May, A.D. Traffic flow fundamentals. 1990.
- Leutzbach, W. Introduction to the theory of traffic flow. Vol. 47. Berlin: Springer-Verlag, 1988.
- Daganzo, C.F. Fundamentals of transportation and traffic operations. Vol. 30. Oxford: Pergamon, 1997.
- Treiber, M., and A. Kesting. "Traffic flow dynamics." Traffic Flow Dynamics: Data, Models and Simulation, Springer-Verlag Berlin Heidelberg (2013).
- Elefteriadou, L. An introduction to traffic flow theory. Vol. 84. New York, NY, USA: Springer, 2014.
- Ni, D. Traffic Flow Theory: Characteristics, Experimental Methods, and Numerical Techniques. Butterworth-Heinemann, 2015.

Of course, there also is a vast, and ever expanding, body of scientific literature which the reader can use as follow-up material.

Contents

1	Variables	1
1.1	Levels of description	1
1.1.1	Microscopic	1
1.1.2	Marcoscopic	2
1.1.3	Other levels	4
1.2	Measuring principles	4
1.2.1	Local	4
1.2.2	Instantaneous	5
1.2.3	spatio-temporal measurements	5
1.3	Stationarity and homogeneity	7
2	Headway models	9
2.1	Relation between headway and capacity	9
2.2	Arrivals per interval	9
2.2.1	Poisson	10
2.2.2	Binomial	10
2.2.3	Negative binomial	12
2.3	Headway distributions	12
2.3.1	Exponential	12
2.3.2	Composite headway models	13
2.4	Critical gap	14
2.4.1	Situations	14
2.4.2	Inflow capacity	14
3	Cumulative curves	17
3.1	Defenition	17
3.2	Vertical queuing model	17
3.3	Travel times, densities and delays	19
3.3.1	Construction of cumulative curves	19
3.3.2	Travel times, number of vehicles in the section	19
3.3.3	Delays	19
3.4	Slanted cumulative curves	20
3.5	Practical limitations	21
3.6	Example application	21
4	Relationships of traffic variables	25
4.1	Fundamental relationship	25
4.2	Fundamental diagram	26
4.2.1	Qualitative understanding of the shape	26
4.2.2	Traffic state	26

4.2.3	Important points	26
4.2.4	Fundamental diagram in different planes	27
4.2.5	Shapes of the fundamental diagram	27
4.3	Microscopic behaviour	29
4.3.1	Equilibrium behaviour	29
4.3.2	Hysteresis	29
4.4	Moving observer	31
5	Shock wave theory	35
5.1	Fixed bottlenecks	35
5.1.1	Theory and derivation of equations	35
5.1.2	Example: Temporal increase in demand at a road with a lane drop	36
5.1.3	Example: Temporal capacity reduction	39
5.2	Moving bottleneck	40
5.2.1	Theory	40
5.2.2	Example 1: moving truck, no overtaking possibilities	41
5.2.3	Example 2: moving truck with overtaking possibilities	42
5.2.4	Example 3: moving truck and high demand	44
5.3	Stop and go waves	46
6	Method of characteristics	47
6.1	Mathematical construction	47
6.1.1	Construction	47
6.1.2	Application to homogeneous roads	48
6.1.3	Interpretation	49
6.2	Application	49
6.2.1	Acceleration fan	49
6.2.2	Deceleration	50
7	Traffic states and Phenomena	53
7.1	Stability	53
7.1.1	Local stability	53
7.1.2	Platoon stability	53
7.1.3	Traffic flow stability	55
7.1.4	Use of stability analysis	55
7.2	Capacity drop	55
7.2.1	Phenomenon description	55
7.2.2	Empirics (from Yuan et al. (2015a))	56
7.3	Stop-and-go wave	57
7.3.1	Phenomenon description	57
7.4	Kerner's Three Phase Traffic Flow Theory	58
7.4.1	States	58
7.4.2	Transitions	60
8	Car-following	63
8.1	Newell's car following model	63
8.2	Characteristics	64
8.2.1	Dependencies	64
8.2.2	Reaction time	64
8.2.3	Multi leader car-following models	65
8.2.4	Insensitivity depending on distance	65
8.3	Examples	67

8.3.1	Helly	67
8.3.2	Optimal Velocity Model	67
8.3.3	Intelligent Driver model	67
8.4	Relation to fundamental diagram	68
9	Macroscopic Dynamic Traffic flow Models	71
9.1	Mathematical models	71
9.2	Spatial and temporal discretisation	72
9.3	Event based	73
9.3.1	Link Transmission Model	73
9.4	Lagrangian coordinates	74
9.4.1	Introduction	74
9.4.2	Mathematical formulation of the traffic flow equations	76
9.4.3	Advantages of Lagrangian formulation	77
9.5	Multi-class	77
9.5.1	Principles	77
9.5.2	Fastlane	80
9.6	Higher order modelling	81
9.7	Suggested problems	81
10	Microscopic lane change models	83
10.1	Introduction	83
10.2	Type of lane changes	83
10.3	Slugs and rabbits	83
10.3.1	Theory	83
10.3.2	Traffic operations	85
10.3.3	Loading	85
10.3.4	Consequences	85
10.4	Utility model	85
10.4.1	Model idea	85
10.4.2	Model equations	86
10.5	Integrated modelling	87
11	Macroscopic fundamental diagram	89
11.1	Perimeter control	91
11.2	Traffic dynamics	92
11.2.1	Approaches to include the standard deviation	92
11.3	Simulation	95
11.4	Recent insights	95
12	Use of traffic models	99
12.1	Goal of the model	99
12.2	Type of models	99
12.2.1	Level	99
12.2.2	Stochasticity	100
12.2.3	Different user classes	101
12.3	Calibration	101
12.3.1	Use of calibration	101
12.3.2	Techniques	102
12.3.3	Number of parameters	103
12.4	Validation	103
12.4.1	Need of validation	103

12.4.2	Data handling for calibration and validation	103
12.4.3	Techniques	104
12.5	Often made mistakes	104

Alphabetical Index 105

A	Test questions	113
A.1	Problem set 1	113
A.1.1	Short questions	113
A.1.2	State recognition	113
A.1.3	Simulation model	114
A.1.4	Moving bottleneck	115
A.1.5	Marathon Delft	115
A.2	Problem set 2	115
A.2.1	Short open questions	115
A.2.2	Leaving the parking lot	116
A.2.3	Traffic lights	116
A.2.4	Car-following model	118
A.2.5	Pedestrians in a narrow tunnel	119
A.2.6	Moving bottleneck with different speeds	119
A.3	Problem set 3	120
A.3.1	Short open questions	120
A.3.2	Multi-leader car-following models	121
A.3.3	Measuring the speed at a cross section	121
A.3.4	Moving bottleneck	122
A.3.5	Multi-lane traffic flow	123
A.4	Problem set 4	124
A.4.1	Short questions	124
A.4.2	From car-following to a fundamental diagram	124
A.4.3	MOBIL lane change model	124
A.4.4	Snow plow	125
A.4.5	Cumulative curves	126
A.4.6	Crown jewels in the tower	127
A.5	Problem set 5	128
A.5.1	Short questions	128
A.5.2	Motorway traffic operations	130
A.5.3	Car-following	131
A.5.4	Partial road blocking near a signalised intersection	131
A.5.5	Network Fundamental Diagram	132
A.6	Problem set 6	133
A.6.1	Short questions	133
A.6.2	Bridge opening	134
A.6.3	Variable road layout	134
A.6.4	Traffic stability	137
A.6.5	Levels of description	137
A.7	Problem set 7	137
A.7.1	Short open questions	137
A.7.2	Cumulative curves	138
A.7.3	Macroscopic traffic variables in case of different vehicle classes	140
A.7.4	Slow truck on the motorway	141
A.8	Problem set 8	141

A.8.1	Short open questions	141
A.8.2	Microscopic effects on the fundamental diagram	142
A.8.3	Prediction of downstream conditions	142
A.8.4	Demonstration of police cars	143
A.8.5	Stairs for cyclists at Delft train station	144
A.9	Problem set 9	144
A.9.1	Short questions	144
A.9.2	Car-following in fog	145
A.9.3	Cleaning the road	146
A.9.4	Mobil lane changing model	146
A.9.5	Pedestrians at a traffic light	147
A.9.6	Hysteresis	148
A.10	Problem set 9	148
A.10.1	Short questions	148
A.10.2	Traffic flow properties	149
A.10.3	Speeds	149
A.10.4	Analyse a car-following model	149
A.10.5	Traffic light	150
A.10.6	Macroscopic Fundamental Diagram	150
A.10.7	Non-vehicular traffic	151
B	Solutions to test questions	153
C	Matlab code for creating (slanted) cumulative curves	191

Chapter 1

Variables

This chapter describes the main variables which are used in traffic flow theory. Section 1.1 will show the different levels (microscopic, macroscopic and other levels) at which traffic is generally described. Section 1.2 will describe different principles (local, instantaneous and spatio-temporal) to measure the traffic flow. The last section (1.3) describes traffic flow characteristics.

1.1 Levels of description

This section will show the different levels at which traffic is generally described. Sections 1.1.1 and 1.1.2 will discuss the variables in the microscopic and macroscopic descriptions in more detail.

In a microscopic traffic description, every vehicle-driver combination is described. The smallest element in the description is the vehicle-driver combination. The other often used level of traffic flow description is the macroscopic traffic description. Different from the microscopic description, this level does not consider individual vehicles. Instead, the traffic variables are aggregated over several vehicles or, most commonly, a road stretch. Typical characteristics of the traffic flow on a road stretch are the average speed, vehicle density or flow (see section 1.1.2). Other levels of description can also be used, these are described in the last section (see section 1.1.3).

1.1.1 Microscopic

In a microscopic traffic description, the vehicle-driver combinations (often referred to as “vehicles”, which we will do from now on) are described individually. Full information of a vehicle is given in its trajectory, i.e. the specification of the position of the vehicle at all times. To have full information on these, the positions of all vehicles at all times have to be specified. A graphical representation of vehicle trajectories is given in figure 1.1

The trajectories are drawn in a space time plot, with time on the horizontal axis. Note that vehicle trajectories can never go back in time. Trajectories might move back in space if the vehicles are going in the opposite direction, for instance on a two-lane bidirectional rural road. This is not expected on motorways. The slope of the line is the speed of the vehicles. Therefore, the trajectories cannot be vertical – that would mean an infinite speed. Horizontal trajectories are possible at speed zero.

Basic variables in the microscopic representation are speed, headway, and space headway. The speed is the amount of distance a vehicle covers in a unit of time, which is indicated by v . Sometimes, the inverse of speed is a useful measure, the amount of time a vehicle needs for to cover a unit of space; this is called the pace p . Furthermore, there is the space headway or spacing (s) of the vehicle. The net space headway is the distance between the vehicle and its leader. This is also called the gap. The gross space headway of a (following) vehicle the distance *including* the length of the vehicle, so the distance from the rear bumper of the leading vehicle to the rear bumper of the following vehicle. Similarly, we can time it takes for a follower to get to reach (with its front bumper) the position of its leader’s rear bumper. This is called the net time headway. If we also add the time it cost to cover the distance of a vehicle length, we get the gross time headway. See also figure 1.2. The symbol used to indicate the headway is h .

From now on, in this reader we will use the following conventions:

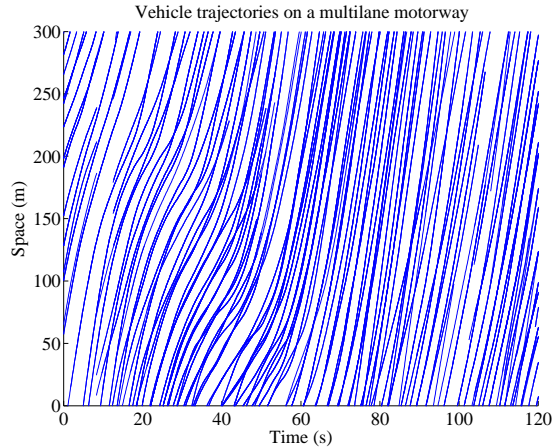


Figure 1.1: Vehicle trajectories on a multilane motorway

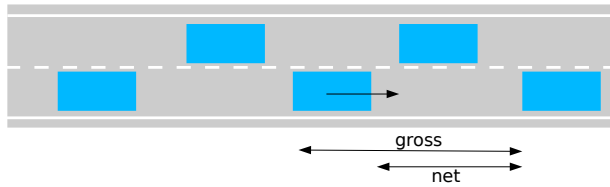


Figure 1.2: The difference between gross and net spacing (or headway)

- Unless specified otherwise, headway means time headway
- Unless specified otherwise, headways and spacing are given as gross values

Figure 1.3 shows the variables graphically. The figure shows two vehicles, a longer vehicle and a shorter vehicle. Note that the length of the vehicles remains unchanged, so the difference between the gross and net spacing is the same, namely the vehicle length. However, the difference between the gross and net time headway changes based on the vehicle speed.

In a trajectory plot, the slope of the line is the speed. If this slope changes, the vehicle accelerates or decelerates. So, the curvature of the lines in a trajectory plot shows the acceleration or deceleration of the vehicle. If the slope increases, the vehicle accelerates, if it decreases, it decelerates.

1.1.2 Marcoscopic

In a macroscopic traffic description, one does not describe individual vehicles. Rather, one describes for each road section the aggregated variables. That is, one can specify the density k , i.e. how close in space vehicles are together. Furthermore, one can specify the flow q i.e. The number of vehicles passing a reference point per unit of time. Finally, one can describe the average speed u of the vehicles on a road section. Other words for flow are throughput, volume or intensity; we will strictly adhere to the term flow to indicate this concept.

All of the mentioned macroscopic variables have their microscopic counterpart. This is summarized in table 1.1. The density is calculated as one divided by the average spacing, and is calculated over a certain road stretch. For instance, if vehicles have a spacing of 100 meters, there are $1/100$ vehicles per meter, or $1000/100=10$ veh/km. The flow is the number of vehicles that pass a point per unit of time. It can be directly calculated from the headways by dividing one over the average headway. For instance, if all vehicles have a headway of 4 seconds, there are $1/4$ vehicles per second. That means there are $3600(s/h)/4(s/veh)= 900$ veh/h. In table 1.1 units are provided and in the conversion from one quantity to the other, one needs to pay attention. Note that provided units are not obligatory:

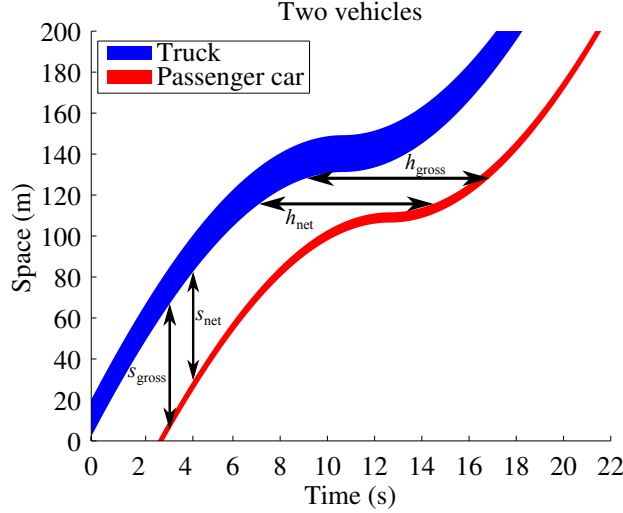


Figure 1.3: The microscopic variables explained based on two vehicles

Table 1.1: Overview of the microscopic and macroscopic variables and their relationship; the pointy brackets indicate the mean.

Microscopic	symbol	unit	Macroscopic	symbol	unit	relation
Headway	h	s	Flow	q	vtg/h	$q = \frac{3600}{\langle h \rangle}$
Spacing	s	m	Density	k	vtg/km	$k = \frac{1000}{\langle s \rangle}$
Speed	v	m/s	Average speed	u	km/u	$u = 3.6 \langle v \rangle$

one can present individual speed in km/h, or density in veh/hm. However, always pay attention to the units before converting or calculating.

Relation to the microscopic level

The average speed is calculated as an average of the speeds of vehicles at a certain road stretch. This speed differs from the average speed obtained by averaging speed of all vehicles passing a certain point. The next section explains the different measuring principles. The full explanation of the differences between the two speeds and how one can approximate the (space) average speed by speeds of vehicles passing a certain location is presented in section 4.4.

Another concept for a traffic flow, in particular in relation to a detector (see also section 1.2), is the occupancy o . This indicates which fraction of a time a detector embedded in the roadway is occupied, i.e. whether there is a vehicle on top of the detector. Suppose a detector has a length L_{det} and a vehicle a length of L_i . The occupancy is defined as the time the detector is occupied, τ_{occupied} divided by all time, i.e. the time it is occupied and time it is not occupied

$$o = \frac{\tau_{\text{occupied}}}{\tau_{\text{occupied}} + \tau_{\text{not occupied}}} \quad (1.1)$$

The occupation time can be derived from the distances and the speed. The distance the vehicle has to cover from the moment it starts occupying the detector up to the time it leaves the detector is its own length plus the length of the detector. Hence, the occupancy time is

$$\tau_{\text{occupied}} = \frac{L_i + L_{\text{det}}}{v} \quad (1.2)$$

Once the first vehicle drives off the detector, the distance for the following vehicle to reach the detector is the gap (i.e., the spacing minus the length of the vehicle) between the vehicles minus the length of the detector. The amount of time

this takes is

$$\tau_{\text{not occupied}} = \frac{s - L_i - L_{\text{det}}}{v} \quad (1.3)$$

Substituting the expressions for the occupancy time and the non-occupancy time into equation 1.1 and rearranging the terms, we get

$$O = \frac{L_i + L_{\text{det}}}{s} \quad (1.4)$$

In practice, the detector length is known for a certain road configuration (usually, there are country specific standards). So assuming a vehicle length, one can calculate the spacing, and hence the density, from the occupancy.

1.1.3 Other levels

Apart from the macroscopic and microscopic traffic descriptions, there are three other levels to describe traffic. They are less common, and are therefore not discussed in detail. The levels mentioned here are mainly used in computer simulation models.

Mesoscopic

The term mesoscopic is used for any description of traffic flow which is in-between macroscopic and microscopic. It can also be a term for simulation models which calculate some elements macroscopically and some microscopically. For instance, dynasmart Dynasmart (2003), uses such a mesoscopic description.

Submicroscopic

In a submicroscopic description the total system state is determined by the sub levels of a vehicle and/or driver. Processes which influence the speed of a vehicle, like for instance mechanically throttle position and engine response, or psychologically speed perception, are explicitly modelled. This allows to explicitly model the (change in) reaction on inputs. For instance, what influence would cars with a stronger engine have on the traffic flow.

Network level

A relatively new way of describing the traffic state is the network level. This has recently gained attention after the publication by Geroliminis and Daganzo (2008). Instead of describing a part of a road as smallest element, one can take an area (e.g. a city center) and consider this as one unit. Chapter 11 is devoted to this description.

1.2 Measuring principles

Whereas the previous sections described which variables are used to describe traffic flow, this section will introduce three principles of measuring the traffic flow. These principles are local, instantaneous and spatio-temporal.

1.2.1 Local

With local measurements one observes traffic at one location. This can be for instance a position at the roadway. To measure motorway traffic, often inductive loops are used. These are coils embedded in the pavement in which a electrical current produces a (vertical) magnetic field. If a car enters or leaves this magnetic field, this can be measured in the current of the coil. Thus, one knows how long a loop is occupied. In the US, usually single loops are used, giving the occupancy of the loop. Using equation 1.4, this can be translated into density. The detectors also measure the flow. As will be explained later in section 4.1, this suffices to completely characterise the traffic flow.

This determination of density builds upon the assumption of the vehicle length being known. One can also measure the length of a vehicle for passing vehicles, using dual loop detectors. These are inductive loops which are placed a known short distance (order of 1 m) from each other. If one measures carefully the time between the moment the vehicle starts occupying the first loop and the moment it starts occupying the second loop, one can measure its speed. If its speed is known, as well as the time it occupies one loop, the length of the vehicle can also be determined.

1.2.2 Instantaneous

Contrary to local measurements, there are instantaneous measurements. These are measurements which are taken at one moment in time, most likely over a certain road stretch. An example of such a measurement is an areal photograph. In such a measurement, one can clearly distinguish spatial characteristics, as for instance the density. However, measuring the temporal component (flow) is not possible.

1.2.3 spatio-temporal measurements

Apart from local or instantaneous measurements, one can use measurements which stretch over a period of time *and* a stretch of road. For instance, the trajectories in figure 1.1 are an example thereof. This section will introduce Edie's definitions of flow, density and speed for an area in space and time.

A combination of instantaneous measurements and local measurements can be found in remote sensing observations. These are observations which stretch in both space and time. For instance, the trajectories presented in figure 1.1 can be observed using a camera mounted on a high point or a helicopter. One can see a road stretch, and observe it for a period of time.

Measuring average speed by definition requires an observation which stretches over time and space. At one location, one cannot determine speed, nor at one moment. One needs at least two locations close by (several meters) or two time instances close by. Ignoring these short distances one can calculate a local mean speed based on speeds of the vehicles passing by location. Ignoring the short times, one can calculate the time mean speed from the speed of the vehicles currently at the road. At this moment, we suffice by mentioning these average speeds are different. Section 4.4 will show how the space mean speed can be approximated from local measurements.

Figure 1.4 shows the same trajectories as figure 1.1, but in figure 1.4 an area is selected. Trajectories within this area in space and time are coloured red. Note that an selected area is not necessarily square. It is even possible to have a convex area, or boundaries moving backwards and forwards in time. The definitions as introduced here will hold for all types of areas, regardless of their shape in space-time.

Let us consider the area X . We indicate its size by W_X , which is expressed in km-h, or any other unit of space times time. For all vehicles, we consider the distance they drive in area X , which we call $d_{X,i}$. Adding these for all vehicles i gives the total distance covered in area X , indicated by TD :

$$TD = \sum_{\text{all vehicles } i} d_{X,i} \quad (1.5)$$

For a rectangular area in space and time, the distance covered might be the distance from the upstream end to the downstream end, but the trajectory can also begin and/or end at the side of the area, at a certain time. In that case, the distance is less than the full distance.

Similarly, we can define the time a vehicle spends in area X , $t_{X,i}$, which we can sum for all vehicles i to get the total time spent in area X , indicated by TT .

$$TT = \sum_{\text{all vehicles } i} t_{X,i} \quad (1.6)$$

Obviously, both quantities grow in principle with the area size. Therefore, the traffic flow is best characterised by the quantities TD/W_X and TT/W_X . This gives the flow and the density respectively:

$$q = \frac{TD}{W_X} \quad (1.7)$$

$$k = \frac{TT}{W_X} \quad (1.8)$$

Intuitively, the relationship is best understood reasoning from the known relations of density and flow. Starting with a situation of 1000 veh/h at a cross section, and an area of 1 h and 2 km. In 1 hour, 1000 vehicles pass by, which all travel 2 kilometres in the area (There the vehicles which cannot cover the 2 km because the time runs out, but there are just as many which are in the section when the time window starts). So the total distance is the flow times the size of the area: $TD = qW_X$. This can be simply rewritten to equation 1.8.

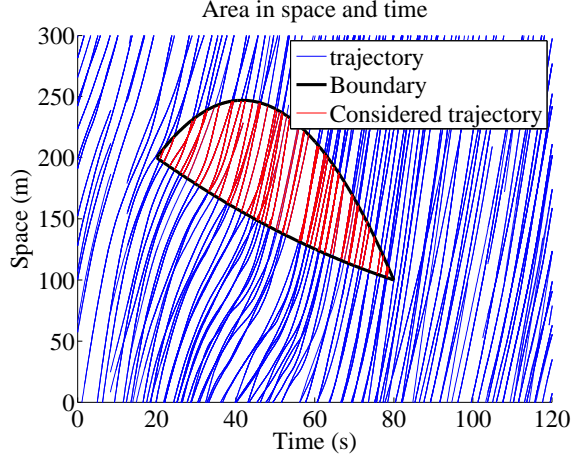


Figure 1.4: Vehicle trajectories and the selection of an area in space and time

A similar relation is constructed for the density, considering again the rectangular area of 1 hour times 2 kilometres. Starting with a density of 10 veh/km, there are 20 vehicles in the area, which we all follow for one hour. The total time spent, is hence $10 \times 2 \times 1$, or $TT = kW_X$. This can be rewritten to equation 1.8.

The average speed is defined as the total distance divided by the total time, so

$$u = \frac{TD}{TT} \quad (1.9)$$

The average travel time over a distance l can be found as the average of the time a vehicle travels over a distance l . In an equation, we find:

$$\langle tt \rangle = \left\langle \frac{l}{v} \right\rangle = l \left\langle \frac{1}{v} \right\rangle \quad (1.10)$$

In this equation, tt indicates the travel time and the pointy brackets indicate the mean. This can be measured for all vehicles passing a road stretch, for instance at a local detector. Note that the mean travel time is *not* equal to the distance divided by the mean speed:

$$\langle tt \rangle = l \left\langle \frac{1}{v} \right\rangle \neq l \frac{1}{\langle v \rangle} \quad (1.11)$$

In fact, it can be proven that in case speeds of vehicles are not the same, the average travel time is underestimated if the mean speed is used.

$$\langle tt \rangle = l \left\langle \frac{1}{v} \right\rangle \leq l \frac{1}{\langle v \rangle} \quad (1.12)$$

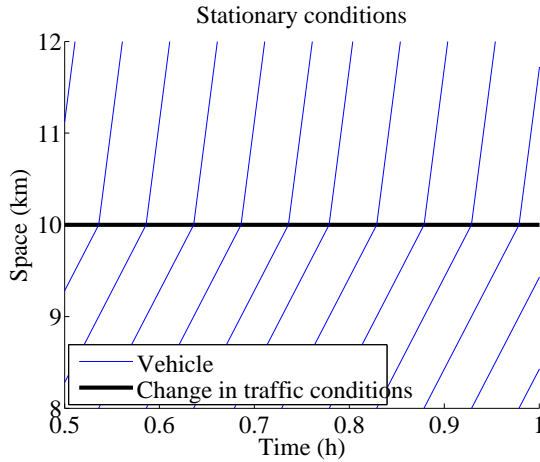
The harmonically averaged speed (i.e., 1 divide by the average of 1 divided by the speed) does provide a good basis for the travel time estimation. In an equation, we best first define the pace, p_i :

$$p_i = \frac{1}{v_i} \quad (1.13)$$

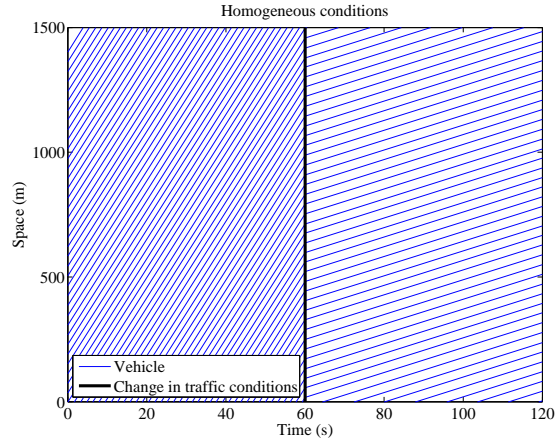
The harmonically averaged speed now is

$$\langle v \rangle_{\text{harmonically}} = \frac{1}{\langle p \rangle} = \frac{1}{\left\langle \frac{1}{v_i} \right\rangle} \quad (1.14)$$

The same quantity is required to find the space mean speed. Section 4.4 shows the difference qualitatively. In short, differences can be several tens of percents.



(a) Stationary conditions



(b) Homogeneous conditions

1.3 Stationarity and homogeneity

Traffic characteristics can vary over time and/or over space. There are dedicated names for traffic if the state does not change.

Traffic is called stationary if the traffic flow does not change over time (but it can change over space). An example can be for instance two different road sections with different characteristics. An example is given in figure 1.5(a), where there first is a low speed, then the speed of the vehicles is high.

Traffic is called homogeneous if the traffic flow does not change over space (but it can change over time). An example is given in figure 1.5(b), where at time 60 the speed decreases at the whole road section. This is much less common than the stationary conditions. For this conditions to occur, externally the traffic regulations have to change. For instance, the speed limits might change at a certain moment in time (lower speeds at night).

Selected problems

For this chapter, consider problems: 5, 6, 162, 172, 173, 174, 175, 197, 218, 233, A.10.3

Chapter 2

Headway models

This section discusses headway models. In this chapter, the headway is always the time headway.

2.1 Relation between headway and capacity

The headway distribution describe which headways can be observed with which probability. One might argue that this is related to the flow, since the average headway is the flow. The flow is determined by the demand. However, in the bottleneck the flow is determined by the minimum headway at which drivers follow each other. Or in other words, the headway distribution determines the capacity in the bottleneck. Suppose the headway distribution is given by $P(h)$. Then, the average headway can be determined by

$$\langle h \rangle = \int_0^{\inf} h P(h) dh \quad (2.1)$$

This is a mathematical way to describe the average headway once the distribution is given. The flow in the active bottleneck, hence the capacity is inverse of the mean headway, see table 1.1:

$$C = 1 / \langle h_{\text{bottleneck}} \rangle \quad (2.2)$$

The number of vehicles arriving in a certain period could be a useful measure. This holds for instance for traffic lights, where the number of arrivals per red period is relevant. As illustrated in figure 2.1, there could be different lanes for different directions at a traffic light. The idea is that the traffic towards one direction will not block the traffic to other directions, hence, the length should be long enough to allow the number of vehicles in the red period. The average number of vehicles in a red period can be determined from the flow. However, mostly requirements are that in p% of the red times (under a constant demand) the queue should not exceed the dedicated lane. In that case, the headway distribution can form the basis for the calculations.

2.2 Arrivals per interval

This section describes the number of arrivals per time interval. For different conditions, this distribution is different. Table 2.2 gives an overview of the distributions described in this section, and gives some characteristics. One should

Table 2.1: The different processes and the underlying assumptions

Headway dist	Process characteristic	Dist of nr of arrivals per interval
Exponential $\text{mean}(h)=\text{std}(h)$	Independent arrivals	Poisson
	Correlated arrivals	Binomial
	Negatively correlated arrivals	Negative binomial

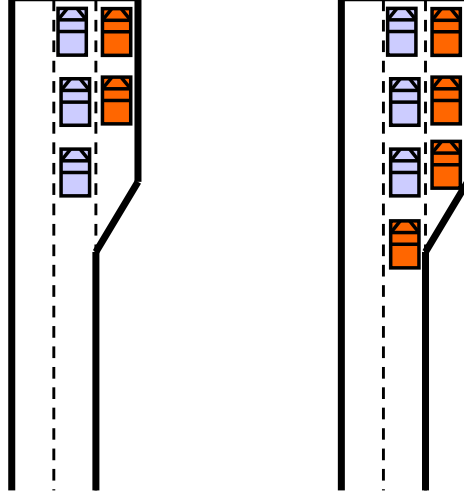


Figure 2.1: A queuing area. The orange coloured vehicles turn right, whereas the blue ones continue straight

Table 2.2: Overview of the means and variances of the different distributions. In this table, q is the flow in the observation period, p is the probability of including the observation in the period.

Distribution	Mean	Variance
Poisson	q	$q = \text{mean}$
Binomial	np	$np(1 - p) < \text{mean}$
Negative binomial	$n(1p)/p$	$n(1p)/p^2 > \text{mean}$

differentiate between the probability of number of arrivals (a macroscopic characteristic, based on aggregating over a certain duration of time), described in this section, and the probability of a headway (a microscopic characteristic).

2.2.1 Poisson

The first distribution function described here is the Poisson distribution. One will observe this distribution function once the arrivals are independent (see also section 2.3.1). The resulting probability is described by a so-called Poisson distribution function. Mathematically, this function is described by:

$$P(X = k) = \frac{q^k}{k!} e^{-q}. \quad (2.3)$$

This equation gives the probability that k vehicles arrive if the average arrival rate *per period* is q . Hence note that one needs to rescale q to units of number of vehicles per aggregation period!

Figure 2.2 shows examples of the Poisson distribution. Note that for low values of the flow (expected value smaller than 1), the probability is decreasing. If the flow is higher, there is a maximum at the number of arrivals which is at a higher value than 1.

Figure 2.3 shows the best fits of this distribution on real life data. This distribution is accurate if the flow is low, and is not so good if the flow increases. This is because once the flow is low, the assumption of independent arrivals does not hold any more. Once vehicles are bound by the minimum headway, the arrivals are not independent any more. This restriction come more into play once the flow is high.

2.2.2 Binomial

The binomial distribution can be used if there are correlations between the arrivals. For instance on busy roads, one can expect that more vehicles drive at a minimum headway. Whereas in case of the Poisson distribution, the variance

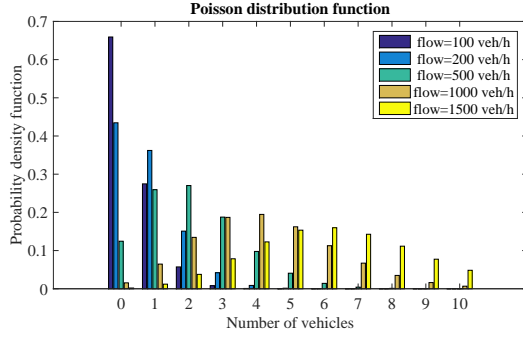


Figure 2.2: Example of the Poisson distribution for different flow values; the flow is indicated in veh/h, and these are the probabilities for arrivals in 15 seconds

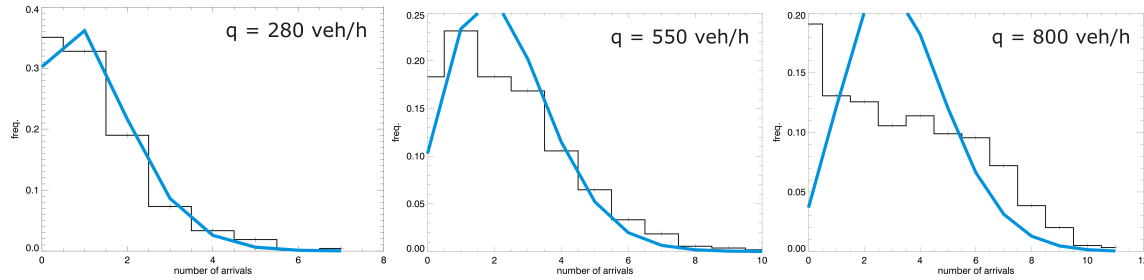


Figure 2.3: Illustration of the number of arrivals from real world data

of the distribution was equal to the mean, in this case the variance is smaller (since more drivers drive at a certain headway). The mathematical equation describing the function is:

$$P(X = k) = \binom{n}{k} p^k (1 - p)^{n-k} \quad (2.4)$$

The idea behind the distribution is that one does n tries, each with an independent success rate of p . The number of successes is k . The mean of the distribution is np , see table 2.2. A certain flow specifies the mean of the arrivals, which hence determines np . This gives a freedom to choose n or p , by which one can match the spread of the function. The number of observations in the distribution can never exceed n , so an reasonable choice of n would be the interval time divided by the minimum headway. Figure 2.4 shows examples of the binomial distribution function.

Note that the variance of the binomial function is smaller than the Poisson distribution for the same flow. This can

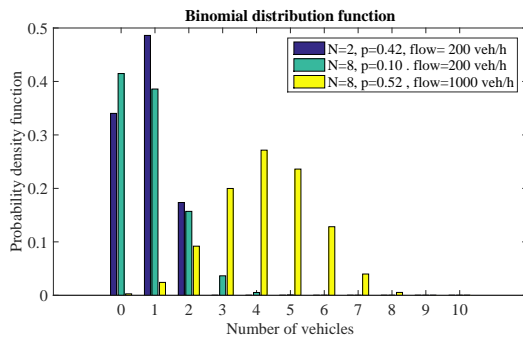


Figure 2.4: Examples of the binomial distribution function for the number of arrivals in an aggregation period

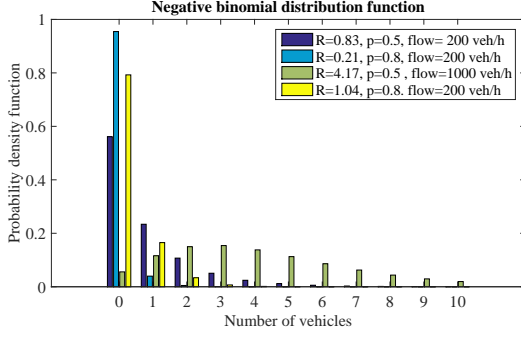


Figure 2.5: Example of the negative binomial function for the number of arrivals in an aggregation period

be a reason to choose this function.

2.2.3 Negative binomial

The negative binomial distribution can be used if there are negative correlations between the arrivals. In traffic this happens for instance downstream of a signalised intersection. If one observes several vehicles at a short headway, one gets a larger probability that next headway will be large because the traffic light will switch to red.

The probability distribution function for the number of observed vehicles in an aggregation interval is:

$$P(X = k) = \binom{k + r - 1}{k} p^k (1 - p)^r \quad (2.5)$$

This distribution describes when one observes individual and independent process with a success rate of p . One observes so until r failures are observed. X is the stochastic indicating how many successes are observed.

Figure 2.5 shows the value of this function for different parameter sets. Note that the variance (and hence standard deviation) be set independently from the mean, like in the binomial distribution function. for this distribution (see table 2.2), the mean is given by $n(1p)/p$, and the variance is given by $n(1p)/p^2$, which is the mean divided by p . Since p is a probability and has a value between 0 and 1, we can derive that the variance is larger than the mean. A larger variance is what one would intuitively expect downstream of a signalised intersection. This characteristic can be used to have an idea of the distribution to use.

2.3 Headway distributions

In this section the exponential headway distribution is described, used with independent arrivals, and composite headway models.

2.3.1 Exponential

The first distribution is the exponential distribution, shown in figure 2.6. This is defined by:

$$P(h|q) = q \exp -qh \quad (2.6)$$

Note that this equation has a *single* parameter, being the flow q . That is the inverse of the average headway. The underlying assumption of this distribution is that all drivers can choose their moment of arrival independently. Consider that each (infinitesimal small) time step a driver considers to leave with a fixed probability. One then gets a exponential distribution function for the headway.

This is a very good assumption on quiet roads, when there are no interactions between the vehicles. The interactions occur once vehicles are limited in choosing their headway, mostly indicated by the minimum headway. An illustration how this works out for a real life case is shown in figure 2.3 for the number of arrivals (see section 2.2).

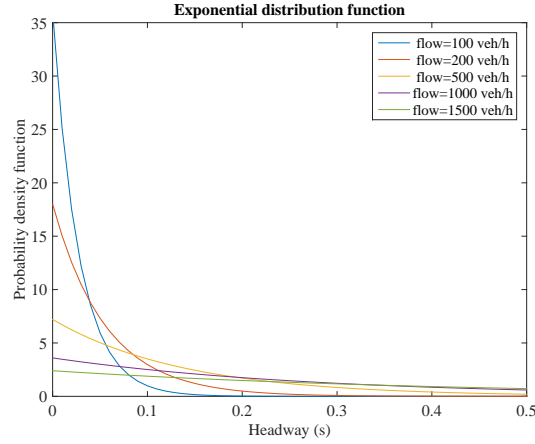


Figure 2.6: The probability density function for headways according to the exponential distribution for different flow values

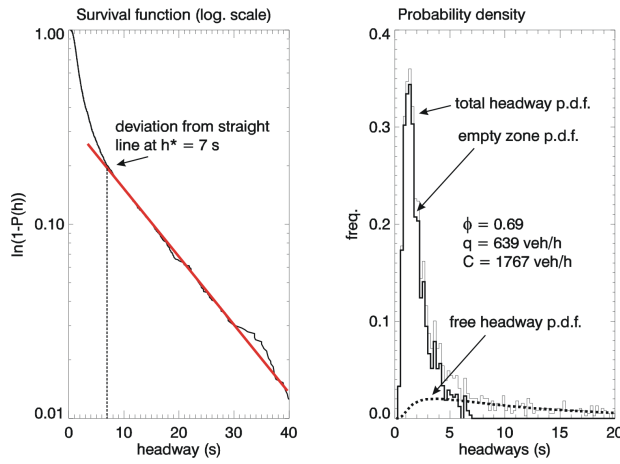


Figure 2.7: Example of the composite headway distribution and its estimation for real life data

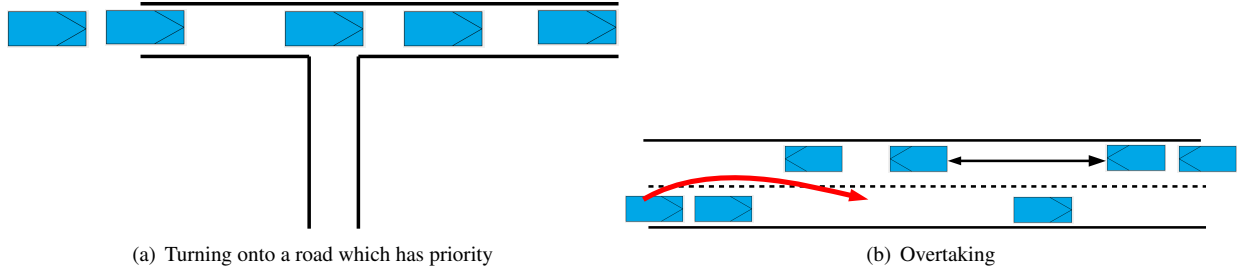
The only good way to test whether the exponential data describes the data one observes is to do a proper statistical test (e.g., a Kolmogorov-Smirnov test). There are also rules of thumb. A characteristic for this distribution is that the standard deviation is equal to the mean. If one has data of which one thinks the arrivals are independent and this criterion is satisfied, the arrivals are very likely to be exponentially distributed.

This distribution function for the headways matches the Poisson distribution function for the number of arrivals.

2.3.2 Composite headway models

Whereas the exponential distribution function works well for low flows, for higher flows the distribution function is not very good. For these situations, so called composite headway distributions are being used (see for more information Hoogendoorn (2005)). The basic idea is that a fraction of the traffic Φ is driving freely following a headway distribution function $P_{\text{free}}(h)$. The other fraction of the traffic $1 - \Phi$ is driving constraint, i.e., is following their leader, and have a headway distribution function $P_{\text{constraint}}(h)$.

In a composite headway distribution, these two distribution functions are combined. The combined distribution



function can hence be expressed as

$$P(h) = \Phi P_{\text{free}}(h) + (1 - \Phi) P_{\text{constraint}}(h) \quad (2.7)$$

Given the reasoning in section 2.3.1, it would make sense to choose an exponential distribution function for the free headways.

A plot of the headway distribution function (in fact, a survival function of the headway, i.e. 1- the cumulative distribution function) is shown in figure 2.7. The vertical axis is a logarithmic axis. Note that in these axis the exponential distribution function is a straight line. That is what is observed for the large headways. For the smaller headways (in the figure, for less then 7 seconds) this does not longer hold. This is due to the limitation of following distance. As the figure shows, this can be determined graphically.

2.4 Critical gap

The critical gap is the smallest gap (time gap) that a vehicle accepts to go into. Some examples are given in section 2.4.1. The relation with the inflow capacity is discussed in section 2.4.2.

2.4.1 Situations

Examples of situations where the critical gap is relevant, are turning onto a road where one has to give priority, overtaking, merging into the traffic stream or lane changing. Some of them are shown in figure 2.4.1.

The critical gap is defined in the flow. Note that the critical gap differs per person, as well as per situation. One might have a small critical gap to merge into a traffic stream moving at slow speed.

For overtaking, the critical gap (measured in headway in the opposite traffic stream) needs to be larger because the traffic is moving in the opposite direction. For instance, if a driver spends 3 seconds on lane of the opposing traffic for an overtaking manoeuvre, during that time the opposing vehicles also move in the direction of the overtaking vehicle. To find the critical (time) gap, one needs to consider the distance the overtaker uses at the other lane (overtaking time times speed) – this is the space the overtaker would need if the opposing vehicles were stationary. To this, one should *add* the distance the opposing traffic moves in the overtaking time (overtaking time times the speed of the opposing vehicles). This combined distance gap (plus arguably a safety margin) can be translated into a time gap. Since one measures the gap as headway in the opposing traffic, one needs to divide the required space gap by the speed of the opposing traffic.

2.4.2 Inflow capacity

Consider the situation as in figure 2.8(a). Consider that the main line traffic (traffic from left to right) has a headway distribution of $P(h)$, and there is an infinite line of vehicles waiting to enter the road, all with an critical gap gc . One can calculate how many vehicles can enter the road per unit of time, as will be shown below.

We know that for certain gaps, vehicles can enter. The first step is to find the number of gaps which pass per unit of time. That equals the number of vehicles (each vehicle causes one new gap). The number of vehicles per unit of time is the flow, which is the inverse of the mean of the headway, which in turn can be calculated from the headway distribution.

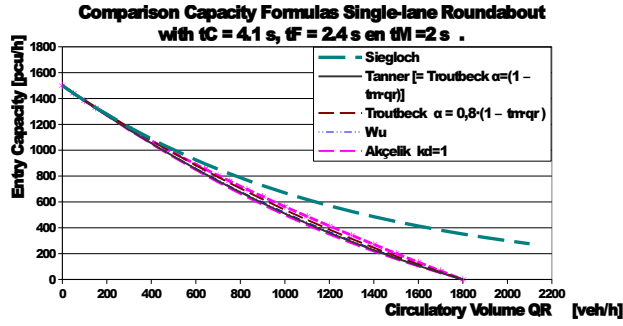


Figure 2.8: The inflow onto a road (or roundabout) as function of the main road (roundabout) traffic – figure from Fortuijn and P. (2015)

Then, for all headways larger than the critical gap, but smaller than twice the critical gap one vehicle can enter. The frequency that this happens is the flow (=gap rate) times the probability that the gap is this size, determined from integrating the probability density function of the headway over the right headways:

$$q_{in1 \text{ vehicle}} = q \int_g c^{2gc} P(h) dh \quad (2.8)$$

The probability that in one gap two vehicles can enter is the integral of the probability density function for the headways from twice the critical gap to three times the critical gap. The rate at which gaps these gaps occur is the flow q , so the rate at which these gaps occur is $q \int_{2gc}^{3gc} P(h) dh$. Per gap, two vehicles enter, so the matching inflow is

$$q_{in2 \text{ vehicles}} = 2q \int_{2gc}^{3gc} P(h) dh \quad (2.9)$$

One can continue this reasoning and find an equation for the inflow:

$$q_{in total} = \sum_n (q_{in n \text{ vehicles}}) = \sum_n nq \int_{ngc}^{(n+1)gc} P(h) dh \quad (2.10)$$

This can numerically be evaluated.

Typically, one would expect the headway in the order of twice the minimum headway. Namely, after merging, one would like to have at least a minimum headway upstream (lag gap) and a minimum headway downstream (lead gap).

In the calculation of the maximum inflow, the headway distribution function plays an important role. As extreme example, suppose that all headways are equal at 99% of the critical gap. Then, the flow is at about half the capacity of the road, but the inflow is 0. For different distribution functions it can be calculated what is the maximum inflow on the main road. This is shown in figure 2.8 for different functions. It shows that the inflow capacity decreases with the main road flow. However, the precise type of distribution matters less: the graphs for the different distribution functions are quite similar.

Selected problems

For this chapter, consider problems: 38, 39, 40, 160, 187, 188, 232, 240

Chapter 3

Cumulative curves

This chapter discusses cumulative curves, also known as cumulative flow curves. The chapter first defines the cumulative curves (section 3.1), then it is show how traffic characteristics can be derived from these (section 3.2). Section 3.4 shows the application of slanted cumulative curves.

3.1 Defenition

The function $N_x(t)$ is defined as the number of vehicles that have passed a point x at time t and is only used for traffic into one direction. Hence, this function only increases over time. Strictly speaking, this function is a step function increasing by one every time a vehicle passes. However, for larger time spans and higher flow rates, the function is often smoothed into a continuous differentiable function.

The increase rate of this function equals the flow:

$$\frac{dN}{dt} = q \quad (3.1)$$

Hence from the flow, we can construct the cumulative curve:

$$N = \int q dt \quad (3.2)$$

This gives one degree of freedom, the value to start at. This can be chosen freely, or should be adapted to cumulative curves for other locations.

3.2 Vertical queuing model

A vertical queuing model is a model which assumes an unlimited inflow and an outflow which is restricted to capacity. The vehicles which cannot pass the bottleneck are stacked “vertically” and do not occupy any space. Figure 3.1 illustrates this principle.

Let us now study the dynamics of such a queue. We discretize time in steps of duration Δt , referred to by index t . The demand is externally given, and indicated by D . At time steps t we compute the flow into and out of the stack (the number of vehicles in the stack indicated as S). In between the time steps, indicated here as $t + 1/2$, the number of vehicles in the stack is updated based on the flows q . Then, the stack provide the basis for the flows in the next time step.

The stack starts at zero. Then, for each time step first the inflow to the stack is computed.

$$q_{in,t} = D \quad (3.3)$$

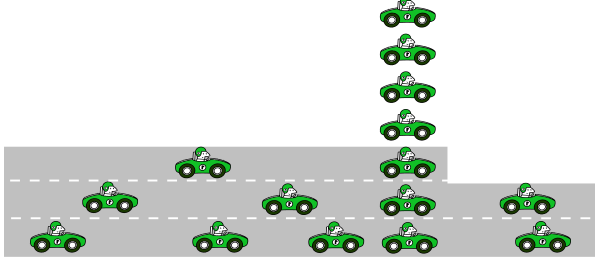


Figure 3.1: Illustration of a vertical queue

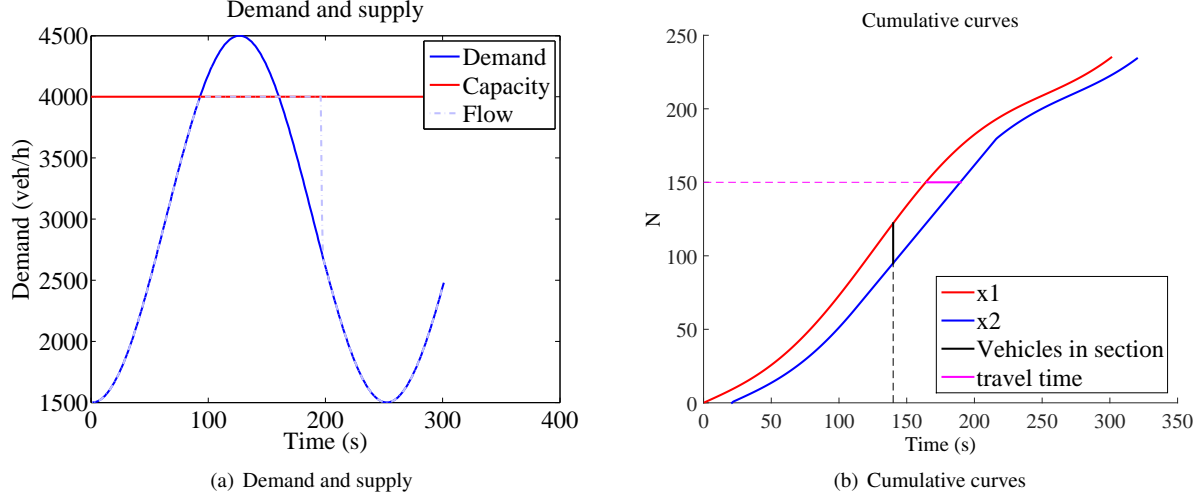


Figure 3.2: Demand and cumulative curves

and the stack is updated accordingly, going to an intermediate state at time step $t+1/2$. This intermediate step is the number of vehicles in the queue if there were no outflow, so the original queue plus the inflow:

$$S_{t+1/2} = S_t + q_{in}\Delta t \quad (3.4)$$

Then, the outflow out of the stack (q_{out}) is the minimum of the number of vehicles in this intermediate queue and the maximum outflow determined by the capacity C :

$$q_{out} = \min\{C\Delta t, S_{t+1/2}\} \quad (3.5)$$

The stack after the time step is then computed as follows

$$S_{i+1} = S_{i+1/2} - q_{out}\Delta t = S_i + (q_{in,i} - q_{out,i})\Delta t \quad (3.6)$$

Let us consider a situation as depicted in figure 3.1, and we are interested in the delays due to the bottleneck with a constant capacity of 4000 veh/h. The demand curve is plotted in figure 3.2(a). The flows are determined using the vertical queuing model. The flows are also shown in figure 3.2(a). Note that the area between the flow and demand curve where the demand is higher than the flow (between approximately 90 to 160 seconds), is the same as the area between the curves where the flow is higher than the demand (between approximately 160 and 200 seconds). The reasoning is that the area represents a number of vehicles (a flow times a time). From 90 to 160 seconds the demand is higher than the flow, i.e., the inflow is higher than the outflow. The area represents the number of vehicles that cannot pass the bottleneck, and hence the number of queued vehicles. From 160 seconds, the outflow of the queue is larger than the inflow. That area represents the number of vehicles that has left the queue, and cannot be larger than the number of vehicles queued. Moreover, the flows remain at capacity until the stack is empty, so both areas must be equal.

3.3 Travel times, densities and delays

This section explains how travel times and delays can be computed using cumulative curves. Note that this methodology does not take spillback effects into account. If one requires this to be accounted for, please refer to shockwave theory (chapter 5).

3.3.1 Construction of cumulative curves

The cumulative curves for the above situation is shown in figure 3.2(b). The curves show the flows as determined by the vertical queuing model. The for the inflow we hence use equation 3.3 and for the outflow we use 3.5; for both, the cumulative curves are constructed using equation 3.2.

3.3.2 Travel times, number of vehicles in the section

A black line is drawn at $t = 140s$ in figure 3.2(b). The figure shows by intersection of this line with the graphs how many vehicles have passed the upstream point x_1 and how many vehicles have passed the downstream point x_2 . Consequently, it can be determined how many vehicles are in the section between x_1 and x_2 . This number can also be found in the graph, by taking the difference between the inflow and the outflow at that moment. This is indicated in the graph by the bold vertical black line.

Similarly, we can take a horizontal line; consider for instance the line at $N = 150$. The intersection with the inflow line shows when the 150th vehicle enters the section, and the intersection with the outflow line shows when this vehicle leaves the section. So, the horizontal distance between the two lines is the travel time of the 150th vehicle. At times where the demand is lower than the capacity, the vehicles have a free flow travel time. So without congestion, the outflow curve is the inflow curve which is translated to the right by the free flow travel time.

The vertical distance is the number of vehicles in the section (ΔN) at a moment t . In a time period dt this adds $\Delta N dt$ to the total travel time (each vehicle contributes dt). To get the total travel time, we integrate over all infinitesimal intervals dt :

$$tt = \int \Delta N dt \quad (3.7)$$

The horizontal distance between the two lines is the travel time for one vehicle, and vertically we find the number of vehicles. Adding up the travel times for all vehicles gives the total travel time:

$$tt = \sum_i tt_i \quad (3.8)$$

In a continuous approach, this changes into

$$tt = \int tt_i di \quad (3.9)$$

Both calculation methods lead to the same interpretation: *the total time spent can be determined by the area between the inflow and outflow curve.*

3.3.3 Delays

Delays for a vehicle are the extra time it needs compared to the free flow travel time. so to calculate delay, one subtracts the free flow travel time from the actual travel time. To subtract the free flow travel time from the travel time, we can graphically move the outflow curve to the left, as is shown in figure 3.3(a). For illustration purposes, the figure is zoomed at figure 3.3(b). The figure shows that if the travel time equals the free flow travel time, both curves are the same, leading to 0 delay.

Similar to how the cumulative curves can be used to determine the travel time, the moved cumulative curves can be used to determine the delay. The delay for an individual vehicle can be found by the horizontal distance between

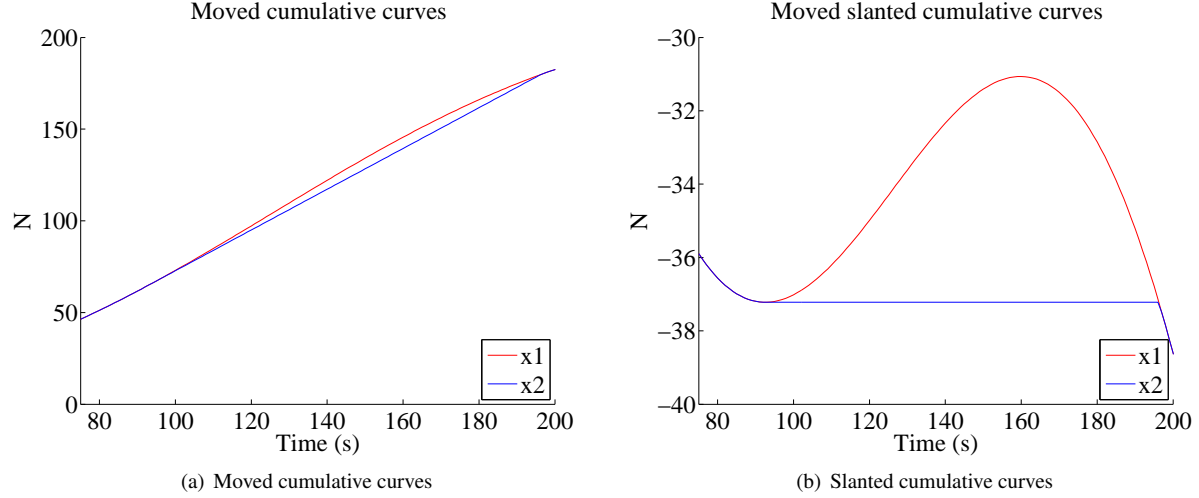


Figure 3.3: Determining the delay and the flows from cumulative curves

the two lines. The vertical distance between the two lines can be interpreted as the number of vehicles queuing. The total delay is the area between the two lines:

$$\mathcal{D} = \int (tt_i - tt_{\text{free flow}}) di \quad (3.10)$$

This is the area between the two lines. If we define N_{queue} as the number of vehicles in the queue at moment t , we can also rewrite the total delay as

$$\mathcal{D} = \int N_{\text{queue}}(t) dt \quad (3.11)$$

3.4 Slanted cumulative curves

Slanted cumulative curves or oblique cumulative curves is a very powerful yet simple tool to analyse traffic streams. These are cumulative curves which are off set by a constant flow:

$$\tilde{N} = \int q - q_0 dt - \int q_0 dt = \int q dt - \int q_0 dt \quad (3.12)$$

This means that differences with the freely chosen reference flow q_0 are amplified: in fact, only the difference with the reference flow are counted. The best choice for the reference flow q_0 is a capacity flow.

Figure 3.3(b) shows the slanted cumulative curves for the same situation as in figure 3.3(a). The figure is off set by $q_0 = 4000$ veh/h. Because the demand is initially lower than the capacity, \tilde{N} reaches a negative value. From the moment outflow equals capacity, the slanted cumulative outflow curve is constant. Since the demand is higher than the capacity, this increases. At the moment both curves intersect again, the queue is dissolved.

The vertical distance between the two lines still shows the length of the queue, N_{queue} . That means that equation 3.10 still can be applied in the same way for the slanted cumulative curves, and the delay is the area between the two lines.

Slanted cumulative curves are also particularly useful to determine capacity, and to study changes of capacity, for instance the capacity drop (see section 7.2). In that case, for one detector the slanted cumulative curves are drawn. By a change of the slope of the line a change of capacity is detected. In appendix C a Matlab code is provided by which cumulative curves can be made, and which includes the computation of several key performance indices.

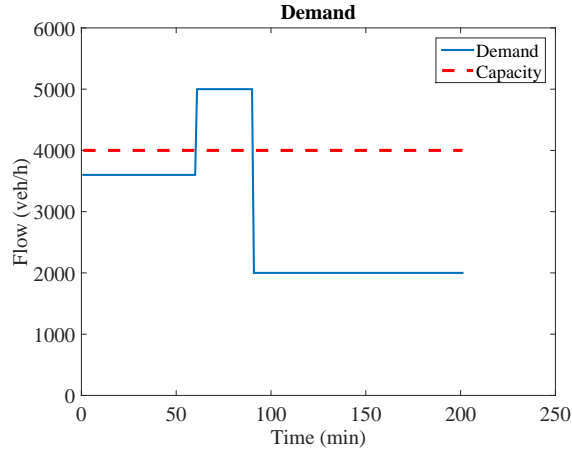


Figure 3.4: Demand and capacity

3.5 Practical limitations

Cumulative curves are very useful for models where the blocking of traffic does not play a role. For calculating the delay in practise, the method is not very suitable due to failing detectors. Any error in the detection (a missed or double counted observation), will change one of the curves and will offset the cumulative flow, and this is never corrected; this is called cumulative drift. Recently, an algorithm has been proposed to check the offsets by cross checking the cumulative curves with observed travel times (Van Lint et al., 2014). This is work under development. Moreover, some types of detectors will systematically miscount vehicles, which makes the above-mentioned error larger.

Apart from their use in models, slanted cumulative curves are very powerful to show changes in capacity in practise.

3.6 Example application

Consider a road with a demand of:

$$q_{in} = \begin{cases} 3600v/h & \text{for } t < 1h \\ 5000v/h & \text{for } 1h < t < 1.5h \\ 2000v/h & \text{for } t > 1.5h \end{cases} \quad (3.13)$$

The capacity of the road is 4000 veh/h. A graph of the demand and capacity is shown in figure 3.4.

1. Construct the (translated=moved) cumulative curves
2. Calculate the first vehicle which encounters delay (N)
3. Calculate the time at which the delay is largest
4. Calculate the maximum number of vehicles in the queue
5. Calculate the vehicle number (N) with the largest delay
6. Calculate the delay this vehicle encounters (in h, or mins)
7. Calculate the time the queue is solved
8. Calculate the last vehicle (N) which encounters delay

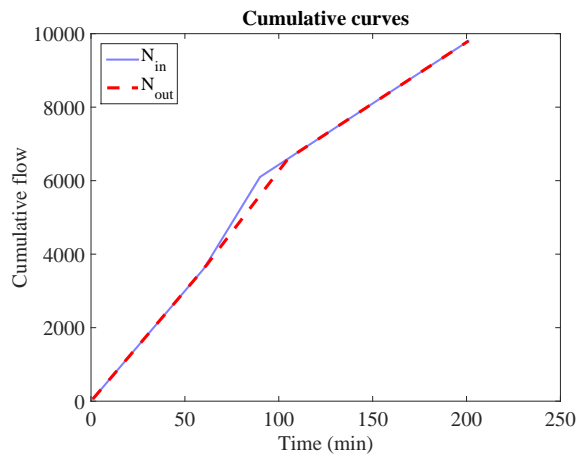
9. Calculate the total delay (veh-h)
10. Calculate the average delay of the vehicles which are delayed (h)

This can be answered by the following:

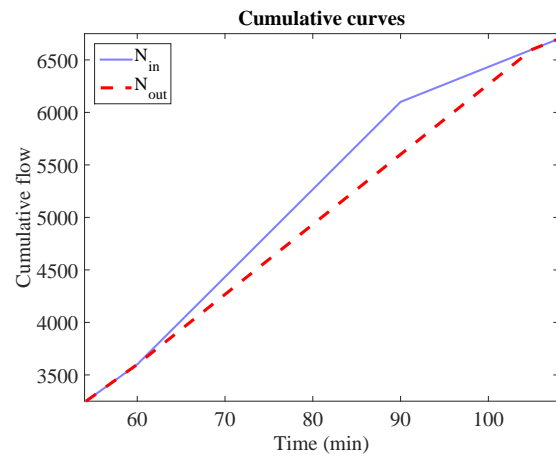
1. For the cumulative curves, an inflow and an outflow curve needs to be constructed; both increase. For the inflow curve, the slope is equal to the demand. For the outflow curve, the slope is restricted to the capacity. During the first hour, the demand is lower than the capacity, hence *the outflow is equal to the demand*. From $t=1\text{h}$, the inflow exceeds the capacity and the outflow will be equal to the demand. The cumulative curve hence increases with a slope equal to the capacity. As long as there remains a queue, i.e. the cumulative inflow is higher than the outflow, the outflow remains at capacity. The outflow remains hence increasing with a slope equal to the capacity until it intersects with the cumulative inflow. Then, the outflow follows the inflow: see figure 3.5(a) and for a more detailed figure 3.5(b).
2. The first vehicle which encounters delay (N) Delays as soon as $q_i C$: so after 1h at $3600 \text{ v/h} = 3600$ vehicles.
3. : The time at which the delay is largest: A queue builds up as long as $q_i C$, so up to 1.5 h. At that moment, the delay is largest
4. The maximum number of vehicles in the queue: 0.5 h after the start of the queue, $0.5 * 5000 = 2500$ veh entered the queue, and $0.5 * 4000 = 2000$ left: so 500 vehicles are in the queue at $t=0.5\text{h}$
5. The vehicle number (N) with the largest delay: $N(1.5\text{h}) = 3600 + 0.5 * 5000 = 6100$
6. : The delay this vehicle encounters (in h, or mins): It is the 2500th vehicle after $t=1\text{h}$. The delay is the horizontal delay between the entry and exit curve. It takes at capacity $2500/4000 = 37.5$ mins to serve 2500 vehicles. It entered 0.5 hours = 30 mins after $t=1$, so the delay is 7.5 mins
7. The time the queue is solved: This is the time point that the inflow and outflow curves intersect again. 500 vehicles is the maximum queue length, and it reduces with $4000 - 2000 = 2000 \text{ veh/h}$. So $500/2000 = 15$ minutes after the time that $q_i C$ the queue is solved, i.e. 1:45h after the start.
8. The last vehicle (N) which encounters delay This is the vehicle number at the moment the inflow and outflow curves meet again. 15 minutes after the vehicle number with the largest delay: $6100 + 0.25 * 2000 = 6600$ veh
9. The total delay. This is the area of the triangle between inflow and outflow curve. This area is computed by $0.5 * \text{height} * \text{base} = 0.5 * 500 * (30+15)/60 = 187.5 \text{ veh-h}$. Note that here we use a generalised equation for the area of a triangle. Indeed, we transform the triangle to a triangle with a base that has the same width, and the height which is the same for all times (i.e., we skew it). The height of this triangle is 500 vehicles (the largest distance between the lines) and the width is 45 minutes.
10. The average delay of the vehicles which are delayed (h) $187.5 \text{ veh-h} / (6600 - 3600) \text{ veh} = 0.0625 \text{ h} = 3.75 \text{ min}$

Selected problems

For this chapter, consider problems: 3, 4, 68, 69, 70, 71, 100, 142, 143, 144, A.7.2, 206, 206, 235, 236, 261



(a) Overview of the cumulative curves



(b) More detailed view of the cumulative curves

Figure 3.5: Cumulative curves for the example

Chapter 4

Relationships of traffic variables

Chapter 1 defined the variables and their definition. This chapter will discuss the relationship between these variables. First of all the mathematically required relationships are shown (section 4.1), then typical properties of traffic in equilibrium are discussed (section 4.2). Section 4.3 discusses these relationships in the light of drivers, and expands this to non-equilibrium conditions. Finally, section 4.4 gives attention to the moving observer.

4.1 Fundamental relationship

In microscopic view, it is obvious that the headway (h), the spacing (s) and the speed (v) are related. The headway times the speed will give the distance covered in this time, which is the spacing. It thus suffices to know two of the three basic variables to calculate the third one.

$$s = hv \quad (4.1)$$

Since headways and spacings have macroscopic counterparts, there is a macroscopic equivalent for this relationship. After reordering, equation 4.1 reads

$$\frac{1}{h} = \frac{1}{s}v \quad (4.2)$$

The macroscopic equivalent of this relationship is the average of this equation. Remembering that $q = \langle \frac{1}{h} \rangle$ and $k = \langle \frac{1}{s} \rangle$, we get:

$$\boxed{q = ku} \quad (4.3)$$

This equation shows that the flow q is proportional with both the speed u and the density k . Intuitively, this makes sense because when the whole traffic stream moves twice as fast if the flow doubles. Similarly, if – at original speed – the density doubles, the flow doubles as well.

Table 4.1 summarizes the variables and their relationships.

Table 4.1: The basic traffic variables and their relationship

Microscopic	Macroscopic
s	$k = \frac{1}{\langle s \rangle}$
h	$q = \frac{1}{\langle h \rangle}$
v	$u = \frac{1}{\langle v \rangle}$
$s = hv$	$q = ku$



Figure 4.1: The extreme situations and an idea for the fundamental diagram

4.2 Fundamental diagram

If two of the three macroscopic traffic flow variables are known, the third one can be calculated. This section will show that there is another relationship. In fact, there is an equilibrium relationship between the speed and the density. First, a qualitative understanding will be given, after that the effect will be shown for various couples of variables. Also, different shapes of the supposed relationship will be shown (section 4.2.5).

4.2.1 Qualitative understanding of the shape

Let us, for the sake of argument, consider the relationship between density and flow. And let us furthermore start considering the most extreme cases. First, the case that there is no vehicle on the road. Since the density is 0, the flow is 0, according to equation 4.3. In the other extreme case the density on the road is very high, and the speed is 0. Using again equation 4.3 we find also for this case a flow of 0. In between, there are traffic states for which the traffic flow is larger than zero. Assuming a continuous relationship between the speed and the density (which is not necessarily true, as will be discussed section 7.2) there will be a curve relating the two points at flow 0. This is indicated in figure 4.1(c).

This relationship is being observed in traffic. However, it is important to note that this is *not* a causal relationship. One might argue that due to the low speed, drivers will drive closer together. Alternatively, one might argue that due to the close spacing, drivers need to slow down.

4.2.2 Traffic state

We can define a traffic state by its density, flow and speed. Using equation 4.3, we only need to specify two of the variables. Furthermore, using the fundamental diagram, one can be sufficient. It is required that the specified variable then has a unique relationship to the others. For instance, judged by figure 4.1(c), specifying the density will lead to a unique flow, and a unique speed (using equation 4.3, and thus a unique traffic state). However, specifying the flow (at any value between 0 and the capacity) will lead to two possible densities, two possible speeds, and hence two possible traffic states.

The speed of the traffic can be derived using the equation 4.3:

$$u = \frac{q}{k} \quad (4.4)$$

For a traffic state in the flow density plane, we can draw a line from the traffic state to the origin. The slope of this line is q/k . So the speed of the traffic can be found by the slope of a line connecting the origin to the traffic state in the flow density plane. The free flow speed can be found by the slope of the fundamental diagram at $k=0$, i.e. the derivative of the fundamental diagram in the origin.

4.2.3 Important points

The most important aspect of the fundamental diagram for practitioners is the capacity. This is the maximum flow which can be maintained for a while at a road. The same word is also used for the traffic state at which maximum flow

is obtained. This point is found at the top of the fundamental diagram. Since we know that the flow can be determined from the headway, we can estimate a value for the capacity if we consider the minimum headway. For drivers on a motorway, the minimum headway is approximately 1.5 to 2 seconds, so we find a typical capacity value of $\frac{1}{2}$ to $\frac{1}{1.5}$ vehicles per second. If we convert this to vehicles per hour, we find (there are 3600 seconds in an hour) $\frac{3600}{2} = 1800$ to $\frac{3600}{1.5} = 2400$ vehicles per hour.

The density for this point is called the critical density, and the according speed the critical speed. The capacity is found when the average headway is shortest, which is when a large part of the vehicles is in car-following mode. This happens at speeds of typically 80 km/h; this then is the critical speed. From the capacity and the critical speed, the critical density can be calculated using equation 4.3. This varies from typically 20 veh/km/lane to 28 veh/km/lane.

For densities lower then the critical density, traffic is in an uncongested state; for higher densities, traffic is in a congested state. In the uncongested part, the traffic flow increases with an increase of density. In the congested branch, the traffic flow decreases with an increase of density. The part of the fundamental diagram of uncongested traffic states is called the uncongested branch of the diagram. Similarly, the congested branch gives the points for which the traffic state is congested.

The free flow speed is the speed of the vehicles at zero density. At the other end, we find the density at which the vehicles come to a complete stop, which is called the jam density. For the jam density, we can also make an estimation based on the length of the vehicles and the distance they keep at standstill. A vehicle is approximately 5 meters long, and they keep some distance even at standstill (2-3 meters), which means the jam density is $\frac{1}{5+3}$ to $\frac{1}{5+2}$ veh/m, or $\frac{1000}{5+3} = 125$ veh/km to $\frac{1000}{5+2} = 142$ veh/km.

4.2.4 Fundamental diagram in different planes

So far, the fundamental diagram has only be presented in the flow density plane. However, since the fundamental equation (equation 4.3) relates the three variables to each other, any function relating two of the three variables to each other will have the same effect. Stated otherwise, the fundamental relationship can be presented as flow-density relationship, but also as speed-density relationship or speed-flow relationship. Figure 4.2 shows all three representations of the fundamental diagram for a variety of functional forms.

In the speed-density plane, one can observe the high speeds for low densities, and the speed gradually decreasing with increasing density. In the speed-flow diagram, one sees two branches: the congested branch with high speeds and high flows, and also a congested branch with a low speed and lower flows.

4.2.5 Shapes of the fundamental diagram

There are many shapes proposed for the fundamental diagram. The data is quite scattered, so different approaches have been taken: very simple functions, functions with mathematically useful properties, or functions derived from a microscopic point of view. Even today, new shapes are proposed. In the remainder of this section, we will show some elementary shapes; the graphs are shown in figure 4.2.

Greenshields

Greenshields was the first to observe traffic flows and publish on this in 1934 (Greenshields, 1934). He observed a platoon of vehicles and checked the density of the platoon and their speed. He assumed this relationship to be linear:

$$v = v_0 - ck \quad (4.5)$$

Note that for $k = \frac{v}{c}$ the speed equals 0, hence the flow equals zero, so the jam density equals $\frac{v}{c}$.

Triangular

The Greenshields diagram is not completely realistic since for a range of low densities, drivers keep the same speed, possibly limited by the current speed limit. The fundamental diagram which is often used in academia is the triangular

fundamental diagram, referring to the triangular shape in the flow-density plane. The equation is as follows:

$$q = \begin{cases} v_0 k & \text{if } k < k_c \\ q_c - \frac{k - k_c}{k_j - k_c} q_c & \text{if } k \geq k_c \end{cases} \quad (4.6)$$

Truncated triangular

Daganzo (1997) shows a truncated triangular fundamental diagram. That means that the flow is constant and maximized for a certain range of densities. The equation is as follows:

$$q = \begin{cases} v_0 k & \text{if } k < k_1 \\ v_0 k_1 & \text{if } k_1 < k < k_c \\ q_c - \frac{k - k_c}{k_j - k_c} q_c & \text{if } k \geq k_c \end{cases} \quad (4.7)$$

Smulders

Smulders (1989) proposed a fundamental diagram in which the speed decreases linearly with the density for the free flow branch. In the congested branch the flow decreases linearly with density.

Drake

Drake et al. (1967) proposes a continuous fundamental diagram where the speed is an exponentially decreasing function of the density:

$$v = v_0 \exp \left(-\frac{1}{2} \left(\frac{k}{k_c} \right)^2 \right) \quad (4.8)$$

Inverse lambda

The capacity drop (see section 7.2) is not present in the fundamental diagrams presented above. Koshi et al. (1981) introduced an ‘inverse lambda’ fundamental diagram. This means the traffic has a free speed up to a capacity point. The congested branch however, does not start at capacity but connects a bit lower at the free flow branch. It is assumed that traffic remains in the free flow branch and after congestion has set in, will move to the congested branch. Only after the congestion has solved, passing a density lower than the density where the congested branch connects to the free flow branch, traffic flows can grow again to higher values. The description is as follows:

$$q = \begin{cases} v_0 k & \text{if } k < k_c \\ v_0 k_1 - \frac{k - k_1}{k_j - k_1} v_0 k_1 & \text{if } k \geq k_1 \text{ and traffic is congested} \end{cases} \quad (4.9)$$

This shape of the fundamental diagram allows for two traffic states with similar densities but different flows. This can yield unrealistic solutions to the kinematic wave model (see section 5).

Wu

An addition to the inverse-lambda fundamental diagram is made by Wu (2002). He assumes the speed in the free flow branch to decrease with increasing density. The shape of the free flow branch is determined by the overtaking opportunities, which in turn depend on the number of lanes, l . The equation for the speed is

$$q = \begin{cases} k \left(1 - \left(\frac{k}{k_1} \right)^{l-1} * v_0 + \left(\frac{k}{k_1} \right)^{l-1} v_p \right) & \text{if } v > u_p \\ v_p k_1 - \frac{k - k_1}{k_j - k_1} v_0 k_1 & \text{if } k \geq k_1 \text{ and traffic is congested} \end{cases} \quad (4.10)$$

Kerner

Kerner (2004) has proposed a different theory on traffic flow, the so-called three phase traffic flow theory. This will be described in more detail in section 7.4. For here, it is important to note that the congested branch in the three phase traffic flow theory is not a line, but an area.

4.3 Microscopic behaviour

Section 4.2 showed the equilibrium relationships observed in traffic. This is a result of behavior, which can be described at the level of individual drivers as well. This section does so. First, the equilibrium behaviour is described in section 4.3.1. Then, section 4.3.2 discusses hysteresis, i.e. structural off-equilibrium behaviour under certain conditions.

4.3.1 Equilibrium behaviour

The fundamental diagram describes traffic in equilibrium conditions. That can happen if all drivers are driving in equilibrium conditions, i.e. all drivers are driving at a headway which matches a speed. Using the relationships in table 4.1 one can change a fundamental diagram on an aggregated level to a fundamental diagram on an individual level. This way, one can relate individual headways to individual speeds.

The fundamental diagram gives the average distance drivers keep. However, there is a large variation in drivers' behaviour. Some keep a larger headway, and some drivers keep a smaller headway for the same speed. These effects average out in a fundamental diagram, since the average headway for a certain speed is used. On an individual basis, there is a much larger spread in behaviour.

4.3.2 Hysteresis

Apart from the variation between drivers, there is also a variation within a driver for a distance it keeps at a certain speed (which we assume in this section as representative of the fundamental diagram). These can be random variations, but there are also some structural variations. Usually the term Hysteresis is used to indicate that the driving behaviour (i.e. the distance) is different for drivers before they enter the congestion compared to after they come out of congestion. That is, the distance *at the same speed* is different in each of these conditions.

Two phenomena might play a role here:

1. Delayed reaction to a change of speed
2. Anticipation of a change in speed

Zhang (1999) provides an excellent introduction to hysteresis. The simplified reasoning is as follows.

Let's first discuss case 1, drivers have a delayed reaction to a change of speed. That means that when driving at a speed, first the speed of the leader reduces, then the distance reduces. So during the deceleration process, the headway is shorter than the equilibrium headway. When the congestion solves, first the leader will accelerate, and the driver will react late on that. That means that the leader will shy away from the considered car, and the distance will be larger than the equilibrium distance.

In case 2, if the driver anticipates the change in speed, the exact opposite happens. Before the deceleration actually happens, a driver will already decrease speed (by definition in anticipation), leading to an larger headway than the equilibrium headway for a certain speed. Under acceleration, the opposite happens, and a driver can already accelerate before the would be suitable in case of equilibrium conditions. Hence, in the acceleration phase, the driver has a shorter headway than in equilibrium conditions for the same speed.

In traffic, we expect drivers to have a reaction time. In fact, the reaction time can be derived from the fundamental diagram, as section 8.1 will show later on. It will also show that the best way to analyse car-following behaviour is not comparing the distance-speed relationship for one pair *at one moment in time*, as shown in figure 4.3. It shows that the drivers have no hysteresis – they copy the movement of the leader perfectly – but still the gap changes with a constant speed. Instead, one should make the analysis of car-following behavior *along the axis parallel to the wave speed*.

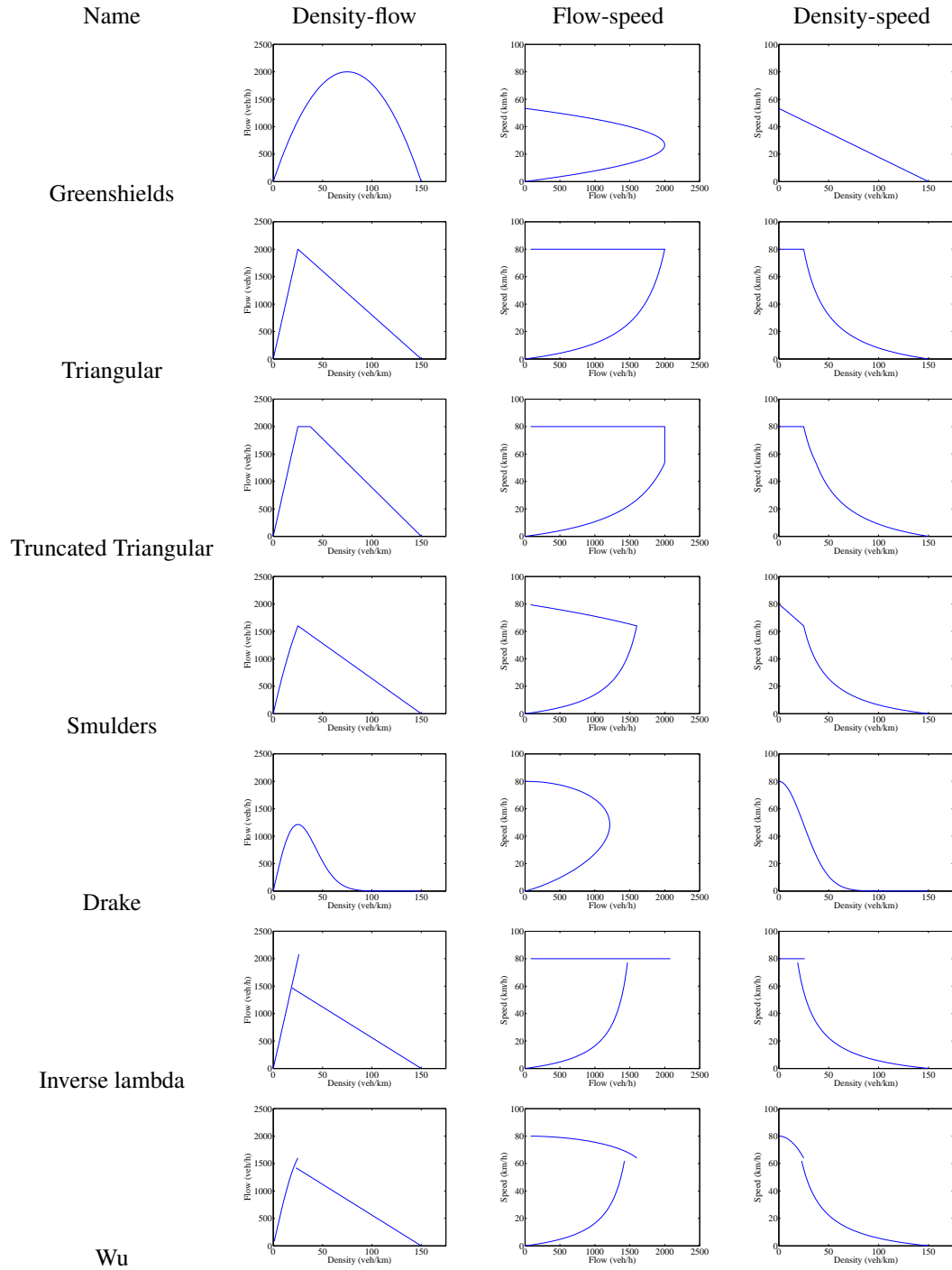


Figure 4.2: Different shapes of the fundamental diagram

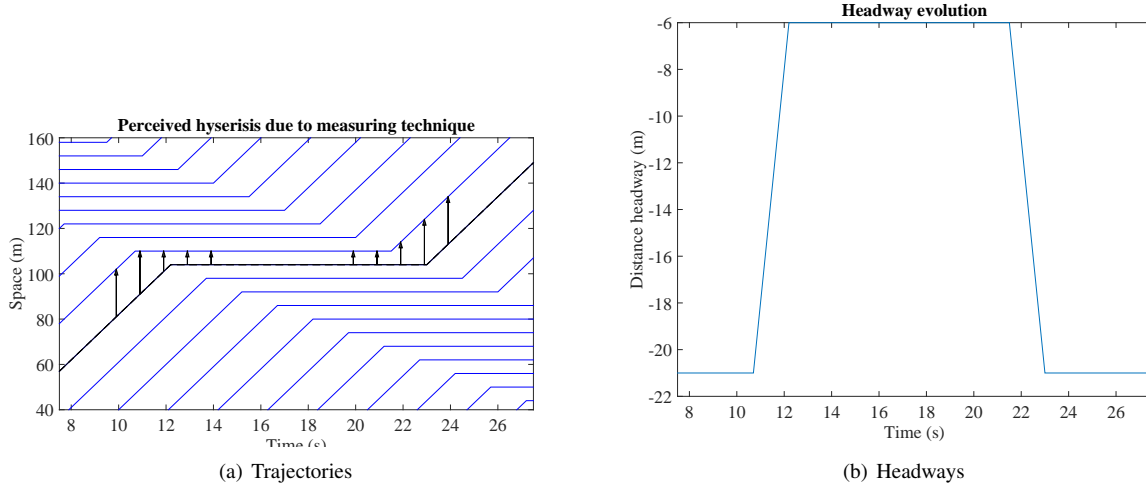


Figure 4.3: Mistakes if making the headway analysis at one moment in time

Laval (2011) provides a very good insight in the differences one can obtain using this correct technique or using the (erroneous) comparison of instantaneous headways (as in the arrows in figure 4.3(b)).

4.4 Moving observer

An observer will only observe what is in the observation range. Many observations are taken at a point in space. This point might move with time, for instance a driver might check the number of trucks he is overtaking. In this case, the driver is moving and observing, this is called a moving observer. This section discusses the effects of the speed of the moving observer, and also discusses the effect of observed subjects passing a stationary observer with different speeds.

Basically, the movement at speed v has no effect on density, but the relative speed of traffic changes. Therefore, applying equation 4.3, the relative flow changes. Written down explicitly, one obtains a relative flow q_{rel} :

$$q_{\text{rel}} = k(v - v) \quad (4.11)$$

RemoveSo indeedIf the observer moves with the speed of the traffic, the observed relative flow becomes zero. In practice if not all vehicles drive at the same speed, the flow needs to be divided into classes with the same speed and the partial flows for each of these classes should be calculated.

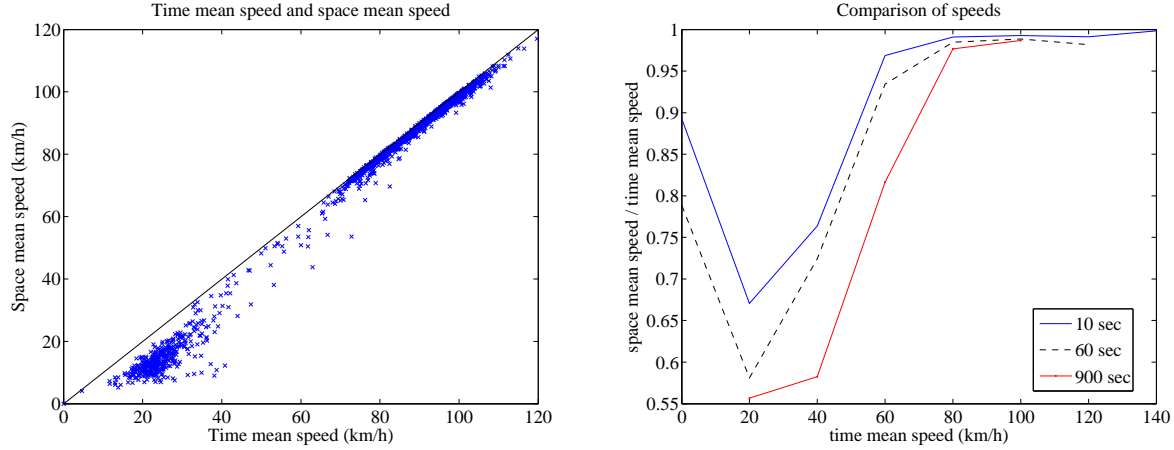
$$q_{\text{rel}} = \sum_v (k_{\text{Vehicles at speed } v} (v - v)) \quad (4.12)$$

Local measurements

Suppose there is a local detector located at location x_{detector} . Now we reconstruct which vehicles will pass in the time of one aggregation period. For this to happen, the vehicle i must be closer to the detector than the distance it travels in the aggregation time:

$$x_{\text{detector}} - x_i \leq t_{\text{agg}} v_i \quad (4.13)$$

In this formula, x is the position on the road and t_{agg} the aggregation time. For faster vehicles, this distance is larger. Therefore, if one takes the local (arithmetic) mean, one overestimates the influence of the faster vehicles. If the influence of the faster vehicles on speeds is overestimated, the average speed u_t is overestimated (compared to the space-mean speed u_s).



(a) The arithmetic mean and the harmonic mean of the speeds of the vehicles passing a cross section of a motorway (b) The arithmetic mean and the harmonic mean of the speeds of the vehicles passing a cross section of a motorway

Figure 4.4: The effect of inhomogeneities in speeds: the difference in arithmetic mean and harmonic mean speed

The discussion above might be conceived as academic. However, if we look at empirical data, then the differences between the time-mean speeds and space-mean speeds become apparent. Figure 4.4 shows an example where the time-mean speed and space-mean speed have been computed from motorway individual vehicle data collected on the A9 motorway near Amsterdam, The Netherlands. Figure 4.4 shows that the time mean speed can be twice as high as the space mean speed. Also note that the space-mean speeds are always lower than the time-mean speeds.

In countries where inductive loops are used to monitor traffic flow operations and arithmetic mean speeds are computed and stored, average speeds are overestimated, affecting travel time estimations. Namely, to estimate the average travel time, the average of $TT = L/v$ is needed, in which L is the length of the road stretch and v the travel speed. Since L is constant, the average travel time can be expressed as

$$\langle TT \rangle = L \left\langle \frac{1}{v} \right\rangle \quad (4.14)$$

From this, it follows that the harmonically averaged speed is required for estimating the mean travel time.

Furthermore, since $q = ku$ (equation 4.3) can only be used for space-mean speeds, we cannot determine the density k from the local speed and flow measurements, complicating the use of the collected data for, e.g. traffic information and traffic management purposes. As figure 4.4 already shows, largest relative deviation is found at the lower speeds. In absolute terms, this is not too much, so one might argue this is not important. However, a low speed means a high density or a large travel time. For estimating the densities, this speed averaging has therefore a large effect, as can be seen in figure 4.5.

Selected problems

For this chapter, consider problems: 1, 66, 90, A.5.3, 140, 141, 155, 156, 176, 177, 178, 189, 196, 195, 198, 216, 224, 225, 246, 256, A.10.5, 259

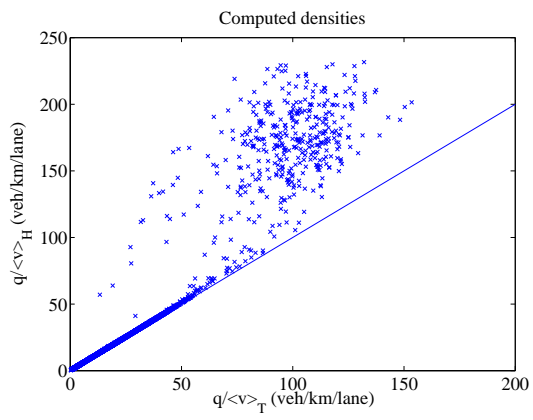


Figure 4.5: Densities computed using arithmic mean speeds or harmonic mean speeds.

Chapter 5

Shock wave theory

This chapter describes shock wave theory to capture queuing dynamics. This differs from cumulative curves in the way that the spatial extent of the queue is considered. The section first gives examples on a fixed bottleneck (section 5.1), then gives examples of the moving bottleneck (section 5.2). Section 5.3 describes the stop-and-go waves in this modelling framework.

5.1 Fixed bottlenecks

In this section Fixed bottlenecks are discussed. At fixed bottleneck some lanes of a highway are (temporarily) blocked. Firstly the theory and derivation of equations will be discussed (section 5.1.1). Thereafter, two examples are given (Section 5.1.2 and 5.1.3)

5.1.1 Theory and derivation of equations

Let us consider a situation with two different states: state A downstream, with a matching q_A , k_A en v_A and state B upstream (q_B , k_B en v_B). The states are plotted in the space-time diagram 5.1. We choose the axis in such a way that the shockwave moves through the point $t=0$ at $x=0$. We will now derive the equation to get the speed of this wave.

In the derivation, we base the reasoning on figure 5.1. The boundary between is called a shock wave. This wave indicates where the speed of the vehicles changes. It is important to note that there are no vehicles captured in the wave itself: the wave itself does not have a physical length. Thus the assumption is that vehicles change speed instantaneously.

Because there are no vehicles in the wave, the number of vehicles entering the wave must be equal to the number of vehicles exiting exiting the wave, or we can state that rate of vehicles entering the wave must be equal to the rate of vehicles exiting the wave. This principle, in combination with the following equation (already presented in equation 4.3) is used to calculate the speed of the wave:

$$q = kv \quad (5.1)$$

The speed of the wave is indicated by w . Note that we can apply this equation to moving frames of reference as well. In that case, the flow changes, as does the speed. The density is invariant under a change of reference speed.

To determine the attachment and exit rate, we will move with the speed of the wave (in the frame of a moving observer). At the downstream end, the density is k_B . The speed in the moving frame of reference is $v_B - w$. The exit rate in the moving frame of reference is calculated using equation 5.1.

$$q_{\text{exit}} = k_B (v_B - w) \quad (5.2)$$

In the same way, the attachment rate can be determined. The upstream density is k_A . The speed of the vehicles in the frame of reference moving with the wave speed w is $v_A + w$. Using equation 5.1 again, we find the attachment rate in this moving frame of reference:

$$q_{\text{attachment}} = k_A (v_A + w) \quad (5.3)$$

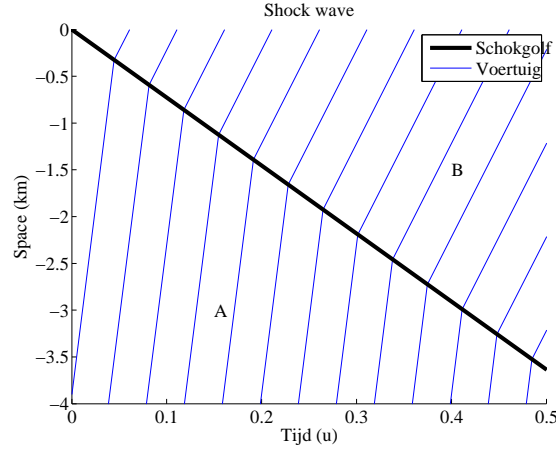


Figure 5.1: A shockwave where traffic speed changes from high to low.

Since these rates have to be equal, we find:

$$q_{\text{exit}} = q_{\text{attachment}} \quad (5.4)$$

$$k_A (v_A - w) = k_B (v_B - w) \quad (5.5)$$

This can be rewritten as:

$$k_A v_A - k_A w = k_B v_B - k_B w \quad (5.6)$$

$$q_A - k_A w = q_B - k_B w \quad (5.7)$$

In the last step, the speeds have been substituted using equation 5.1. We can solve this equation for the shock wave speed w . We find

$$q_A - q_B = (-k_B + k_A) w \quad (5.8)$$

And isolating w give the wave speed equation:

$$w = \frac{q_A - q_B}{k_A - k_B} = \frac{\Delta q}{\Delta k} \quad (5.9)$$

Note that in a space-time plot, the speed w is the slope of the shock wave between A and B. The right hand side is the ratio between the difference in flow and the difference in density of states A and B. This is also the slope of a line segment between A and B in the flow-density plot. This becomes very useful when constructing the traffic states.

The above reasoning holds for the speed of any shock wave, moving backward or forward. The following section shows an example for both.

5.1.2 Example: Temporal increase in demand at a road with a lane drop

Let's consider a 3 lane road with a reduction to 2 lanes over a 1 km section between $x=10$ and $x=12.5$ (see figure 5.2(b)). For the road, we assume lanes with equal characteristics, described by a triangular fundamental diagram with a free speed of 80 km/h, a capacity of 2000 veh/h/lane and a jam density of 150 veh/km/lane. At the start of the road, there is a demand of 2500 veh/h which temporarily increases to 5000 veh/h between $t=1$ h and $t=2$ h (see the demand profile in figure 5.2(b)). The question we will answer in this example is: *What are the resulting traffic conditions?*

The final answer to the question are the traffic states which are shown in table 5.1, and shown on the fundamental diagram in figure 5.3(a). The speed of the shock waves is given in table 5.2, and the resulting traffic situation is shown in figure 5.3(b). We will now explain how this solution can be found.

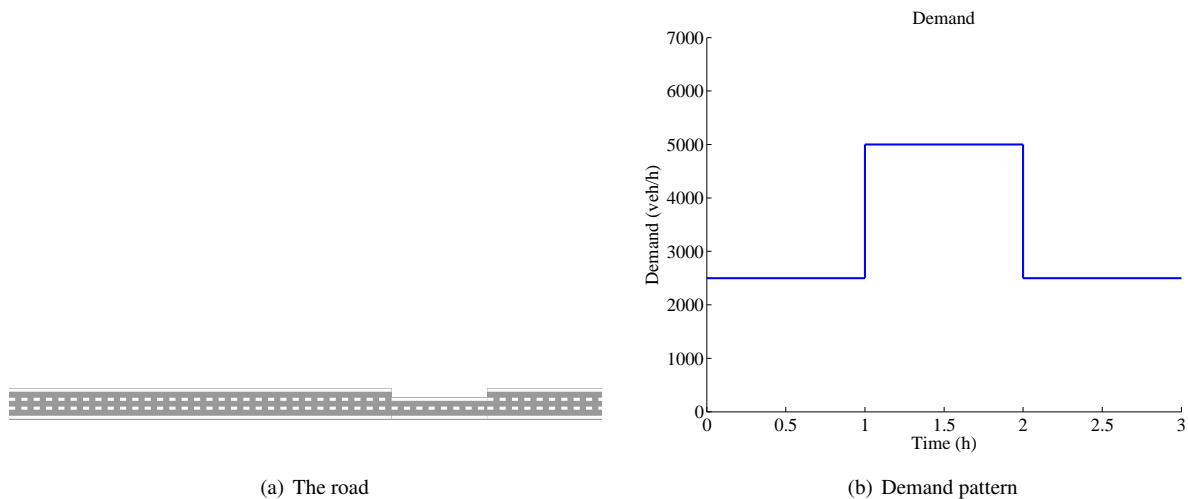


Figure 5.2: Situation

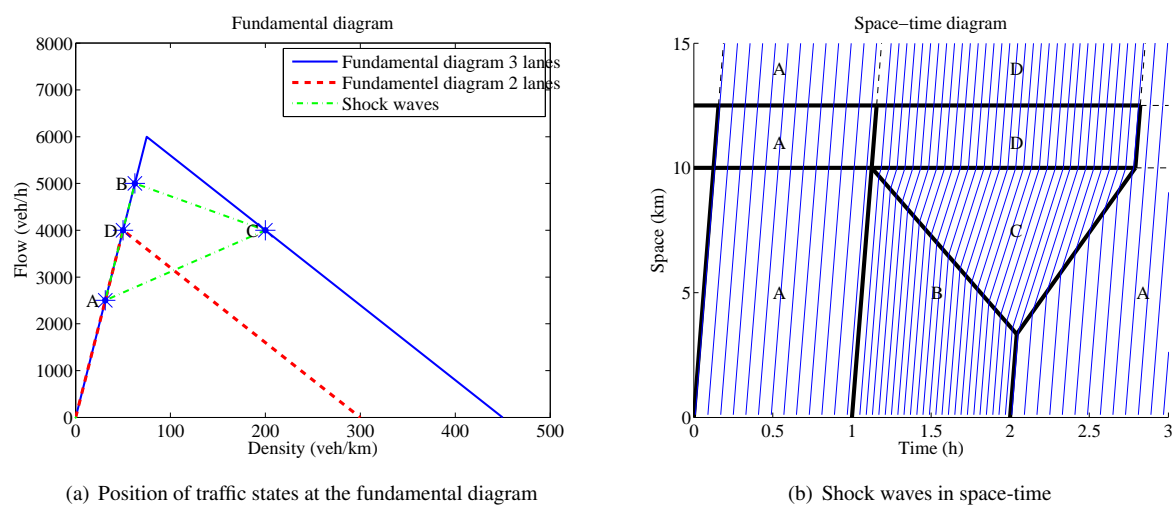


Figure 5.3: The situation

Table 5.1: The states on the road

Toestand	Stroom (vtg/u)	Dichtheid(vtg/km)	Snelheid (km/u)
A	2500	31.25	80
B	5000	62.5	80
C	4000	200	20
D	4000	50	80

Table 5.2: The shock waves present on the road

State 1	State 2	shock wave speed w (km/h)
A	B	80
B	C	-7.3
A	A	8.9

The inflow to the system is given, being 2500 veh/h (state A) and 5000 veh/h (state B) on a three lane road. The matching densities can be computed from the fundamental diagram for a three lane road. This gives densities of (equation 5.1) $k_A = \frac{q_A}{u_A} = \frac{2500}{80} = 31.25 \text{ veh/km}$ and $k_B = \frac{q_B}{u_B} = \frac{5000}{80} = 62.5 \text{ veh/km}$. The separation with the empty road moves forward with a speed of 80 km/h, i.e. the speed of the vehicles. This can also be found by the shock wave equation, equation 5.9. The difference in flow is 2500 veh/h and the difference in density is 31.25 veh/km. The shock wave then moves with:

$$w_{0A} = \frac{q_0 - q_A}{k_0 - k_A} = \frac{-2500}{-31.25} = 80 \text{ km/h} \quad (5.10)$$

Note that it does not matter whether the speed of shock wave w_{0A} or shock wave w_{A0} is calculated. This remark holds for every combination of states.

Also the wave between state A and B moves forward with 80 km/h, calculated by equation 5.9:

$$w_{AB} = \frac{q_A - q_B}{k_A - k_B} = \frac{2500 - 5000}{31.25 - 62.5} = 80 \text{ km/h} \quad (5.11)$$

Note that this equals the free flow speed. This is because we use a triangular fundamental diagram. The speed w_{ab} is the direction of the line segment AB in figure 5.3(a). This has the same slope as the slope of the free flow speed (i.e. the slope of the fundamental diagram at the origin) because its shape is triangular.

Now this wave hits the two lane section. The flow is higher than the capacity of the two lane section. That means that downstream, the road will operate at capacity, and upstream a queue will form (i.e. we have a congested state). The capacity of the downstream part is, according to the fundamental diagram, 4000 veh/h (state D). The speed follows from the (triangular) fundamental diagram, and is 80 km/h. The density hence is:

$$k_D = \frac{q_D}{u_D} = \frac{4000}{80} = 50 \text{ veh/km} \quad (5.12)$$

If 4000 veh/h drive onto the two lane segment, 4000 veh/h have to drive off the three lane segment (no vehicles can be lost or created at the transition from three to two lanes). That means that upstream of the transition, we have a congested state with a flow of 4000 veh/h. The density is derived from the fundamental diagram:

$$q_{\text{cong}} = q_{\text{capacity}} - q_{\text{capacity}} \frac{k - k_c}{k_j - k_c} = 4000 \quad (5.13)$$

Substituting the parameters for the fundamental diagram, and realising that the capacity is found by $q_{\text{capacity}} = l u_{\text{capacity}} k_c$ (l is the number of lanes) we calculate the density at point C, 200 veh/km. Graphically, we can find point C on the fundamental diagram by the intersection of the congested branch and a line at a constant flow value of 4000 veh/h.

The speed at which the tail of the queue moves backwards, i.e., the speed of the boundary between B and C, is calculated by the shock wave equation (equation 5.9)

$$w_{BC} = \frac{q_B - q_C}{k_B - k_C} = \frac{5000 - 4000}{62.5 - 200} = -7.3 \text{ km/h} \quad (5.14)$$

Note that this speed can also be derived graphically from the fundamental diagram, i.e. the slope of the line segment BC. That the slope in figure 5.3(a) and figure 5.3(b) is graphically not the same, is a consequence of different axis scales in the figures.

Then the demand reduces again and the inflow state returns to A. When lower demand hits the tail of the jam, the queue can solve from the tail. At the head of the queue, this change has no influence yet, since drivers are still waiting to get out onto the smaller roadway segment. The boundary between C and A moves with a speed of

$$w_{CA} = \frac{q_C - q_A}{k_C - k_A} = \frac{4000 - 2500}{200 - 31.25} = 8.9 \text{ km/h} \quad (5.15)$$

Here again, the speed could also be derived graphically, by the slope of the line segment AC.

Then, this wave arrives at the transition of the two lane road to a three lane road, and the congestion state C is dissolved. In the two lane part, the flow is now the same as the demand (the state in A, 2500 veh/h). The boundary between state D and A moves forward with a speed of

$$w_{DA} = \frac{q_D - q_A}{k_D - k_A} = \frac{4000 - 2500}{50 - 31.25} = 80 \text{ km/h} \quad (5.16)$$

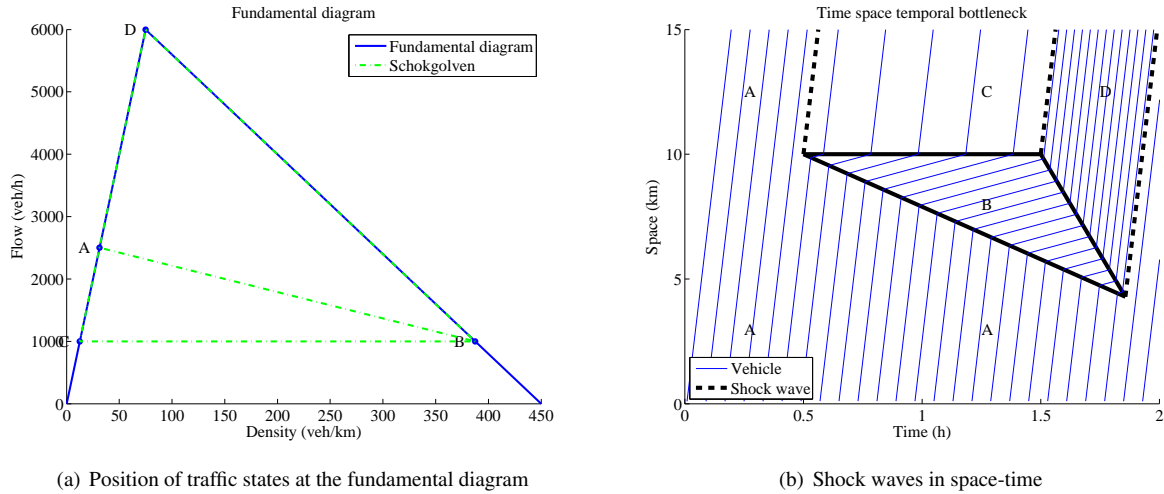


Figure 5.4: The situation

Table 5.3: The states on the road with a temporal bottleneck

Number	Flow	Density	Speed
A	2500	31.25	80
B	1000	387.5	
C	1000	12.5	12.5
D	6000	75	75

5.1.3 Example: Temporal capacity reduction

Another typical situation is a road with a temporal local reduction of capacity, for instance due to an accident. This section explains which traffic situation will result from that.

The case is as follows. Consider a three-lane freeway, with a triangular fundamental diagram. The free flow speed is 80 km/h, the capacity is 2000 veh/h/lane and the jam density is 150 veh/km/lane. The demand is constant at 2500 veh/h. From $t=1$ h to $t=2$ h, an incident occurs at $x=10$, limiting the capacity to 1000 veh/h. Calculate the traffic states and the shock waves, and draw them in the space-time diagram. Also draw several vehicle trajectories.

For referring to certain states, we will first show the resulting states, and then explain how these states are constructed. Figure 5.4(a) shows the fundamental diagram and the occurring states, 5.4(b) shows how the states move in space and time. The details of the states can be found in table 5.3, and the details of the shock waves can be found in table 5.4.

At the start, there are free flow conditions (state A) at an inflow of 2500 veh/h. For the assumed triangular fundamental diagram, the speed for uncongested conditions is equal to the free flow speed, so 80 km/h. The matching density can be found by applying equation 5.1: $k_A = \frac{q}{u} = \frac{2500}{80} = 31.25$ veh/km.

From $t=1$ to $t=2$, a flow limiting condition is introduced. We draw this in the space time diagram. The flow is too high to pass the bottleneck, so the moment the bottleneck occurs, a congested state (B) will form upstream.

Table 5.4: The shock waves present on the road with a temporal bottleneck

State 1	State 2	shock wave speed w (km/h)
A	C	80
B	C	0
A	B	-4.2
B	D	16

Downstream of the bottleneck we find uncongested conditions (once the vehicles have passed the bottleneck, there is no further restriction in their progress): state C. For state C, the flow equals the flow that can pass the bottleneck, which is given at 1000 veh/h. The speed is the free flow speed of 80 km/h, so the matching density can be found by applying equation 5.1: $k_C = \frac{q}{u} = \frac{1000}{80} = 12.5$ veh/km. The speed of the shock wave between state A and C can be calculated using the shock wave equation, 5.9:

$$w_{AC} = \frac{q_A - q_B}{k_A - k_B} = \frac{2500 - 1000}{31.25 - 12.5} = 80 \text{ km/h} \quad (5.17)$$

This equals the free flow speed. Graphically, we understand this because both states can be found at the free flow branch of the fundamental diagram (figure 5.4(a)) and the shock wave speed is the slope of the line segment connecting these states. Because the fundamental diagram is triangular, this slope is equal to the slope at the origin (i.e., the free flow speed).

Upstream of the bottleneck a congested state forms (B). The flow in this area must be the same as the flow which can pass the bottleneck. This is because at the bottleneck no new vehicles can be formed. That means state B is a congested state with a flow of 1000 veh/h. From the fundamental diagram we find the matching density in the congested branch, 387.5 veh/km. The speed at which the shock between states A and B now moves, can be calculated using equation 5.9:

$$w_{AB} = \frac{q_A - q_B}{k_A - k_B} = \frac{2500 - 1000}{31.25 - 387.5} = -4.2 \text{ km/h} \quad (5.18)$$

The minus sign means that the shock wave moves in the opposite direction of the traffic, upstream. We could also graphically derive the speed of the shock wave by the slope of the line between point A and B in the fundamental diagram.

Once the temporal bottleneck has been removed, the vehicles can drive out of the queue: state D. Because state C is congested, the outflow will be capacity (or the queue discharge rate in case there is a capacity drop). That is for this case a flow of 3×2000 veh/h = 6000 veh/h. Realising the vehicle speed equals the free flow speed of 80 km/h, the density can be found using equation 5.1:

$$k_D = \frac{q_D}{u_D} = \frac{6000}{80} = 75 \text{ veh/km} \quad (5.19)$$

The shock wave between state B and D moves backward. The speed thereof can be found by applying equation 5.9

$$w_{BD} = \frac{q_B - q_D}{k_B - k_D} = \frac{1000 - 6000}{387.5 - 75} = -16 \text{ km/h} \quad (5.20)$$

The negative shock wave speed means the wave moves upstream. Intuitively, this is right, since the vehicles at the head of the queue can accelerate out of the queue, and thus the head moves backwards.

5.2 Moving bottleneck

This section describes what happens if the road is blocked, either completely or not completely, by a moving bottleneck. This can be a slow moving truck or agricultural vehicle, a funeral or wedding procession. First the theory is explained (section 5.2.1), and then three examples follow (section 5.2.2, 5.2.3 and 5.2.4).

5.2.1 Theory

For the moving bottleneck, the same theory applies as for the fixed bottleneck. The recipe is the same: check for each bottleneck whether the demand exceeds capacity. If so, there is congestion upstream and a free flow condition (or capacity) downstream. Once again, the shock wave equation applies (equation 5.9).

Different compared to the regular, fixed bottlenecks, is the position of the congested state. For fixed bottlenecks, the flow upstream of the bottleneck equals the flow downstream of the bottleneck. In case of moving bottlenecks this differs. Consider a bottleneck which moves downstream without any overtaking opportunities. The downstream flow

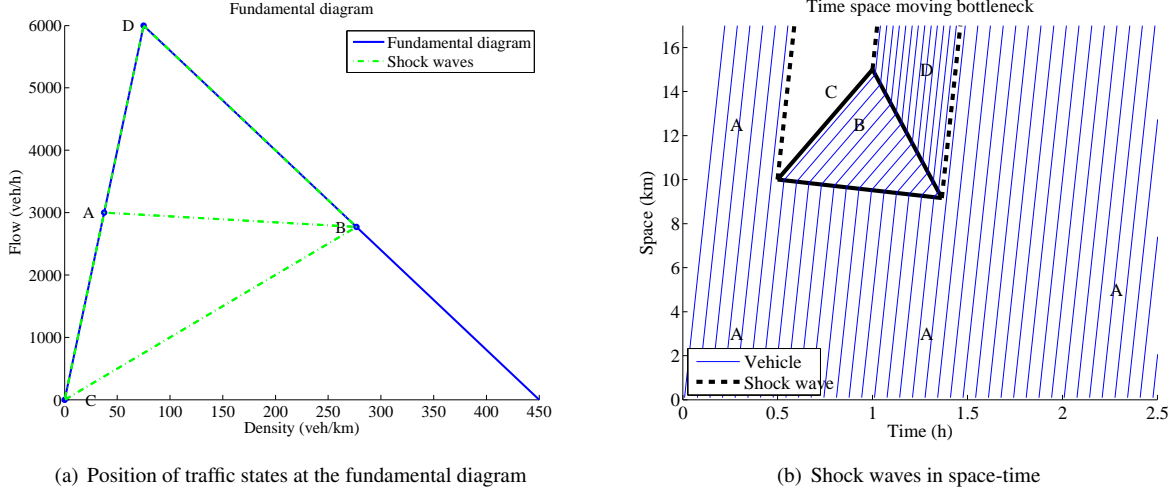


Figure 5.5: The situation with a moving bottleneck without overtaking opportunities

is zero, but vehicles can accumulate in the growing area between the considered point and the moving bottleneck, so the upstream flow is not zero.

In these types of calculations, the capacity of vehicles passing the moving bottleneck is usually an input. This gives the downstream point at the fundamental diagram. To find the upstream state on the fundamental diagram, one has to realise the shock wave *is* the moving bottleneck, so the speed of the shock wave *must* equal the speed of the moving bottleneck. By constructing a shock wave moving with the speed of the moving bottleneck in the fundamental diagram from the uncongested downstream point, one finds the congested point. This is at the intersection of the line segment starting at the uncongested point moving with the bottleneck speed and the congested branch of the fundamental diagram. The following examples clarify the procedure.

5.2.2 Example 1: moving truck, no overtaking possibilities

Consider a three lane road, where at all three lanes a triangular fundamental diagram holds. The capacity is 2000 veh/h/lane, the free flow speed 80 km/h and the jam density 150 veh/km. The demand is 3000 veh/h. A truck enters the road at $t=0.5$ h and $x=10$ km, and leaves the road at $t=1$ h and $x=15$ km, hence driving 10 km/h. There are no overtaking opportunities. What is the traffic state at the road?

The solution of this example is given in a space-time diagram (figure 5.5(b)) and in the fundamental diagram (figure 5.5(a)). The characteristics of the states are given in table 5.5, and the characteristics of the shock waves are given in table 5.6. The explanation how these points are found follows below.

At two points states can be identified at the fundamental diagram (figure 5.5(a)), the initial state A (flow of 2500 veh/h, free flow speed 80 km/h) and the state downstream of the moving bottleneck (given “no overtaking possibilities” hence density zero and flow zero). In these examples, the states are identified by only two variables from the three flow, density and speed, since the third one can be calculated using equation 5.1.

The position upstream of the moving bottleneck can be determined by the intersection of two lines:

$$q_1 = q_C + v(k - k_C) \quad (5.21)$$

$$q_2 = q_D + w(k - k_c) \quad (5.22)$$

The first equation is a line in the fundamental diagram, figure 5.5(a) starting from point C and moving forward with the bottleneck speed v . The second line is the congested branch of the fundamental diagram, in which w is the slope of the congested branch. The intersection of these lines can be found by solving the density k from the equation $q_1 = q_2$. For this upstream density, the density of state B, we find $k_B = 277 \text{ veh/km}$. The matching flow is found by filling this in either equation 5.21 or 5.21, resulting in $q_B = 2769 \text{ veh/km}$. The speed is determined by the ratio of flow and

Table 5.5: The states on the road for a moving bottleneck without overtaking opportunities

Name	Flow	Density	Speed
A	3000	37.5	80
B	2769	277	10
C	0	0	NaN
D	6000	75	80

Table 5.6: The shock waves present on the road for a moving bottleneck without overtaking opportunities

State 1	State 2	shock wave speed w (km/h)
A	B	-0.96
B	C	10
A	C	80
D	C	80
B	D	-16
A	D	80

density: $u = \frac{q_B}{k_B} = \frac{2769}{277} = 10 \text{ km/h}$. Note that this is the speed of the moving bottleneck. This must be since there are no overtaking opportunities.

The speed of the shock wave between A and B can be calculated using the shock wave equation 5.9 applied to state A and B:

$$w_{AB} = \frac{q_A - q_B}{k_A - k_B} = \frac{3000 - 2769}{37.5 - 277} = -0.96 \text{ km/h} \quad (5.23)$$

This means the shock wave moves upstream with a low speed. With a different speed of the moving bottleneck or a different demand level, the shock wave might move faster upstream (lower bottleneck speed or higher demand), or it might move downstream (higher bottleneck speed or lower demand).

The speed of the shock wave between state B and C can also be calculated with equation 5.9. It can be determined from reasoning instead of calculations as well: it must be equal to the speed of the moving bottleneck, 10 km/h.

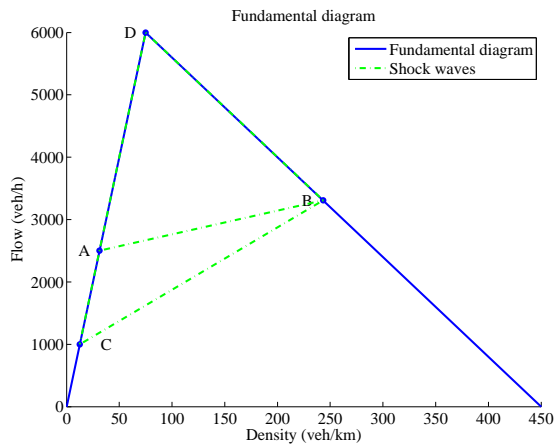
Once the moving bottleneck has left the road, vehicles will exit the jam. This means a boundary between the jam state, state B, at the capacity state, state D. For capacity the flow (6000 veh/h) and speed (80 km/h) can be derived from the road characteristics. The speed of the shock wave between state D and B can be determined by applying the shock wave equation (5.9) on state B and D. Alternatively, from the fundamental diagram in figure 5.5(a) we see that must equal the slope of the congested branch of the fundamental diagram, -16 km/h. Because any shock wave between any congested state and capacity moves with this speed, this speed is also called the wave speed of the fundamental diagram.

Speeds of shock waves between A and C, C and D, and D and A all can be calculated using the shock wave equation 5.9. Moreover, all these states lie on the free flow branch of the fundamental diagram, so the shock waves between these states move at the free flow speed of 80 km/h.

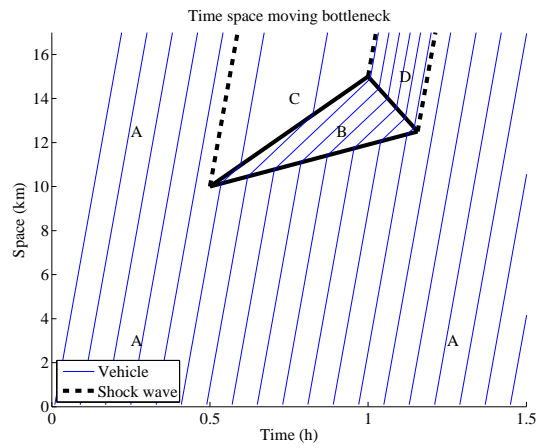
5.2.3 Example 2: moving truck with overtaking possibilities

Now, let's consider a different situation, where overtaking of the moving bottleneck is possible. We change the conditions as follows. Consider a three lane road, where at all three lanes a triangular fundamental diagram holds. The capacity is 2000 veh/h/lane, the free flow speed 80 km/h and the jam density 150 veh/km. The demand is 2500 veh/h. A truck enters the road at $t=0.5\text{h}$ and $x=10 \text{ km}$, and leaves the road at $t=1\text{h}$ and $x=15 \text{ km}$, hence driving 10 km/h. There are overtaking opportunities, such that downstream of the bottleneck the flow is 1000 veh/h. What is the traffic state at the road?

The states and fundamental diagram, as well as the resulting traffic states are show in figures 5.6(a) and 5.6(b) respectively. Tables 5.7 and 5.8 give the properties of the states and the shock waves respectively. Below, it is explained how these states and waves are found.



(a) Position of traffic states at the fundamental diagram



(b) Shock waves in space-time

Figure 5.6: The situation at a moving bottleneck with overtaking possibilities

Table 5.7: The states on the road at a moving bottleneck with overtaking possibilities

State	Flow (veh/h)	Density(veh/km)	Speed (km/h)
A	2500	31.25	80
B	3307	243	13.6
C	1000	12.5	80
D	6000	75	80

Table 5.8: The shock waves present on the road at a moving bottleneck with overtaking possibilities

State 1	State 2	shock wave speed w (km/h)
A	B	3.8
A	C	80
D	C	80
B	D	-16
A	D	80

The demand is the same as in the previous example, so state A is the same. Downstream of the moving bottleneck there is a free flow traffic state (it is downstream of the bottleneck, so it is free flow). The flow is given at 1000 veh/h, and since it is in free flow, the speed is 80 km/h. Hence, the density is $k_C = \frac{q_C}{u_C} = \frac{1000}{80} = 12.5$ veh/km.

Since the demand is higher than the capacity of the moving bottleneck, upstream of the bottleneck, a congested state occurs. It is separated from state C by a shock wave which moves with the speed of the moving bottleneck (it is the moving bottleneck). This means we have to find state B in the fundamental diagram which connects to state C with a line with a slope of 10 km/h; this line is indicated by q_1 (equation 5.24). Furthermore, state B has to lie on the congested branch of the fundamental diagram, indicated by q_2 (equation 5.25). The position upstream of the moving bottleneck can be determined by the intersection of two lines:

$$q_1 = q_C + v(k - k_C) \quad (5.24)$$

$$q_2 = q_D + w(k - k_c) \quad (5.25)$$

We find the density for state B by $q_1 = q_2$. This results in $k_B = 243$ veh/km. The matching flow can be found by substituting this into equation 5.24 or equation 5.25, leading to $q_B = 3307$ veh/h.

The shock wave speeds between B and C, as well as the shock wave speed between A and B can be calculated using the shock wave equation, equation 5.9:

$$w_{BC} = \frac{q_B - q_C}{k_B - k_C} = \frac{3307 - 1000}{243 - 12.5} = 10 \text{ km/h} \quad (5.26)$$

$$w_{AB} = \frac{q_A - q_B}{k_A - k_B} = \frac{2500 - 3307}{31.25 - 243} = 3.8 \text{ km/h} \quad (5.27)$$

Note that the shock wave between B and C moves with the speed of the moving bottleneck.

Once the moving bottleneck leaves the road, the method is exactly the same as in the previous example. The queued vehicles exit state B at the road capacity, state D with a flow 6000 veh/h and a speed of 80 km/h. The shock wave between state D and B moves backward with a speed which can be calculated by the shock wave equation. The shock wave speed must also be equal to the wave speed of the fundamental diagram, so using the knowledge of the previous example, we find $w_{BD} = -16$ km/h.

5.2.4 Example 3: moving truck and high demand

Consider a three lane road, where at all three lanes a triangular fundamental diagram holds. The capacity is 2000 veh/h/lane, the free flow speed 80 km/h and the jam density 150 veh/km. The demand is increased to 4500 veh/h. A truck enters the road at $t=0.5$ h and $x=10$ km, and leaves the road at $t=1$ h and $x=15$ km, hence driving 10 km/h, limiting the flow downstream of the moving bottleneck to 1000 veh/h. What are the conditions on the road?

The states and fundamental diagram, as well as the resulting traffic states are shown in figures 5.7(a) and 5.7(b) respectively. Tables 5.9 and 5.10 give the properties of the states and the shock waves respectively. This situation is very similar to the situation described in example 2 (section 5.2.3). Below, we will comment on the similarities and differences.

The downstream part is the same. States A and C, as well as the congested state upstream of the moving bottleneck are determined by the properties of the moving bottleneck, and are thus the same as in the previous example. The speed of the wave between state A and B differs, since state A is different. The speed can be calculated using the shock wave equation, equation 5.9:

$$w_{AB} = \frac{q_A - q_B}{k_A - k_B} = \frac{4500 - 3307}{56.25 - 243} = -6.3 \text{ km/h} \quad (5.28)$$

So, the methodology to compute the shock wave speed is the same. However, the phenomenon is different: contrary to the previous example, the shock wave moves upstream.

When the moving bottleneck leaves the road, the queue discharge (capacity) state D is also the same as in the previous example. Since states B and D are the same, the shock wave speed between the two is also the same. Also the shock wave speed between state A and D is the same, because both points are at the free flow branch of the fundamental diagram, hence the shock wave speed is the speed of the free flow branch of the (triangular) fundamental diagram.

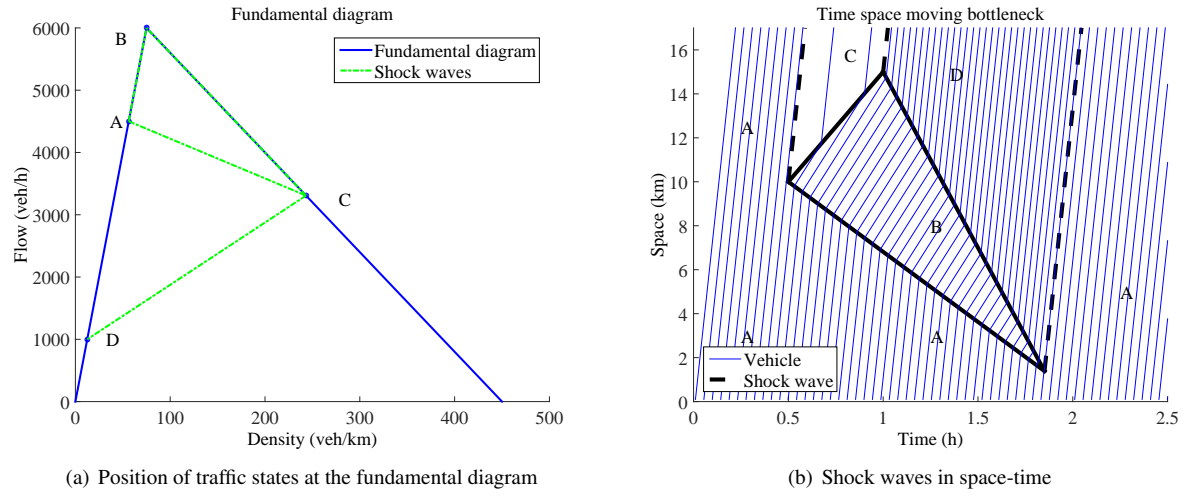


Figure 5.7: The situation for the moving bottleneck with overtaking opportunities and a high demand.

Table 5.9: The states on the road for the moving bottleneck with overtaking opportunities and a high demand.

State	Flow (veh/h)	Density(veh/km)	Speed (km/h)
A	4500	56.25	80
B	3077	243	13.6
C	1000	12.5	80
D	6000	75	80

Table 5.10: The shock waves present on the road for the moving bottleneck with overtaking opportunities and a high demand

State 1	State 2	shock wave speed w (km/h)
A	B	-6.3
A	C	80
B	C	10
D	C	80
B	D	-16
A	D	80

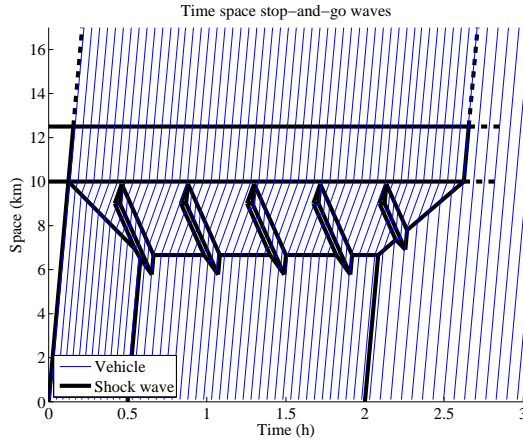


Figure 5.8: Stop and go waves in time and space

5.3 Stop and go waves

On motorways, often so called stop-and-go waves occur. These short traffic jams start from local instabilities, and the speed (end flow) in the stop-and-go waves is almost zero. For a more detailed explanation, see section 7.3. Now the speed of the boundaries of the traffic states are known, we can apply this to stop-and-go waves, and understand why this typical pattern arises (figure 5.8).

The stop-and-go waves arise in dense traffic. The traffic demand is then mostly near capacity, or at approximately the level of the queue discharge rate. The upstream boundary of such a shock moves upstream. When it is in congested conditions, both the upstream state (the congested condition) and the downstream state (the standing traffic) are congested, hence the upstream boundary moves backwards with a speed equal to the wave speed of the fundamental diagram. Once it gets out of congestion, the inflow is most likely approximately equal to the capacity of the road. That means that the upstream boundary moves with a speed which is equal to the slope of the line in the fundamental diagram connecting the capacity point with the point of jam density, which is the wave speed.

The downstream boundary separates the jam state (standing traffic) with capacity (by default: vehicles are waiting to get out of the jam, hence a capacity state occurs). The speed between these two states is found by connecting the points in the fundamental diagram. The resulting speed is the wave speed of the fundamental diagram.

After the first stop-and-go wave has moved upstream, the inflow in the second stop-and-go wave equals the outflow of the first stop-and-go wave. These are the upstream respectively the downstream state of the second wave, which thus are the same. In between, within the wave, there is another, jammed state. According to shock wave theory the shock between state A and B (i.e., the upstream state and the state within the stop-and-go wave) and the shock between B and A (i.e. the state within the stop-and-go wave and the downstream state, which equals the upstream state) is the same. This speed is approximately equal for all roads, 15-20 km/h (Schreiter et al., 2010). Hence, the length of the stop-and-go wave remains the same.

This way, stop-and-go waves can travel long distances upstream. Section 7.4 will discuss the stop-and-go waves and their characteristics in more detail.

Selected problems

For this chapter, consider problems: A.1.4, A.2.6, 67, 72, A.3.4, A.4.4, 101, 102, A.5.4, A.6.3, A.7.4, A.8.3, A.8.4, A.9.3, 260

Chapter 6

Method of characteristics

The kinematic wave model provides a relatively simple approach to reproduce and predict the spatio-temporal characteristics of traffic congestion by means of a macroscopic model, either by simulation (numerical solution approaches) or, as we will discuss in this chapter, analytically. The so-called *method of characteristics* (MoC) is a well known solution method for partial differential equations.

The kinematic wave model is, however, a bit special. Since in many cases, the kinematic wave model does not have a classical solution (solutions which are continuously differentiable) due to the occurrence of shocks. As a result, we will look for so-called *generalised solutions* (weak solutions that are piece-wise continuously differentiable). However, since there are an infinite number of generalised solutions, we will have to look for a special solution which satisfies the *entropy condition* (i.e. local maximisation of the flow).

This chapter describes the MoC approach to determine solutions of the kinematic wave model. We will start with briefly explaining the general concept and the mathematics. Then, section 6.2 will show two examples.

6.1 Mathematical construction

This section first describes the construction of the curves, then applies the theory to a road with no entering and exiting traffic Section 6.1.3 gives the interpretation.

6.1.1 Construction

Let us consider the kinematic wave model:

$$\frac{\partial k}{\partial t} + \frac{\partial q}{\partial x} = r - s \quad (6.1)$$

where $k = k(t, x)$ denotes the density, $q = q(t, x)$ denotes the flow and r and s denote the source and sink terms. We furthermore have:

$$q = Q(k, t, x) \quad (6.2)$$

Note that we allow spatial and temporal fluctuations in the fundamental diagram.

Now suppose that we know the traffic conditions (i.e. the traffic density) for a boundary \mathcal{B} in the (t, x) plane. These can either reflect initial conditions (e.g. the density on the road at some initial time $t = t_0$), boundary conditions (inflow into the considered roadway section; outflow restrictions), etc.

Together with the boundary conditions, the kinematic wave model can be used to determine the traffic conditions influence by the traffic conditions described in at the boundary \mathcal{B} (see figure 6.1).

The idea of the method of characteristics is to transform the kinematic wave model (which is a partial differential equation) into a set of ordinary differential equations, which can be solved with standard techniques. To see how to do this, we fill in Eq. (6.2) into Eq. (6.1) yielding:

$$\frac{\partial k}{\partial t} + \frac{\partial Q}{\partial k} \frac{\partial k}{\partial x} = \frac{\partial k}{\partial t} + c \frac{\partial k}{\partial x} = r - s - \frac{\partial Q}{\partial x} \quad (6.3)$$

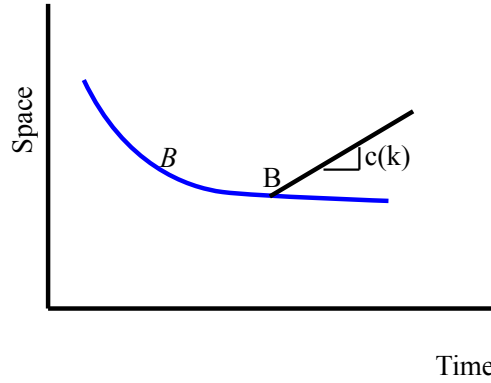


Figure 6.1: A boundary with known traffic states in the space-time diagram, and a characteristic curve

Note that $c = c(k, t, x) = \frac{\partial Q}{\partial k}$ is the slope of the fundamental diagram at (t, x) , describing the speed of a very small shock (a so-called kinematic wave).

Let us now consider a point B on the boundary \mathcal{B} . This point (t_B, x_B) describes the initial point of the characteristic curve. Next to the initial point, the curve is defined by its slope, which is by definition equal to the kinematic wave speed $c = c(k, t, x)$ (see figure 6.1. This gives us the following expression:

$$\frac{dx}{dt} = c(k, t, x) \quad (6.4)$$

with:

$$x(t_B) = x_B \quad (6.5)$$

Note that on the boundary we know the density k . If we are able to determine the change in the density along the characteristic from that point onward, we can determine the density along the characteristic. That is, we want to establish $\frac{dk}{dt}$. We get:

$$\frac{dk}{dt} = \frac{\partial k}{\partial t} + \frac{\partial k}{\partial x} \frac{dx}{dt} \quad (6.6)$$

Since along the characteristic, we have $\frac{dx}{dt} = c$, we can rewrite:

$$\frac{dk}{dt} = \frac{\partial k}{\partial t} + c \frac{\partial k}{\partial x} = r - s - \frac{\partial Q}{\partial x} \quad (6.7)$$

with initial condition $k(t_B, x_B) = k_B$ given. This ordinary differential equation shows how the density changes along the characteristic. Considering all characteristics emanating from the boundary should allow us to construct the density everywhere within the interior of the boundary, at least at all points where the density is determined by the conditions in the boundary (so-called region of influence of \mathcal{B}).

6.1.2 Application to homogeneous roads

To further our results, let us now consider a homogeneous road, i.e. $Q(k, t, x) = Q(k)$. Furthermore, no traffic enters or exits the road. In this case, Eq. (6.7) becomes:

$$\frac{dk}{dt} = 0 \quad (6.8)$$

This means that the derivative of the density along the characteristic is equal to 0, i.e. the density is constant along the characteristic. Since $k(t_B, x_B) = k_B$, along the entire characteristic we have $k(t, x) = k_B$. In other words, the density is conserved along the characteristic curve.

Furthermore, the density is constant along the curve, so the kinematic wave speed is $c = c(k) = \frac{\partial Q}{\partial k}$. Since by definition the characteristic curve satisfies $\frac{dx}{dt} = c$, the slope of the curve is under these conditions constant meaning that the curve is in fact a straight line.

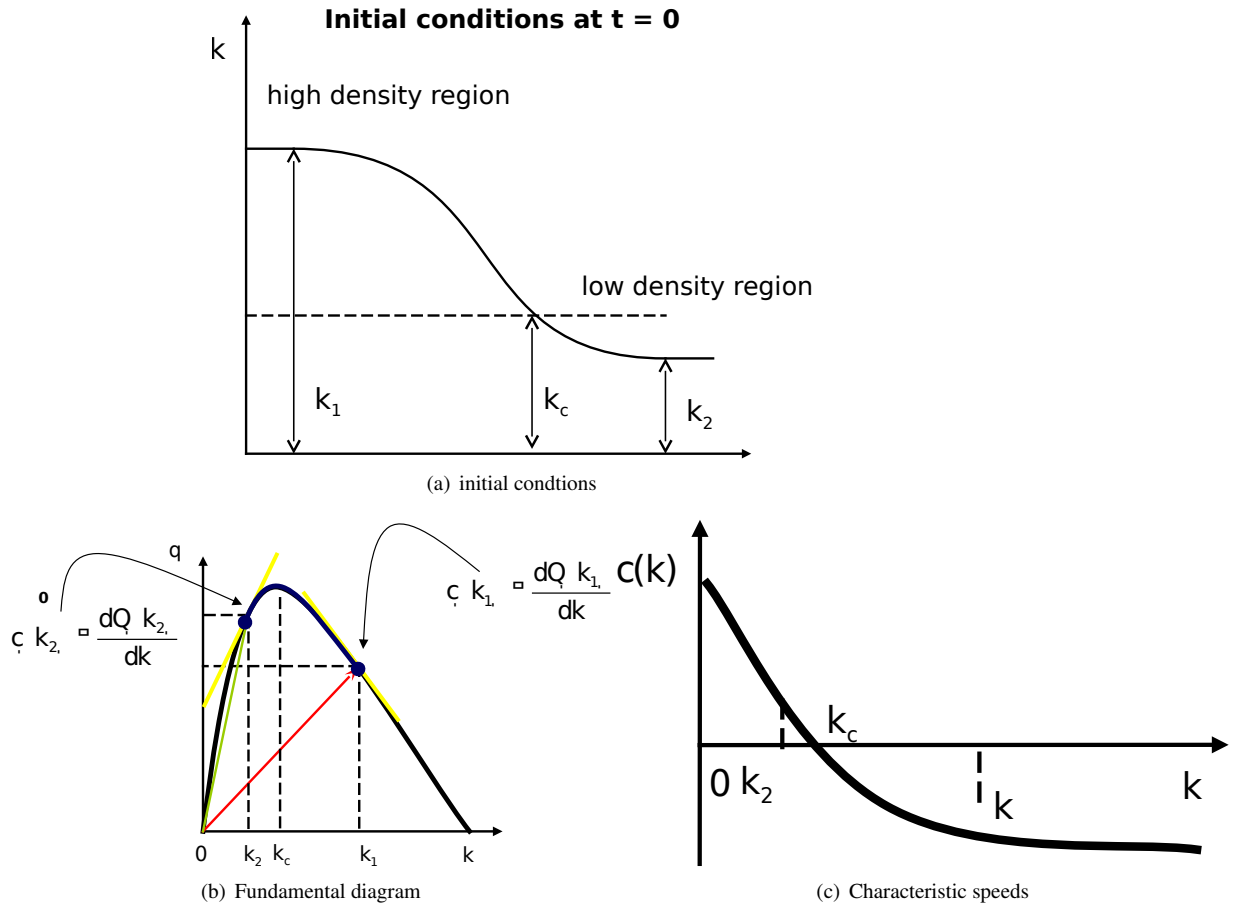


Figure 6.2: Traffic states and their characteristic speeds for an acceleration fan

6.1.3 Interpretation

The consequence from the mathematics described in section 6.1.1 is that traffic states always propagate on lines in space-time moving with the speed of the derivative of the fundamental diagram. This makes the construction of the characteristics very simple, and the characteristics can be used to track back or forward traffic conditions in space and time.

6.2 Application

Let us now see an application of the method of characteristics in the prediction of traffic conditions. For this case, we will take the boundary \mathcal{B} to be the initial conditions on an infinite length roadway section. Two cases will be considered here: the first one where traffic is dense upstream and in low density downstream (e.g., the moment a traffic light turns to green). Also the different situation is considered, where traffic upstream is in a low density condition and traffic downstream is in a high density condition.

6.2.1 Acceleration fan

Consider a situation where upstream traffic is in an overcritical state (i.e., density is higher than the critical density) and downstream the traffic is in an undercritical state, see figure 6.2(a). The characteristic speeds depend on the traffic density. For a concave fundamental diagram (see figure 6.2(b)) they are sketched in figure 6.2(c).

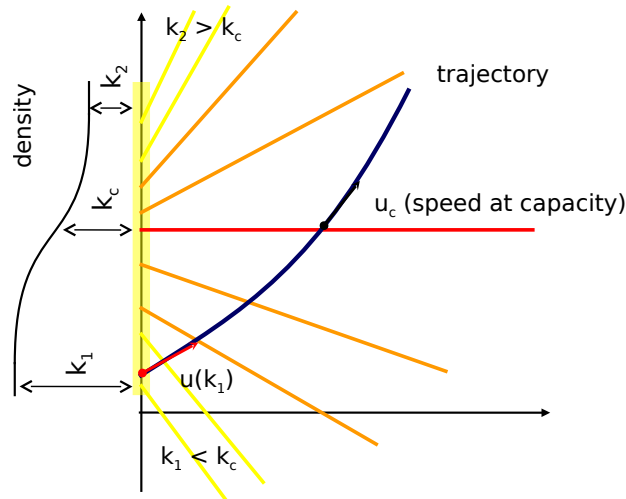


Figure 6.3: The kinematic waves (or characteristic curves) for an traffic situation where the upstream traffic state is overcritical and the downstream traffic state is undercritical

For each of the states at the initial position the density is determined. For that density, the characteristic speed is determined, i.e., the derivative of the fundamental diagram at that density. Note once more that these speed are not the speeds of the vehicles in that traffic state. Figure 6.2(c) sketches the characteristic speed. The traffic states now propagate with that speed. This means that states in the free flow condition propagate in the forward direction, whereas congested traffic states move in the backward direction. The capacity state moves at a speed zero, so remains at the same location.

The characteristic curves and their speeds are shown in figure 6.3. Due to the concavity of the fundamental diagram, these lines spread out. The area over which the density changes hence take place increases. Because the lines are straight, the increase is linear over time. Because of the pattern, this phenomenon is also called an acceleration fan.

Note that the analysis here is based on a concave fundamental diagram. If a triangular fundamental diagram would be used, one might argue there are only two waves: one moving forward with the free flow speed and one moving backward with the wave speed. This would leave a void in conditions at the area in between these waves. It is better to consider a triangular fundamental diagram as a continuously differentiable fundamental diagram which happens to change curvature very slowly on the branches and very quickly at the top. In that case, the same analysis can be done.

In case of a traffic light, the density drop can be sudden, where upstream of the traffic light the traffic is in jam density and downstream the road is empty. Then, this could be approximated by a smooth curve with a very sharp decrease of density with an increase of space at the stop line. Then, one could apply the same analysis, yielding the same characteristic curves expanding, now all from the location of the stop line.

6.2.2 Deceleration

A similar construction can be made for a deceleration wave. The difference is that in this case the upstream traffic states have a higher density than the downstream ones. The traffic states with higher densities, in this case the downstream states, have lower characteristic speeds (see figure 6.2(b)). See figure 6.4 shows the characteristics in space time. In case of a deceleration, the upstream characteristics travel faster than the downstream characteristics, leading to intersecting characteristics. Since each characteristic curve represent a traffic state, crossing characteristics would mean having two traffic states at the same place at the same time.

If the characteristics cross, one has to revert to shockwave theory. Each of the characteristics indicates a certain traffic state. If these two traffic states meet, one has a shock for which the speed is known (see section 5).

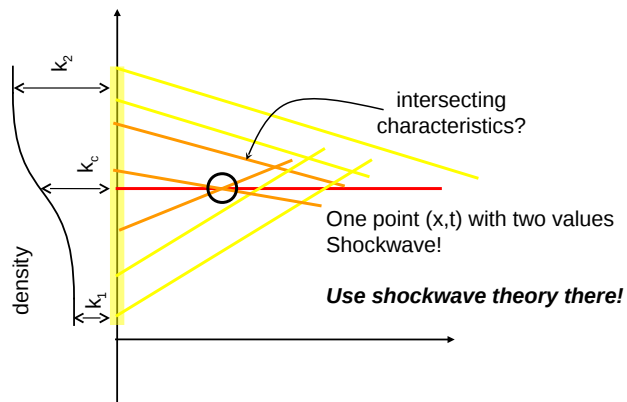


Figure 6.4: Illustration of the characteristics in space-time for an deceleration

Selected problems

For this chapter, consider problems: 145, 146, 147, 217

Chapter 7

Traffic states and Phenomena

This chapter discusses some of the important phenomena in traffic.

7.1 Stability

In traffic, we can differentiate between three levels of stability: local, platoon, and traffic. This is indicated in table 7.1, and shown graphically in figure 7.1.

Table 7.1: Identification scheme for different levels of stability

Name	relevant vehicles	criterion
Local	One vehicle pair	Does the follower relax into a steady state speed after a speed change of the leader?
Platoon	A platoon of vehicles	Does the change of speed of a leader increase over the vehicle number in the platoon?
Traffic	More than one platoon	Does the speed disturbance propagate to the next platoon?

7.1.1 Local stability

For local stability, one has to consider one vehicle pair, in which the second vehicle is following the leader. If the leader reduces speed, the follower needs to react. In case of local stability, he does so gracefully and relaxes into a new state. Some car following models in combination with particular parameter settings will cause the following vehicle to continuously change speeds. The following vehicle then has oscillatory speed with increasing amplitude. This is not realistic in real life traffic.

7.1.2 Platoon stability

For a platoon, it should be considered how a change of speed propagates through a platoon. This is called platoon stability or string stability. Consider a small change in speed for the platoon leader. The following vehicle needs to react (all vehicles in the platoon are in car-following mode). Platoon stability is whether the speed disruption will grow over the vehicle number in the platoon. In platoon stable traffic, the disruption will reduce, in platoon unstable traffic, this disruption will grow.

Note that platoon stability becomes only relevant to study for locally stable traffic. For locally stable traffic, one can have platoon instability if for a single vehicle the oscillations decrease over time, but they increase over the vehicle number, as shown in figure 7.1.

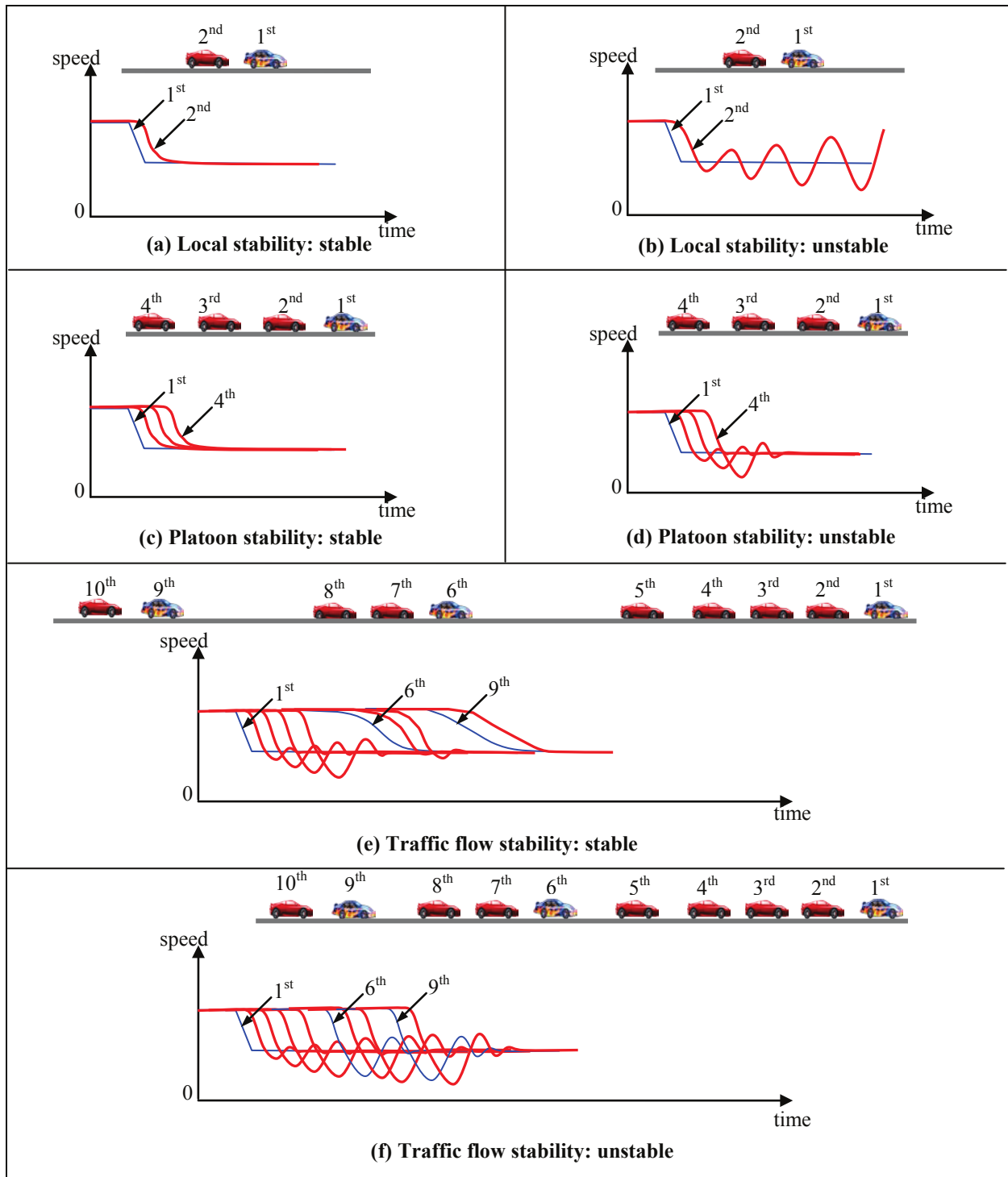


Figure 7.1: Graphical view of the three different types of stability. The graphs show the speeds as function of time for different vehicles. Figure from Pueboobpaphan and van Arem (2010)

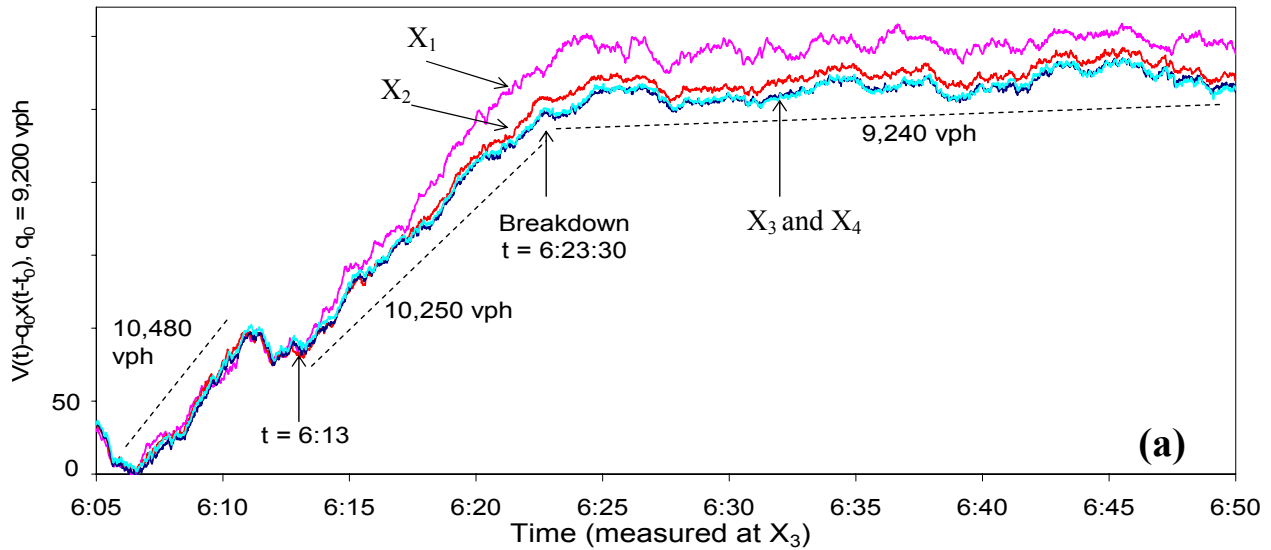


Figure 7.2: Example of an analysis with slanted cumulative curves, from Cassidy and Rudjanakanoknad (2005)

7.1.3 Traffic flow stability

The third type of stability is traffic flow stability. This indicates whether a traffic stream is stable. For the other types of stabilities, we have seen that stability is judged by the speed profile of another vehicle. For traffic flow stability it matters whether a change in speed of a vehicle will increase over a long time to any vehicle, even exceeding the platoon boundary. Traffic which is platoon stable is always traffic stable. The other way around, platoon unstable traffic is not always traffic unstable. It could happen that the unstable platoons are separated by gaps which are large enough to absorb disruptions. In this case, the traffic flow is stable, but the platoons are not. If the disruption propagates to other platoons, the traffic flow is unstable.

7.1.4 Use of stability analysis

There are mathematical tools to check analytically how disruptions are transmitted if a continuous car-following model is provided. For platoon stability this is not very realistic since all drivers drive differently. Therefore an analytical descriptions should be taken with care if used to describe traffic since one cannot assume all drivers to drive the same. In fact, driver heterogeneity has a large impact on stability. The other way around, the stability analysis could indicate whether a car-following model is realistic.

From data, one knows that traffic is locally stable and mostly platoon unstable. Depending on the traffic flows, it can be traffic unstable or stable. For large number of vehicles, traffic is generally stable (otherwise, there would be an accident for any speed disruption).

7.2 Capacity drop

7.2.1 Phenomenon description

The capacity drop is a phenomenon that the maximum flow over a bottleneck is larger before congestion sets in than afterwards. That is, once the bottleneck is active, i.e. there is a congested state upstream of the bottleneck and no influence from bottlenecks further downstream, the traffic flow is lower. This flow is called the queue discharge rate, or sometimes the outflow capacity.

The best way to analyse this is by slanted cumulative curves. Generally, the flow during congestion would be the same. That is, the queue outflow does not depend on the length of the queue. Therefore, a natural way to offset the

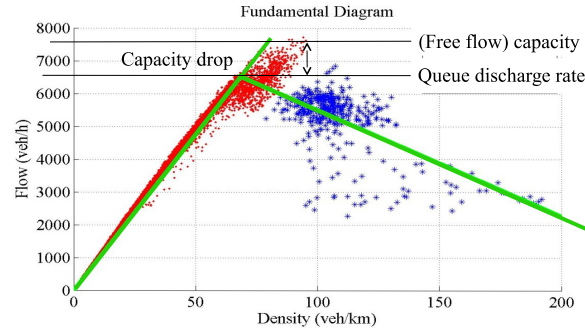


Figure 7.3: Illustration of the capacity drop in the fundamental diagram using real-world data

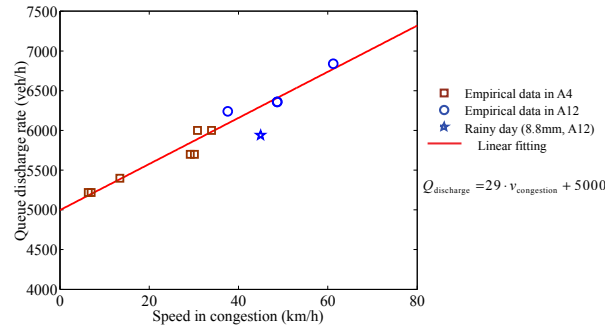


Figure 7.4: The dependency of the queue discharge rate of the speed in the queue (from Yuan et al. (2015a))

cumulative curves is by the flow observed during discharging conditions. One would observe an increasing value before congestion sets in.

In the fundamental diagram, one would then observe a congested branch which will not reach the capacity point. Instead, one has a lower congested branch, for instance the inverse lambda fundamental diagram. The capacity drop is the difference between the free flow capacity and the queue discharge rate. This is shown in figure 7.3.

7.2.2 Empirics (from Yuan et al. (2015a))

Capacity with congestion upstream is lower than the possible maximum flow. This capacity drop phenomenon has been empirically observed for decades. Those observations point out that the range of capacity drop, difference between the bottleneck capacity and the queue discharging rate, can vary in a wide range. Hall and Agyemang-Duah (1991) report a drop of around 6% on empirical data analysis. Cassidy and Bertini (1999) place the drop ranging from 8% to 10%. Srivastava and Geroliminis (2013) observe that the capacity falls by approximately 15% at an on-ramp bottleneck. Chung et al. (2007) present a few empirical observations of capacity drop from 3% to 18% at three active bottlenecks. Excluding the influences of light rain, they show at the same location the capacity drop can range from 8% to 18%. Cassidy and Rudjanakanoknad (2005) observe capacity drop ranging from 8.3% to 14.7%. Oh and Yeo (2012) collect empirical observations of capacity drop in nearly all previous research before 2008. The drop ranges from 3% up to 18%. The large drop of capacity reduces the performance of road network.

In most of observations, capacity drop at one bottleneck only exhibits a small day to day deviation (Chung et al., 2007; Cassidy and Bertini, 1999). However, it is possible to observe a large difference in the capacity drop empirically at the same location. Srivastava and Geroliminis (2013) observe two different capacity drop, around 15% and 8%, at the same on-ramp bottleneck. Yuan et al. (2) observe different discharging flows at the same freeway section with a lane-drop bottleneck upstream and estimate the outflow of congestion in three-lane section ranging from 5400 vph to 6040 vph. All of these studies show that the capacity drop can be controlled and some strategies have been described to reach the goal (Chung et al., 2007; Carlson et al., 2010; Cassidy and Rudjanakanoknad, 2005). Those control

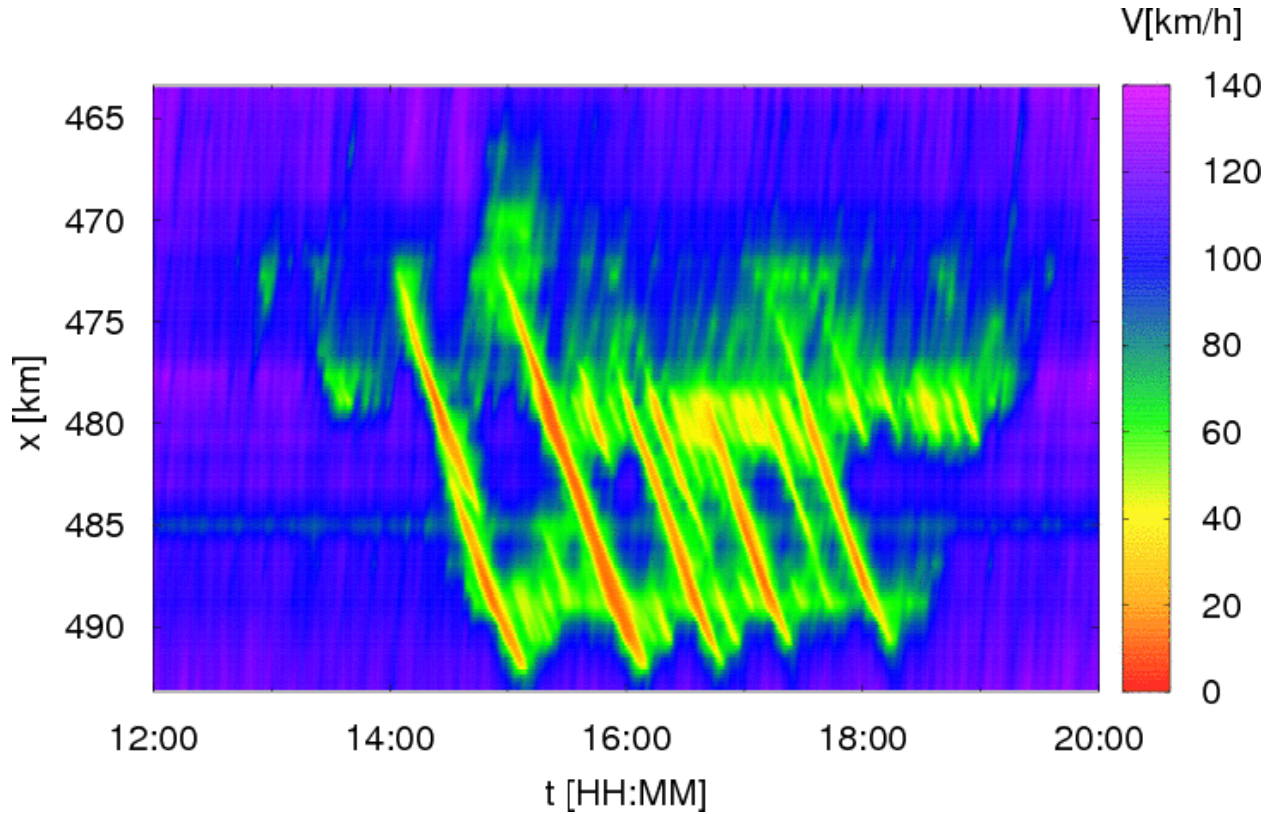


Figure 7.5: Space-time plot of the traffic operations of the German A5, 14 October 2001 – figure from traffic-states.com

strategies strongly rely on the relation between the congestion and the capacity drop.

Recent research Yuan et al. (2015a) clearly shows this relationship with speed, see figure 7.4.

The main cause of the capacity drop is not identified yet. Some argue it is lane changing, others argue it is the limited acceleration (not instantaneous), whereas others argue it is the *difference* in acceleration (not all the same). This remains an active field of research, both for causes of the capacity drop and for ways to control it.

7.3 Stop-and-go wave

7.3.1 Phenomenon description

Stop-and-go waves are a specific type of traffic jams. Generally, all traffic states at the congested branch are considered congested states. Sometimes traffic experiences short so-called stop-and-go waves. In these short traffic jams, vehicles come to (almost) a complete standstill. The duration of the queues is a few minutes. At the downstream end of the jam, there is no physical bottleneck. For many drivers, it is surprising they have been in the queue “for no obvious reason”.

The outflow of these stop-and-go waves is at the point of the queue discharge rate. Since the traffic in the jam is at almost standstill, the density in the stop-and-go wave is jam density. The speed at which the head moves, can be determined with shock wave theory. Using the fact that the wave speed is the difference in flow divided by the difference in density, we find that the head propagates backward with the wave speed (the slope of the congested branch of the fundamental diagram).

These short jams usually start in congestion. Only if traffic is unstable, short disturbances can grow to jams. In free traffic, the spacing between platoons is usually large enough to ensure these jams do not grow. That means that upstream of the stop-and-go wave, traffic conditions are probably close to capacity. A similar traffic state upstream

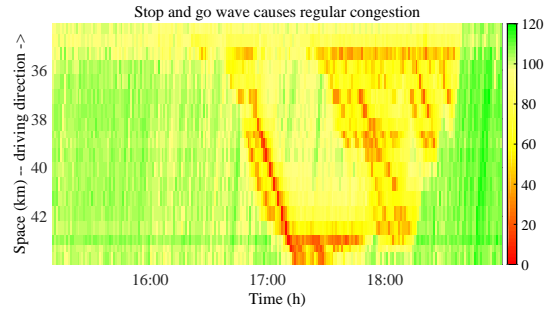


Figure 7.6: Example of a stop-and-go wave triggering a standing queue at the A4 motorway

and downstream of the stop-and-go wave means that the upstream and downstream boundary move at the same speed. Therefore, the jam keeps its length.

Often, these type of jams occur regularly, with intervals in the order of 10 minutes. Then, the outflow of the first stop-and-go wave (queue discharge rate) is the inflow of the second one. Then, the upstream and downstream boundary must move at the same speed. Hence, the jams move parallel in a space-time figure – see also figure 7.5.

Since traffic in the jam is (almost) at standstill, no flow is possible. That means that the upstream boundary must continue propagating backwards through a bottleneck – the inflow keeps at the same level and the vehicles which join the queue have no choice but join the queue keeping their desired jam spacing to their predecessor. Once the jam passes the bottleneck, the desired outflow would be the queue discharge rate of the section where the congestion is. However, the capacity of the bottleneck might be lower.

In such a case, the stop-and-go wave triggers a standing congestion, as is seen in figure 7.6. A stop-and-go wave propagates past a bottleneck near location 43 km. The outflow of the stop-and-go wave would be larger, but now the flow is limited. Between the stop-and-go wave and the bottleneck, a congested state occurs, of which the flow equals the flow through the bottleneck (a localised bottleneck, so at both sides the same flow). This congested state is at the fundamental diagram. For most applications where the congested branch of the fundamental diagram is considered a straight line, this congested state will lie on the line connecting the queue discharge point with the jam density. The speed of the downstream boundary of the stop-and-go wave is now determined by the slope of the line connecting the “stopped” jam state with the new congestion state. Since these are all on the same line, the speed is the same, and the stop-and-go wave continues propagating.

7.4 Kerner’s Three Phase Traffic Flow Theory

In the first decade of this century, the number of traffic states were debated. Kerner (2004) claimed that there would be three states (free flow, congested, and synchronised). He claimed that all other theories, using two branches of the fundamental diagram – a free flow branch and a congested branch – assumed two states. This led to a hefty scientific debate, of which the most clear objections are presented by Treiber et al. (2000) and Helbing et al. (1999). A main criticism of them is that the states are not clearly distinguished. Whereas most scientists now agree that three phase traffic flow theory is not a fully correct description of traffic flow, it includes some features which are observed in traffic. In order to discuss these features and introduce name giving for them, the theory is included in the course. This reader provides a short description for each of the states: an interested reader is referred to Kerner’s book for full information (Kerner, 2004), or the wikipedia entry on three phase traffic flow theory for more concise information.

7.4.1 States

Kerner argues there are three different states: free flow, synchronized flow and wide moving jams.

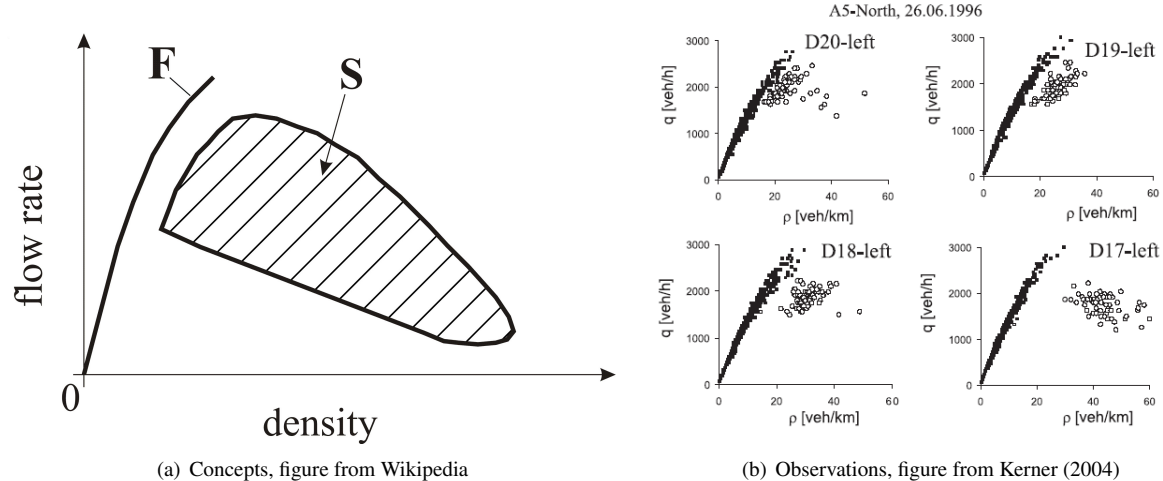


Figure 7.7: Synchronized flow

Free flow

In free flow traffic, vehicles are not (much) influenced by each other and can move freely. In multi-lane traffic, this means that vehicles can freely overtake. Note that as consequence, the traffic in the left lane is faster than the traffic in the right lane. The description of Kerner's free flow state therefore has similarities with the description of the two-pipe regime in Daganzo's theory of slugs and rabbits.

Synchronized flow

Synchronized flow is found in multi-lane traffic and is characterized by the fact that the speeds in both lanes become equal – hence the name of the state: the speeds are “synchronized”. This could be seen similar to the one-pipe regime of Daganzo.

In Kerner's three phase traffic flow theory this is one of the congested states, the other one being wide moving jams. The characterising difference between the two is that in synchronised flow, the vehicles are moving at a (possibly high) speed, whereas in wide moving jams, they are al (almost) standstill. Kerner attributes several characteristics to the synchronized flow:

1. Speeds in all lanes are equal
2. Speeds can be high
3. The flow can be high – possibly higher than the maximum free flow speed. Note that in this case, the “capacity” of the road is found in the synchronized flow.
4. (Important) there is an area, rather than a line, of traffic states in the fundamental diagram.

The area indicated by an “S” in figure 7.7(a) is the area where traffic states with synchronised flow can be found. Note that in the figure, the free flow branch (“F”) does not extend beyond the maximum flow. However, note that for a certain density, various flows are possible. The explanation by Kerner is that drivers have different equilibrium speeds, leading to different flows.

Wide moving jams

A wide moving jam is most similar to what is more often called a “stop and go wave”. Stop-and-go relates to the movement an individual vehicle makes: it stops (briefly, in the order of 1-2 minutes), and then sets off again. Kerner

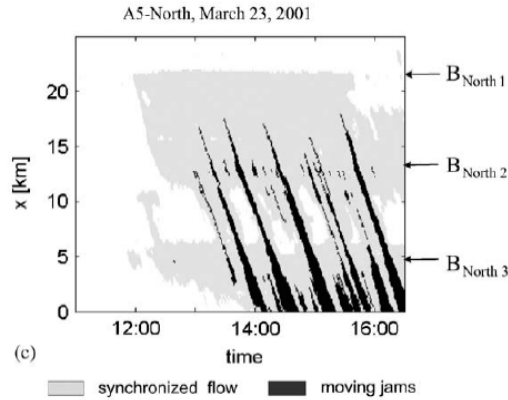


Figure 7.8: Observations of wide moving jams propagating through synchronised flow; figure from Kerner (2004)

relates the name to the pattern (it moves in the opposite direction of the traffic stream), and “wide” is related to the width (or more accurately, it would be called length: the distance from the tail to the head) of the queue compared to the acceleration/deceleration zones surrounding the jam. The speed in the jam is (almost) 0. In the flow-density plan, the traffic state is hence found at flow (almost) 0 and jam density.

By consequence hence the tail moves upstream with every vehicle attaching to the jam. The head also moves upstream, since the vehicles drive off from the front. Hence the pattern of the jam moves upstream. This phenomenon is purely based on the low flow inside the jam, hence it can travel upstream for long distances (dozens of kilometers). It can pass through areas of synchronised flow, and pass on and off ramps, see figure 7.8

7.4.2 Transitions

The other aspect in which Kerner’s theory deviates from the traditional view, is the transitions between the states. Kerner argues there are probabilities to go from the free flow to the synchronized flow and from synchronized flow to wide moving jams. These probabilities depend on the density, and are related to the size of a disturbance.

Let’s consider the transition from free flow to synchronized flow as an example. As the density approaches higher densities, the perturbation which is needed to move into another state, is reducing (since the propagation and amplification increases). One can draw the minimum size of an disturbance which changes the traffic state as function of the density, see figure 7.9. Besides, one also knows with which probability these disturbances occur. Hence, one can describe with what probability a phase transition occurs, see figure 7.9.

Selected problems

For this chapter, consider problems: A.1.2, 12-13, 25, 30, 31, A.2.2, 64, 99, 107, 108, 109 110, A.5.1, A.5.2, 153, 161, 183, 180, 192, 193, 190, 219, 244, 245, A.10.2

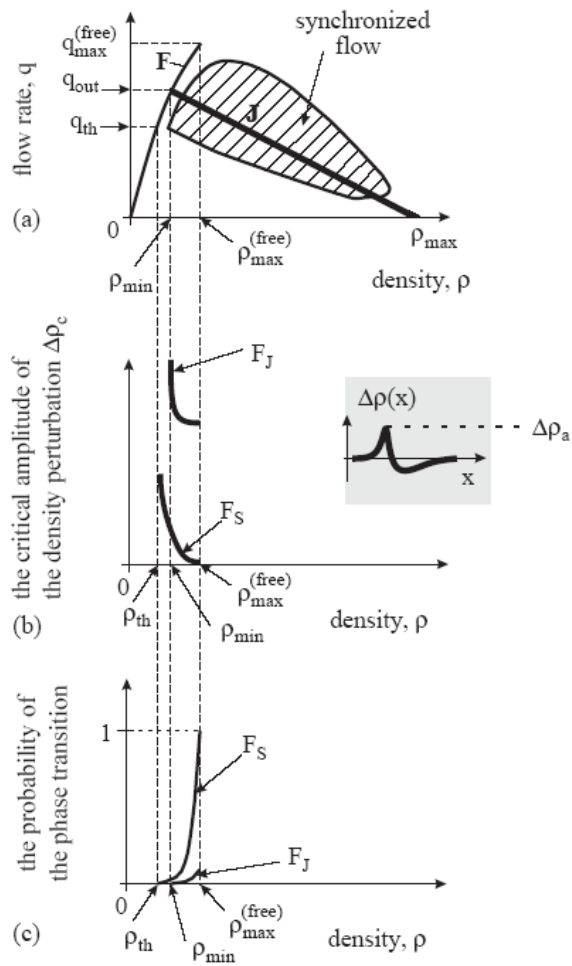


Figure 7.9: Transitions between the phases, figure from Kerner (2004)

Chapter 8

Car-following

A car following model describes the lateral action of the vehicle as function of it's leader(s). That can be, it describes its position, speed or acceleration. There are many different forms, and all have their advantages and disadvantages. They all aim to describe driving behavior, and human behavior is inconsistent and hence difficult to capture in models.

This chapter does not give an overview of all models, nor an historical overview. That is given by Brackstone and McDonald (1999). Instead, in this chapter we discuss the simplest, Newell's, and discuss some characteristics which one might include.

8.1 Newell's car following model

The most easy car-following model is the model presented by Newell (2002). It prescribes the position of the following x_{i+1} car as function of the position of the leader x_i . The model simply states that the of the follower is a distance s_j upstream of the position of the leader of a time τ earlier

$$x_{i+1}(t) = x_i(t - \tau) - s_j \quad (8.1)$$

This means that the follower's trajectory is a copy of the leader's trajectory, translated over a vector $\{\tau, s_j\}$ in the xt -plane (see figure 8.1). This vector has also a direction, which can be computed by dividing its vertical component over the horizontal component.

$$w = \frac{s_j}{\tau} \quad (8.2)$$

This slope is the speed at which information travels backward in congested conditions, and hence is the slope of the congested branch of the fundamental diagram.

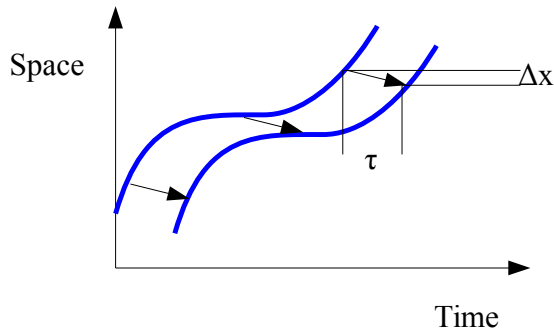


Figure 8.1: Newell's car-following model is translating a leader's trajectory over a vector $\{\tau, s_j\}$

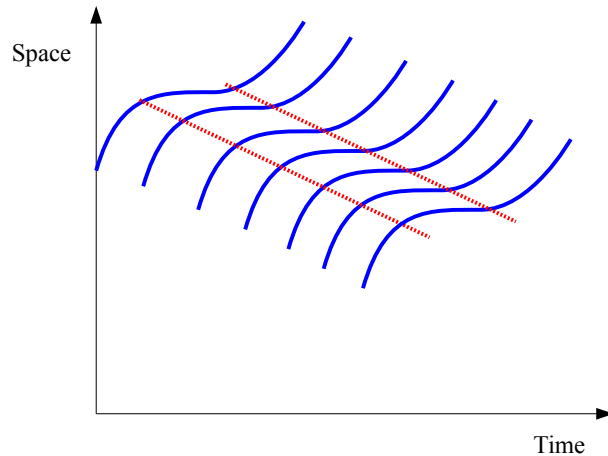


Figure 8.2: The average of the car-following behavior of drivers each with different parameters of the newell model leads to a shock wave speed

For each driver, different values for τ and s_j can be found. From empirical analysis Chiabaut et al. (2010) it is shown that averaging the slopes over more than 12 drivers would yield a constant shock wave speed. This is illustrated in figure 8.2. Although the parameters of the car-following model are all different, there is an average translation of the disturbance, indicated by the red dotted line.

8.2 Characteristics

8.2.1 Dependencies

The car-following model describes the action of the following vehicle. That of course can depend on the movement of the leading vehicle. Some elements which are often included in a car-following model are:

- Acceleration of the leader: if the leader accelerates, the follower can get closer
- Speed: a higher speed would require a longer spacing
- Speed difference: if a follower is approaching his predecessor at a high speed, he needs to brake in time
- Spacing: if the spacing is large, he might (i) accelerate and/or (ii) be less influenced by its leader
- Desired speed: (i) the faster he wants to go, the more his desire to close a gap. But also (ii) even if the predecessor is far away, the follower will not exceed its desired speed

All these elements occur in car-following models. This list combines elements used for different type of models. For instance, some models might prescribe a distance, and hence use speed as input, whereas others might prescribe a speed, and use distance as input.

Surprisingly, many of the available car-following models are “incomplete”, i.e. they lack one or more of the above elements and are therefore limited in their use. Using them for a dedicated task is of course allowable. A user should ensure that the model is suited for the task.

8.2.2 Reaction time

Human drivers have a reaction time. Mostly, the models are evaluated at time steps, which are chosen small, often in the order of 0.1 second. A good model allows to set the reaction time of the driver separately. Then, only information which is more than a reaction time earlier can influence a driver's acceleration.

Some models will use the model time step as reaction time. In that case the speed or acceleration of the model is evaluated every time step, which then is typically 1 second. Information of the previous time step is immediately used in the next time step, and in between there are no accelerations considered. The effect of reaction time on the traffic flow is described in Treiber et al. (2006). Generally speaking, a large reaction time can make the traffic flow unstable.

8.2.3 Multi leader car-following models

Human drivers can anticipate on the movement of their leader by looking ahead and considering more leaders. This has empirically been shown by Ossen (2008). Generally, one would adapt the car-following model allowing n times the spacing for the n th leader. Also, one might expect that a follower acts less sensitive on inputs from leaders further away – that might be in terms of lower acceleration (i.e., closer to zero) or later (i.e., a higher reaction time).

Two “mistakes” are common, leading to multi-leader car-following models which seem to make sense, but are not realistic.

1. In the car-following behavior, only vehicles in the same platoon should be considered, or vehicles which might influence the following vehicle. A car-following model which always takes three leaders regardless of the spacings might take a leader which is a long distance away, which in reality will not influence the driver.
2. If the car following model predicts the *average* acceleration caused by each of the leaders, it might be that the follower crashes into its leader. Instead, a minimum operator is usually more suitable.

8.2.4 Insensitivity depending on distance

Most car-following models indicate drivers will adapt their speed based on the action of their leaders. Wiedemann (1974) states that drivers only react if the required action is above a certain threshold. Specifically, he indicates that within some bounds, drivers are unable to observe speed differences. One might also argue that within some boundaries, drivers are unwilling to adapt their speeds because the adaptation is too low. These bounds depend on the spacing between the leader and follower: the larger the spacing, the larger the speed difference needs to be before a driver is able to observe the speed difference. As example, a 1 km/h speed difference might be unobservable (or unimportant to react upon) on a 200 meter spacing, but if the spacing is 10 meter, this is observable (or important).

It is relevant to draw a diagram relating the relative speed to the spacing, as is done in figure 8.3. The thresholds are indicated: within these bounds, the driver is insensitive and is considered to keep his current speed. Outside the bounds, the driver accelerates to match the traffic situation.

When the leader brakes, the follower closes in. That means that point is in the right half (the follower has a higher speed) and the line is going down (the spacing reduces because the follower is driving faster). At a certain moment, the follower comes closer to his leader and starts reacting to the speed difference, i.e. he will reduce speed. He can either not brake enough and have still a higher speed, or overreact. If the braking is not enough, the situation is the same as the starting situation, and the same situation will occur. Therefore, we will assume for the further reasoning that the follower overreacts.

The overreaction means that the follower will have a lower speed than the leader. That means that the speed difference will go through zero (the y-axis in the figure). At that moment, the speeds are equal, so the spacing remains momentarily the same. Therefore, when crossing the y-axis, the line is horizontal. After that, the leader drives at a higher speed than the follower, and the spacing will start increasing. For low speed differences, the speed difference is under the observation threshold and the follower does not adapt his acceleration. Only once the next bound is reached, he will notice the leader is shying away and start accelerating again.

If he will again overreact, the speed difference will become positive. Again, the speed difference will go through zero (the y-axis) where the line has a horizontal tangent line (a zero speed difference means that at that moment the spacing remains constant). One can continue constructing this figure, and it shows that in this phase plane (i.e., the plane relative speed - spacing) the leader-follower pair makes circles.

The wider the circles are, the wider the observation thresholds. The threshold are considered to be expanding for larger spacings. Empirical studies (e.g., Knoop et al. (2009); Hoogendoorn et al. (2011) indeed reveal these type of circles.

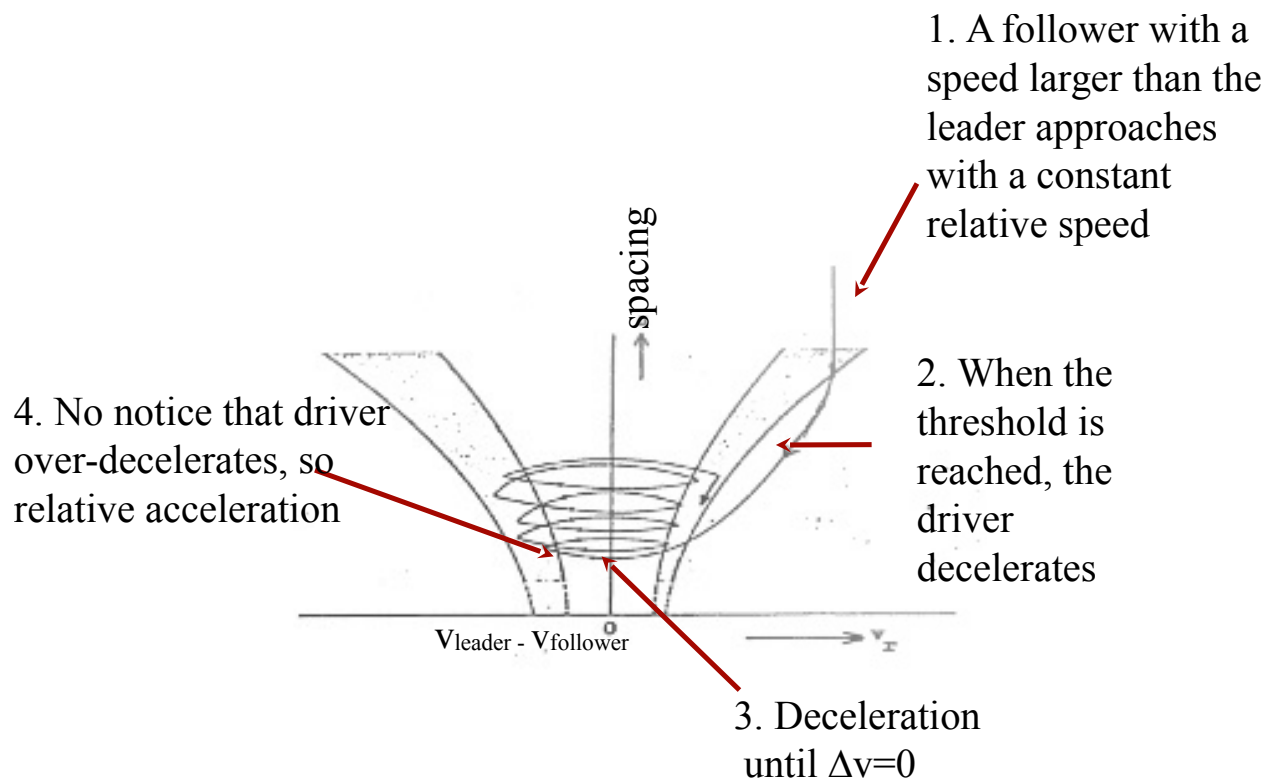


Figure 8.3: Schematic overview of the principles by Wiedemann

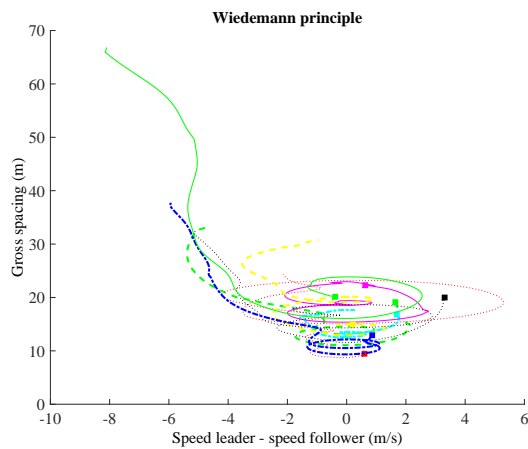


Figure 8.4: Empirical observations of leader-follower pairs in the relative speed - spacing plane

Caution is required in interpreting these figures. A Newell car-following model does not implement these type of observation thresholds. However, the relative speed - spacing figures will show circles due to the reaction time. Namely, once the leader brakes, the follower will not yet, and in the relative speed - spacing plan this will be shown as a part of a circle. A correct analysis tracks the car-following behaviour not at the same moments in time (vertical lines in the space time diagram), but at lines moving back with the shock wave speed. When doing so for the Newell model, one would not find any circles at all. A detailed analysis of this methods is presented by Laval (2011)

Finally, some words on the principle in relation to car-following. Car-following models prescribe the position, speed or acceleration of the follower based on the position, speed, or acceleration of their leaders. The principle laid out in this section only mentions when the speed is *not* adapted, but does not specify the acceleration outside the thresholds. As such, it therefore cannot be considered a car-following model. Instead, it can be combined with another car-following model to get a complete description.

8.3 Examples

This section shows the most used models, apart from the Newell car-following model described in 8.1.

8.3.1 Helly

The first model we describe here is the Helly model (Helly, 1959). The Helly model prescribes a desired spacing s^* as function of the speed v :

$$s^* = s_0 + Tv \quad (8.3)$$

Note that this could be considered as a spacing at standstill (jam spacing) plus a dynamic part where T is the net time headway (subtracting the jam spacing from desired spacing).

Now the acceleration is determined by a desire to drive at the same speed as the predecessor and a desire to drive at the desired headway. The model prescribes the following acceleration:

$$a(t) = \alpha (\Delta v(t - \tau)) + \gamma (s(t - \tau) - s^*) \quad (8.4)$$

In this equation, Δv is the speed difference, t is a moment in time and τ a reaction time.

8.3.2 Optimal Velocity Model

The optimal velocity model proposed by Bando et al. (1995) is a car-following model specifying the acceleration a as follows:

$$a = a_0(v^* - v) \quad (8.5)$$

In this equation, v is the speed of the vehicle, and a_0 a reference acceleration (tunable parameter, constant for a specific vehicle-driver combination). v^* is determined as follows:

$$v^* = 16.8(\tanh(0.086(s - 25) + 0.913)) \quad (8.6)$$

In this equation, s is the spacing (in meters) between the vehicle and its leader, giving the speed in m/s.

8.3.3 Intelligent Driver model

Treiber et al. (2000) proposes the Intelligent Driver Model. This prescribes the following acceleration:

$$\frac{dv}{dt} = a_0 \left(1 - \left(\frac{v}{v_0} \right)^4 - \left(\frac{s^*(v, \Delta v)}{s} \right)^2 \right) \quad (8.7)$$

with the desired spacing s^* as function of speed v and speed difference Δv :

$$s^*(v, \Delta v) = s_0 + vT + \frac{v\Delta v}{2\sqrt{ab}} \quad (8.8)$$

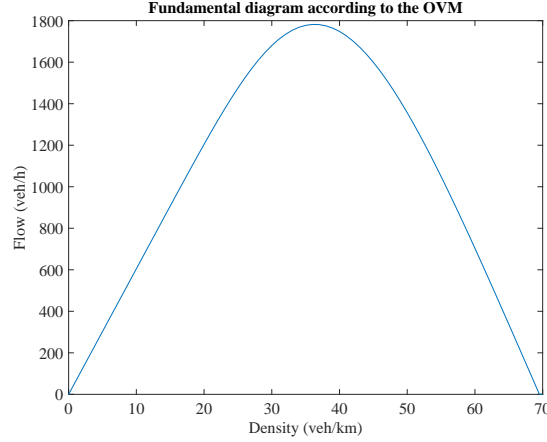


Figure 8.5: Fundamental diagram according to the OVM

In this equation, Δv is the speed difference between the leader and the follower, a is acceleration and b a comfortable deceleration. a_0 is a reference acceleration (parameter).

8.4 Relation to fundamental diagram

The fundamental diagram gives in its usual form the relation between the density and the flow for homogeneous and stationary conditions. Also car-following models can describe homogeneous and stationary conditions. In that case, all vehicles should drive at the speed and should not change speed (stationary). Therefore, the acceleration of all vehicles must be zero.

Many car-following model prescribe a the acceleration based on speed and spacing. The equilibrium conditions mean that the acceleration is zero (and one might argue the relative speeds as well). The relation between spacing and speed then gives an implicit equation for the spacing-speed diagram. Using that the density is the inverse of the (average) spacing, and the flow is (average) speed times density, one can reformulate the spacing-speed diagram from the car-following model into a fundamental diagram.

Take for example the OVM, equation 8.5 and equation 8.6. Equilibrium conditions prescribe that drivers do not accelerate, hence $a_0(v^* - v) = 0$. That means that either $a_0 = 0$, or

$$(v^* - v) = 0 \iff v^* = v \quad (8.9)$$

. Since a_0 cannot be zero – in that case the vehicle would never accelerate. Therefore, in equilibrium conditions, equation 8.9 should hold. Using equation 8.6, we find:

$$v = 16.8(\tanh(0.086(s - 25) + 0.913)) \quad (8.10)$$

This gives a relation between speed and spacing. For a fundamental diagram in flow-density, that gives (using $q = kv$:

$$q = kv = k(16.8(\tanh(0.086(s - 25) + 0.913))) \quad (8.11)$$

The spacing can be changed into a density. Since all vehicle have the same spacing (equilibrium conditions), we may use

$$s = \langle s \rangle - 1/k \quad (8.12)$$

Substituting this in equation 8.11, we find an expression for the fundamental diagram.

$$q = k(16.8(\tanh(0.086(1/k - 25) + 0.913))) \quad (8.13)$$

Note that in this expression with the values as in equation 8.6, density should be in vehicles per meter and the resulting flow is given in veh/s. Converting these units, this results in the fundamental diagram as shown in figure 8.5.

Selected problems

For this chapter, consider problems: 11, A.2.4, A.3.2, A.4.2, 133, 154, 179, 181, 221, 223, A.10.4

Chapter 9

Macroscopic Dynamic Traffic flow Models

This chapter describes the principles which can be used in macroscopic traffic flow modelling. First, the mathematical models are presented (section 9.1). From section 9.2 several discretisation schemes are presented, i.e. models which can be implemented in a computer model.

9.1 Mathematical models

Also on the macroscopic level, one can model the traffic operations. The main advantages of macroscopic modelling over microscopic modelling are

1. a lower calculation time
2. less sensitive to stochastic effects

Simulating traffic flow macroscopically means that one has to find the equations of the dynamics of the macroscopic traffic flow variables. Conservation of vehicles yield the following equation:

$$\frac{\partial k}{\partial t} + \frac{\partial q}{\partial x} = 0 \quad (9.1)$$

The most basic modelling is first order modelling. In this case, a fundamental diagram is assumed, and hence there is a relationship

$$q = q(k) \quad (9.2)$$

Substituting this equation in equation 9.1, we find

$$\frac{\partial k}{\partial t} + \frac{\partial q}{\partial k} \frac{\partial k}{\partial x} = 0 \quad (9.3)$$

This can be rewritten using the characteristic speed (see chapter 6): $\frac{\partial q}{\partial k} = c(k)$

$$\frac{\partial k}{\partial t} + c(k) \frac{\partial k}{\partial x} = 0 \quad (9.4)$$

As chapter 6 already showed, the boundary conditions for the traffic flow can come from either downstream or upstream. Therefore, a combination of a downwind and an upwind scheme have been proposed, as section 9.2 will show. A way to overcome the problem of changing direction of the limiting conditions is to change the coordinate system. Section 9.4 will discuss this method in more detail.

Regardless of the coordinate system, one might introduce different vehicle classes. Section 9.5 discusses this phenomenon; a way to implement it in a computer model in discrete equations is proposed in section 9.5.2.

All above methods use the fundamental diagram as starting point. This is not necessarily true. Section 9.6 discusses higher order models, i.e. models where traffic states can deviate from the fundamental diagram based on dynamics.

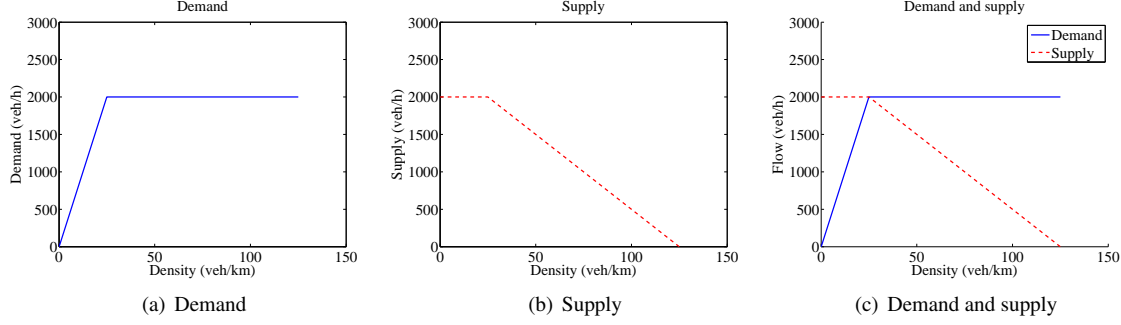


Figure 9.1: The demand and supply curves

9.2 Spatial and temporal discretisation

The most standard way to calculate traffic models is to discretise the space and time. In particular, this section will explain the cell transmission model, as introduced by Daganzo (1994). Mathematically speaking, this model is based on the model independently proposed by Lighthill and Whitham (1955) and Richards (1956) that is discretized in space and time and solved with a solution scheme proposed by Godunov (Godunov, 1959). The model is also referred to as LWR model, to Lighthill, Williams and Richards.

To start, a road is split up into segments of length L , and time is discretised in steps of Δt . The state of a cell i at time step t is determined by its density. For each cell, the fundamental diagram is specified. First the concept is explained. Then, the details and equations are given.

In uncongested conditions, the flow between upstream cell i and a downstream cell $i + 1$ is determined by the demand (in veh/h) from cell i to cell $i + 1$. If there are more vehicles, the demand is higher. The actual demand can be derived from the density in cell i and the fundamental diagram.

In congested conditions, the demand is high (many vehicles want to get out of the area), but the supply is the restriction of the flow. In this case, the downstream cell $i + 1$ restricts the flow. The flow is hence determined by the flow in the downstream cell, which can be derived from the density and the fundamental diagram.

Once the flow between cell i and cell $i + 1$ is determined, the densities in the cells can be updated, and the process can be started again.

The more formal traffic flow scheme is as follows. We start by splitting the fundamental diagram into two parts. We define a demand function D as function of the density, which equals the flow for undercritical conditions and the capacity in overcritical conditions.

$$D = \begin{cases} q(k) & \text{if } k \leq k_c \\ C & \text{if } k > k_c \end{cases} \quad (9.5)$$

This indicates how much traffic wants to go from the upstream cell to the downstream cell.

Similarly, we create a supply function S , which limits the flow at the entry of a cell in cases in which the cell is in overcritical conditions. This function equals capacity for undercritical conditions, and is equal to the flow given by the congested branch of the fundamental diagram in overcritical conditions:

$$S = \begin{cases} C & \text{if } k \leq k_c \\ q(k) & \text{if } k > k_c \end{cases} \quad (9.6)$$

The demand and supply curves resulting from a triangular fundamental diagram can be found in figure 9.1. The flow from cell i to cell $i + 1$ is determined by the minimum of the demand in cell i and the supply in cell $i + 1$:

$$q_{i,i+1} = \min \{D_i, S_{i+1}\} \quad (9.7)$$

From figure 9.2, it also shows how the fundamental diagram results from the minimum of demand and supply.

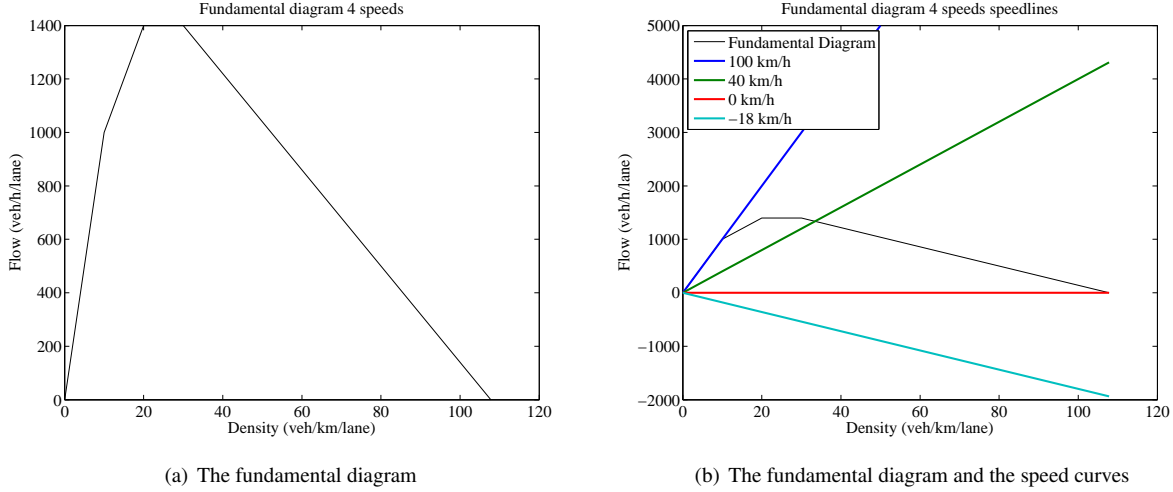


Figure 9.2: The fundamental diagram in the flow density plane

This can be translated into an actual number of vehicles by the time step, by multiplying this flow by its duration, i.e. the duration of a time step Δt . The effect that this flow has on the densities in the cells depends on the lengths of the cells:

$$\Delta k_i = (q_{i-1,i} - q_{i,i+1}) (\Delta t / L) \quad (9.8)$$

9.3 Event based

In event based models, time is not approached by infinitely small time steps. Instead, the traffic is assumed to stay the same up to the next event.

A simple event based traffic model is the shock wave theory discussed in section 5. There, the traffic states propagate until two waves intersect, and the next wave will be created. Then again, the next event can be calculated, but there is no need to check how the waves propagate in the mean time.

9.3.1 Link Transmission Model

The link transmission model is a model developed by Yperman et al. (2006). It considers nodes as base elements, and using cumulative curves it is determined how much traffic can flow into the link and out of the link. Just like the cell transmission model, a demand and a supply are determined; the difference being that this has to be determined *only once* per node. A link hence does not need to be cut in different cells, which makes the computation more efficient.

It is based on Newell (1993), which gives limits for the number of vehicles which will have passed a specific point. That is maximized by the traffic, but limited by either demand or supply.

Suppose the road has a piecewise linear fundamental diagram, as in figure 9.2(a). Each of the pieces of the fundamental diagram corresponds with a wave speed. For several moving observers, passing with a speed v one can calculate the maximum flow passed this observer, which can be calculated by (see equation 4.11). The flow for a certain density is given by the fundamental diagram. However, by moving there is a flow kv subtracted from it. This flow difference which should be subtracted is indicated in the colored lines in figure 9.2(b). The flow relative to the observer is then the distance between that line and the fundamental diagram, or in an equation (equal to equation 4.11):

$$q_{\text{rel}} = k(v - v) \quad (9.9)$$

This maximum flow is plotted in figure 9.2(b). This relative flow for each of the observers is plotted in figure 9.3(a). It is important to note that these relative flows are maximum for the density range in which the characteristic speed of the fundamental diagram matches the speed of the corresponding moving observer.

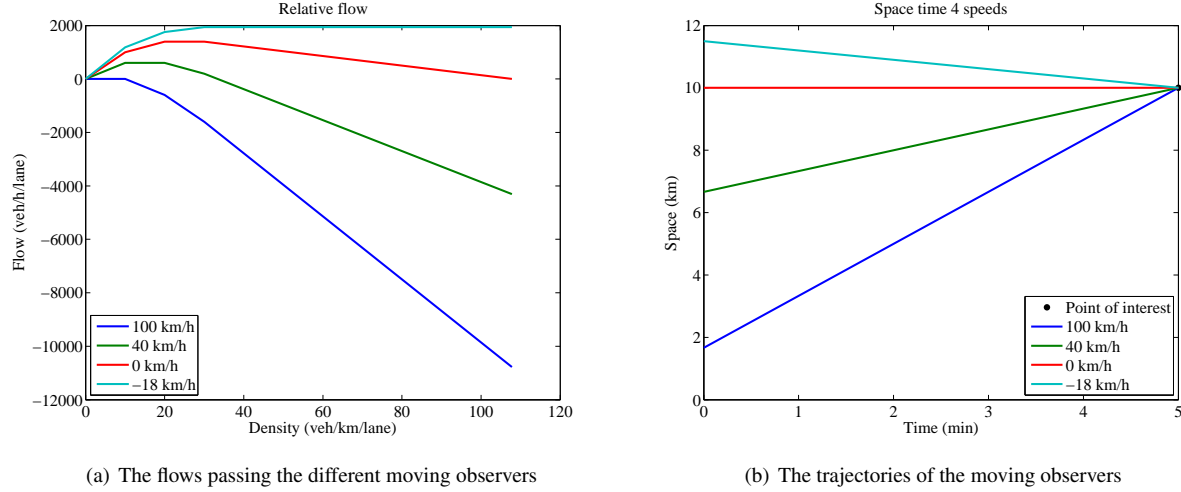


Figure 9.3: Calculating the flow using moving observers

These flows are measured along a moving path, as indicated in figure 9.3(b). For the point of interest, indicated in the figure, one can calculate how many vehicles have passed. This depends on the conditions earlier in time. The limits of the number of vehicles that can have passed are given by relative flows passing the moving observer.

In our case for four different parts of the fundamental diagram, there are four paths along which the relative flow should be checked, as shown in figure 9.3(b). If the initial conditions (at $t=0$) are known, the cumulative vehicle number at each of the starting points of these lines is known (indicated by $N_{0,i}$). To this initial cumulative vehicle number we should add the relative flow times the time to have the restriction on the vehicle number for that particular moving observer, indexed i

$$N_{\text{lim}}^i \leq N_{0,i} + q_{\text{rel}} \Delta t \quad (9.10)$$

Because the relative flow is maximum if the characteristic speed is the speed of the moving observer, we know that we can only consider the maximum flow pass the moving observer. Or in other words, the lower flows for other densities do not need to be considered. Hence the vehicle number in the point of interest can be calculated:

$$N = \min_i (N_{\text{lim}}^i) \quad (9.11)$$

9.4 Lagrangian coordinates

9.4.1 Introduction

The classical kinematic wave model is based on an Eulerian coordinate system. Recently, an alternative formulation in Lagrangian coordinates was introduced by Leclercq et al. (2007). The principal difference between the Eulerian formulation and the Lagrangian formulation is the coordinate system. In Eulerian coordinates, the traffic state at location x at time t is described. Therefore, the coordinates are fixed in space. However, in Lagrangian coordinates the traffic state of the n -th vehicle at time t is described. Hence, coordinates *move with the vehicles*. In other words: in Eulerian coordinates traffic is observed from a fixed point alongside the road, in Lagrangian coordinates traffic is observed from a vehicle travelling with the traffic flow. The main variables in Eulerian coordinates are, as have been used throughout the reader, density and flow as functions of time and space. In the Lagrangian formulation these are the spacing and the speed as function of the time and the vehicle number. This is summarised in table 9.1.

Figure 9.4 shows an illustration of the Lagrangian coordinate system in the x - t plane. Vehicles are numbered in opposite direction of the driving direction, in which the first vehicle has the lowest number. Note that, just as in the traditional Eulerian formulation, we assume that traffic can be modelled as a continuum. Therefore, n is not integer but can take any real value. As a consequence, vehicle spacing and velocity can be determined also between vehicles.

Table 9.1: The variables in the Lagrangian formulation

Variable	Euler	Lagrange
Traffic state	Flow q	Speed v
	Density k	Spacing s
Variable	space	vehicle number
	time	time

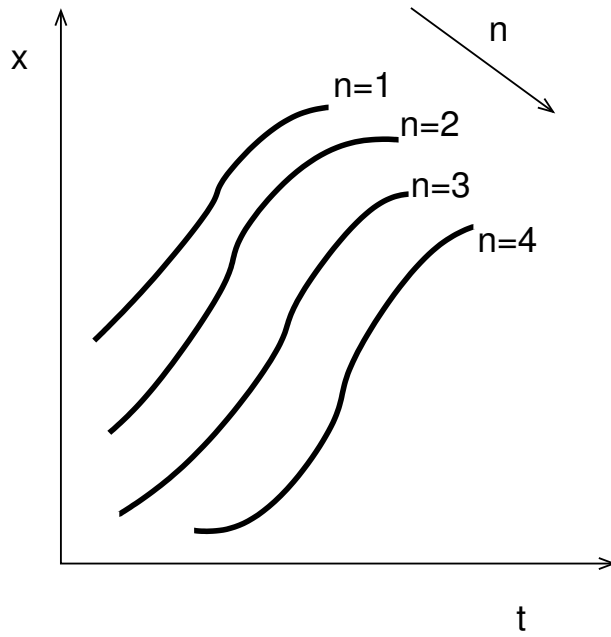


Figure 9.4: Some vehicle trajectories in the (t, x) -plane.

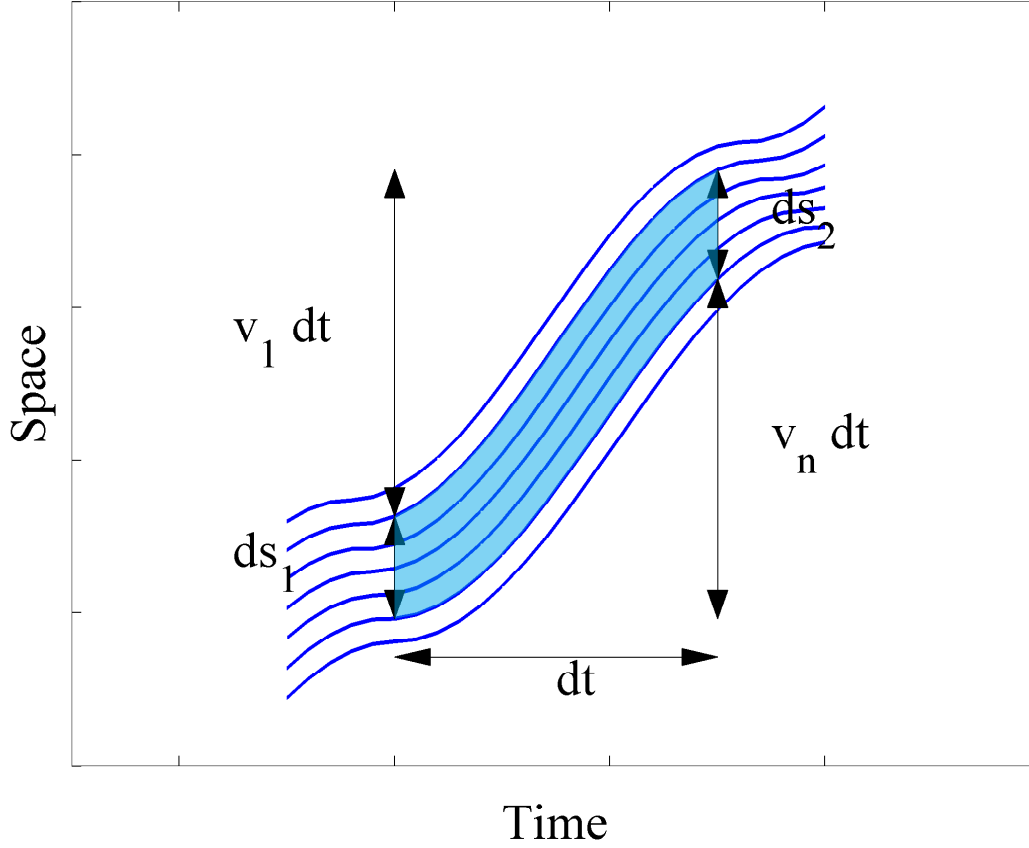


Figure 9.5: Graphical illustration of the variation of platoon length in Lagrangian coordinates

9.4.2 Mathematical formulation of the traffic flow equations

In the Eulerian coordinate system we have the following equation for conservation of vehicles:

$$\frac{\partial \rho}{\partial t} + \frac{\partial Q(\rho)}{\partial x} = 0 \quad (9.12)$$

In the Lagrangian formulation this changes into

$$\frac{\partial s}{\partial t} + \frac{\partial V(s)}{\partial n} = 0 \quad (9.13)$$

In the sequel of this section, we will give an intuitive derivation for this conservation equation, using figure 9.5. The figure shows vehicle trajectories of which a group (a platoon) of several (dn) vehicles is followed over some time dt . This control volume is indicated as a blue box. The length of the platoon changes over time as it travels forward. On the one hand, the original length at time t_1 is increased by the distance traveled by the first vehicle (n_1) in the platoon between t_1 and t_2 . On the other hand, it is decreased by the distance travelled by the last vehicle n_2 in the same time interval. This can be written as:

$$s_{\text{new}} dn = s_{\text{old}} dn + v_{\text{first}} dt - v_{\text{last}} dt \quad (9.14)$$

Now we take an infinitesimal volume, i.e. we follow a small platoon over a small time interval. Rearrangement gives:

$$\frac{s_{\text{new}} - s_{\text{old}}}{dt} + \frac{v_{\text{first}} - v_{\text{last}}}{dn} = 0 \quad (9.15)$$

We take an infinitesimal volume, i.e. we let $dn \rightarrow 0$ and $dt \rightarrow 0$. This yields the Lagrangian conservation equation:

$$\frac{\partial s}{\partial t} + \frac{\partial v}{\partial n} = 0. \quad (9.16)$$

9.4.3 Advantages of Lagrangian formulation

The main disadvantage of the Eulerian discretisation scheme is the numerical diffusion. Figure 9.6 shows this diffusion. The situation starts with a high density (jam density, 150 veh/km) between km 3 and 4. At km 5, the road is blocked. Once the simulation starts, shockwave theory predicts that the shock remains intact. This is what should be modelled by the method.

We modelled this situation with different time and space resolutions. The temporal resolution (time step) varied from 1 to 20 to 60 seconds. The numerical diffusion is lowest if the cell length are as short as possible, but if the cell lengths should never be smaller than the time step times the free flow speed. The cell lengths were chosen to match the temporal resolution. For the simulation, we chose a fundamental diagram with $k_c=25$ veh/km, $k_j=150$ veh/km, and $C=2000$ veh/h.

The numerical implementation of the model shows a different phenomenon. This is called numerical diffusion: due to the numerical scheme of the solution, the shock is smoothed. The magnitude of this diffusion depends on the time step of the scheme. The numerical diffusion is not or less present with a well chosen discretisation scheme in lagrangian coordinates. Figure 9.7 shows how the numerical schemes can work.

In summary these are the main advantages of the Lagrangian formulation are:

- “Easy” numerical discretization (simulation)
- Accurate simulation results
- Fast simulation
- Trajectories of (individual) vehicles come out by default

9.5 Multi-class

9.5.1 Principles

Another dimension, which in principle can be combined with all discretisations mentioned above, is the number of classes in the model. Usually, these are trucks and passenger cars, since these have distinct characteristics. The three main differences are:

1. Trucks have a lower speed
2. Trucks have a longer length
3. Trucks have a lower acceleration

In first-order traffic flow modelling, accelerations are not considered as such, and thus difference three is ignored. The first two differences lead to a different fundamental diagram for trucks.

Figure 9.8 shows what the influence is of different speeds at the gross headways. For high speeds, the gross distance consist mainly of net headway, and thus the truck does not occupy much more space than a passenger car. For low speeds, this difference is the same, but relatively, this difference is larger.

The capacity is the maximum number of vehicles that can pass a cross section per unit of time. As is clear from the above, this number will be less if the traffic stream consist of more trucks. The effect of trucks is expressed as

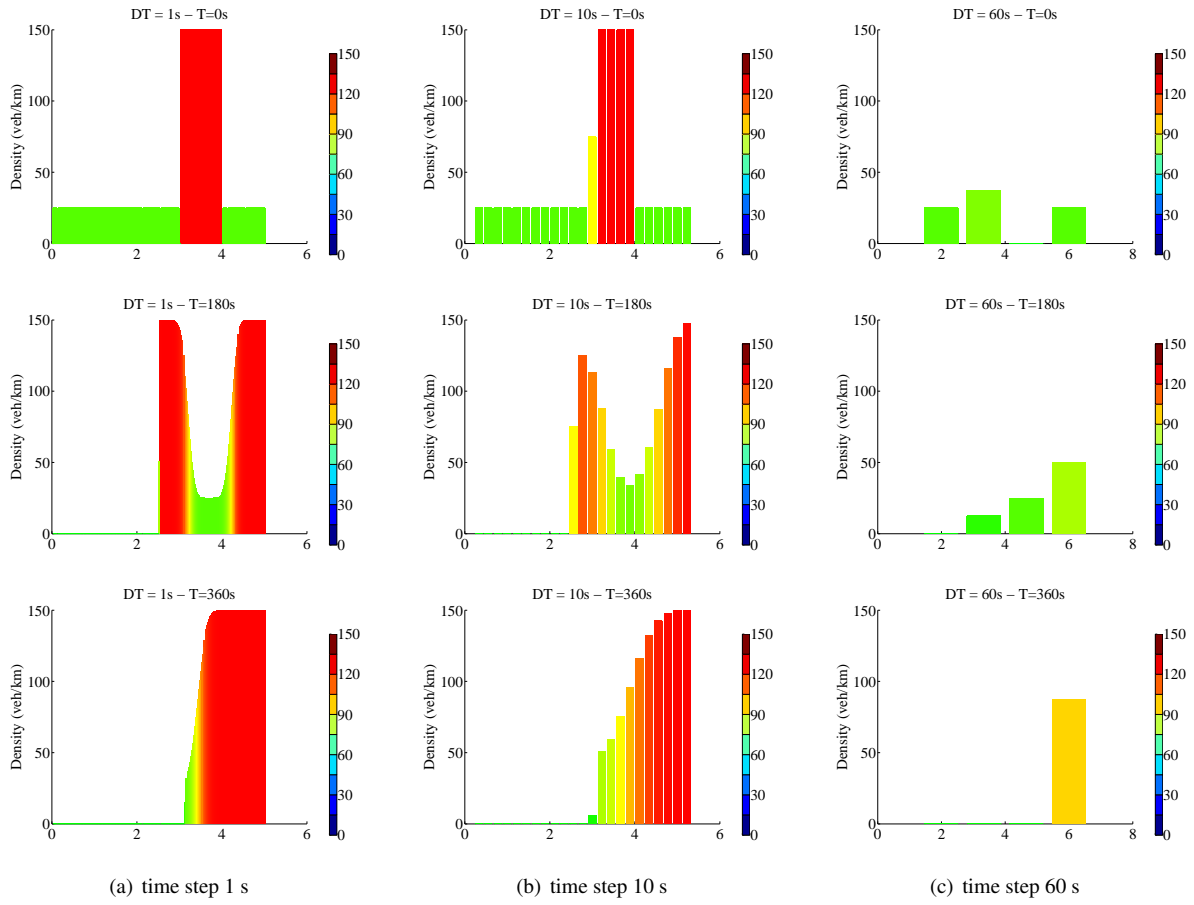


Figure 9.6: An example of the numerical diffusion in an Eulerian discretisation scheme

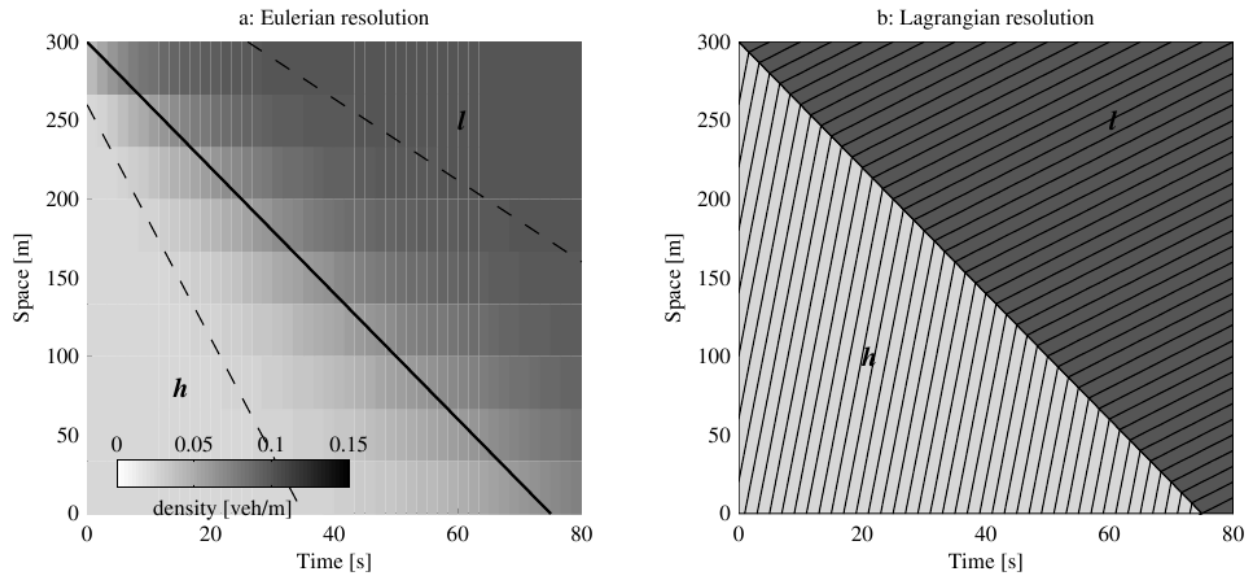


Figure 9.7: Simulation results of the backward propagation of a congestion tail, simulated in Lagrangian and Eulerian coordinates. Figure from Leclercq et al. (2007)

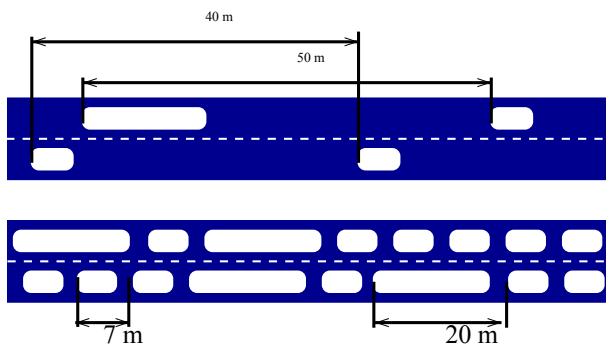


Figure 9.8: The influence of the vehicle length on the density and the remaining net spacing for different speeds

passenger car equivalent, or PCE. The PCE value for vehicles in class J is indicated by \mathcal{P}_J . In this description, the flow is limited by the capacity:

$$q \leq \sum_J \mathcal{P}_J q_J \quad (9.17)$$

In this equation, q_J , is the flow of vehicle class J . PCE values for trucks can be found in hand books, for instance Transportation Research Board, (2000); Heikoop (2011). Typically, the PCE for trucks is around 2. If we consider a road with a capacity of 2000 pcu/h (passenger car unit, but often simply quoted as 2000 veh/h), a demand of 2000 passenger cars per hour is critical. A demand of 1800 passenger cars per hour and 200 trucks per hour leads to an effective demand of $1800 + 2 \cdot 200 = 2200$ pce/h (see equation 9.17), which is overcritical. Given the vehicle demand of 1800 veh/h and the capacity of 2000 pcu/h, there is a remaining capacity of 200 pcu per hour. This equals a flow of $200/2 = 100$ trucks/h.

1. [PCE calculation]Exercise: calculate the PCE for trucks for the fastlane discription for 10% and 20% trucks. Assume reasonable numbers for the unknown variables.

9.5.2 Fastlane

The two classes can be mixed, and then the classes should interact. Fastlane (van Lint et al., 2008) is a model where this mixture is incorporated. The model is based on a class-specific fundamental diagram which gives the relation between the *net* distance headway and the speed. Note that this relation does not directly work with the density, i.e., the inverse of the gross distance headway. The reasoning is that the speed of both classes in congestion is equal and depends only on the net distance headway. Because trucks are longer, the gross distance headway for the same speeds is longer for trucks. By separating the headways from the length of the vehicle, only one speed-headway relationship for congestion needs to be specified.

The independent variable for the model could be “empty space”. This can be uniquely changed into a generalized density, assuming a uniform vehicle of one passenger car vehicle.

Using these principles, as well as the class-specific fundamental diagrams and the model equations for the Fastlane model can be derived. The resulting model equation can be found in Van Wageningen-Kessels (2013), from which the remainder of this section is taken.

Before we reformulate the multi-class conservation equation into Lagrangian coordinates we need some definitions and preliminaries. We define class 1 as the reference class for the coordinate system. This implies that only vehicles of class 1 are numbered. Therefore, coordinate n refers to the number of vehicles of class 1 that have passed location x until time t . Furthermore, the coordinate system moves with the vehicles of class 1, i.e. with velocity v_1 . Therefore, the Lagrangian time derivative in the multi-class model is defined by:

$$\frac{D}{Dt} = \frac{\partial}{\partial t} + v_1 \frac{\partial}{\partial x} \quad (9.18)$$

Finally, the class-specific spacing of class 1 can be expressed as the partial derivative:

$$s_1 = -\frac{\partial x}{\partial n} \quad (9.19)$$

Realising that $s_u = 1/k_u$, this can be substituted into the Eulerian conservation equation (9.13), the quotient rule is applied and the result is rewritten:

$$\frac{\partial}{\partial t} \left(\frac{1}{s_u} \right) + \frac{\partial}{\partial x} \left(\frac{v_u}{s_u} \right) = 0 \quad \Rightarrow \quad \frac{\partial s_u}{\partial t} - s_u \frac{\partial v_u}{\partial x} + v_u \frac{\partial s_u}{\partial x} = 0 \quad (9.20)$$

Subsequently, substituting the multi-class Lagrangian time derivative (9.18) yields:

$$\frac{Ds_u}{Dt} - s_u \frac{\partial v_u}{\partial x} + (v_u - v_1) \frac{\partial s_u}{\partial x} = 0 \quad (9.21)$$

Finally, (9.19) is substituted to find the Lagrangian multi-class conservation equation:

$$\frac{Ds_u}{Dt} + \frac{s_u}{s_1} \frac{\partial v_u}{\partial n} + \frac{v_1 - v_u}{s_1} \frac{\partial s_u}{\partial n} = 0 \quad (9.22)$$

We note that for class 1 the conservation equation (9.22) reduces to a simpler form:

$$\frac{Ds_1}{Dt} + \frac{\partial v_1}{\partial n} = 0 \quad (9.23)$$

Yet an alternative formulation of the conservation equation in Lagrangian coordinates is proposed in (Yuan et al., 2015b; Yuan, 2013):

$$\frac{Ds_u}{Dt} + \frac{\partial v_u}{\partial n_u} = 0 \quad (9.24)$$

with Lagrangian time derivative:

$$\frac{D}{Dt} = \frac{\partial}{\partial t} + v_u \frac{\partial}{\partial x_u} \quad (9.25)$$

The main difference is that in this model a different coordinate system is introduced for each class. The coordinate systems are coupled via the fundamental relation and the effective density function. Yuan et al. (2015b); Yuan (2013) argue that this formulation may lead to more efficient simulations if there are only few vehicles in the reference class.

9.6 Higher order modelling

There are other macroscopic models, which include more terms and can include traffic states that are not on the fundamental diagram. That way, hysteresis can be included. One of the most used higher order models is the Metanet model. In this model, the speed increase is limited, representing a reaction time and a limited acceleration. In this reader we do not discuss these models. For more information on the disadvantages and advantages, see Daganzo (1995) and Aw and Rascle (2000). For more information on the Metanet model, see Kotsialos et al. (2002), which is a macroscopic equivalent of the Payne car-following model (Payne, 1971).

9.7 Suggested problems

28, A.2.1, A.3.1, 88, 134, 135, 136, 194, 241, 242, 243

Chapter 10

Microscopic lane change models

10.1 Introduction

The parts up to now are mainly focussed on the longitudinal driving behaviour and the modelling thereof. This chapter discusses lateral driving behaviour. For multi-lane roads, the lane changing plays an important role. In fact, lane changing is claimed to be the main cause for traffic breakdowns Ahn and Cassidy (2007). They argue that a single lane change manoeuvre might lead to a disturbance which grows and due to overreaction, leads to a stop and go wave. Moreover, the lane flow distribution (LFD) is not equal at bottlenecks, implying that in some lanes there is capacity remaining even though the combined flow gets overcritical.

Firstly this chapter discusses a lane selection model from a psychological perspective section 10.3). Then, in section 10.4 a microscopic lane change model is introduced. Section 10.5 discusses more advanced lane change models, combining lateral and longitudinal movements.

10.2 Type of lane changes

Three types of lane changes are distinguished. They are shown in figure 10.1 and explained below

1. Desired lane changes are lane changes which a driver does to be better off, usually because the speed in the adjacent lane is larger.
2. Mandatory lane changes are lane changes which a driver does because he has to to continue to its destination. This might be because the lane ends and the driver has to merge, or because the road splits into roadways with different directions, see figure 10.1(b)
3. Courtesy lane changes are lane changes which a driver makes to help other drivers. There is no direct benefit for the driver that makes the lane change.

10.3 Slugs and rabbits

This section describes a theory of lane selection, posed by Daganzo (2002a,b).

10.3.1 Theory

This theory poses there are slugs and rabbits, two different types of drivers each with a specific type of lane selection. They are defined as follows:

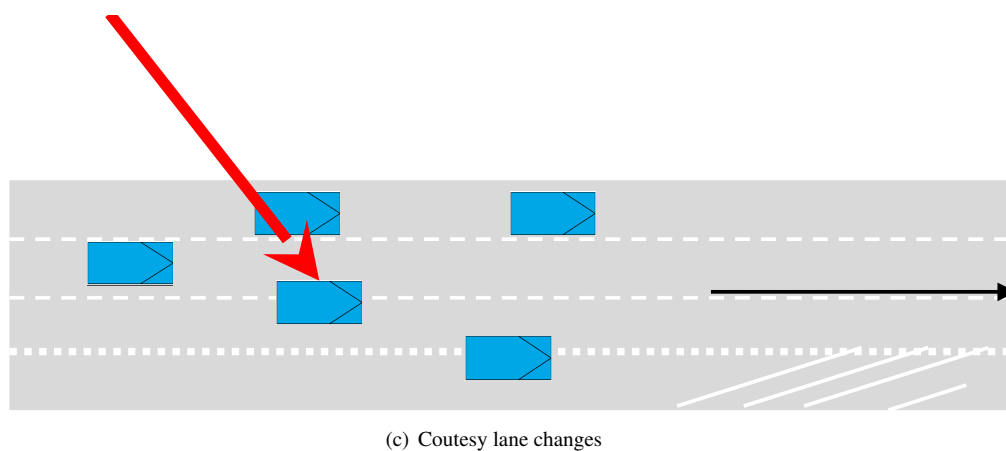
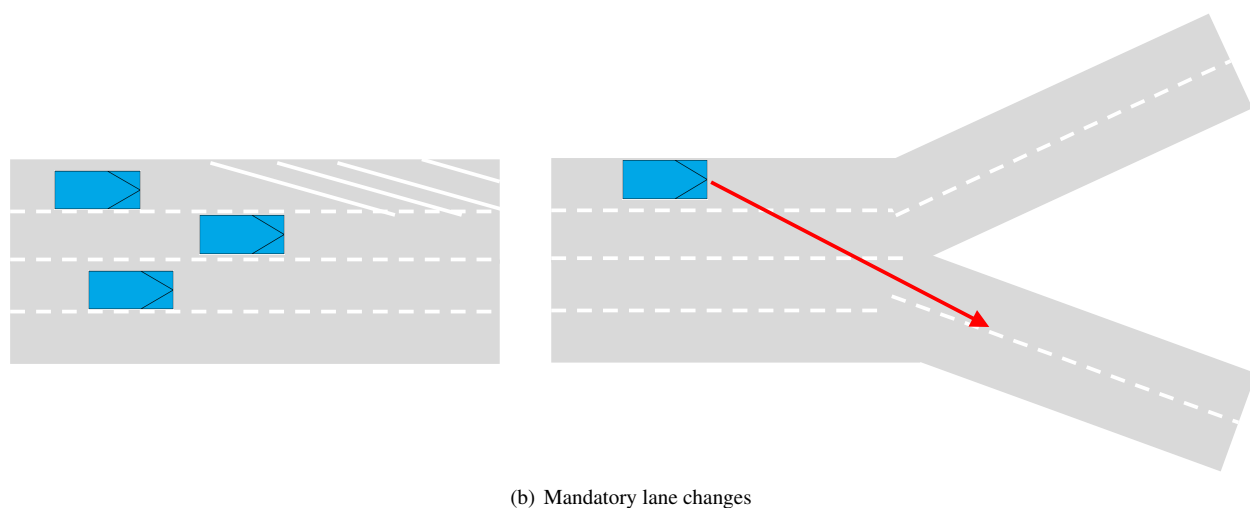
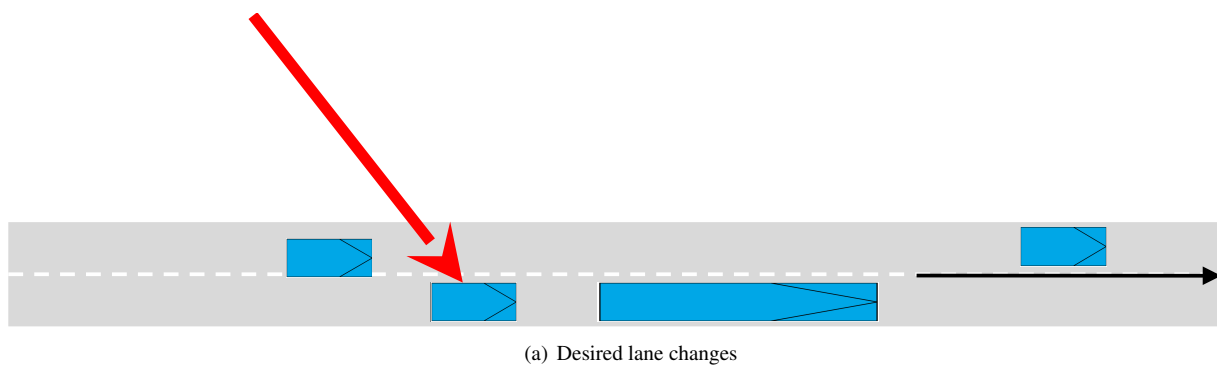


Figure 10.1: Different type of lane changes

Category	free speed	lane choice
Slug	Low	always right
Rabbit	High	Fastest

This means that the left lane(s) can operate at a different speed, and even in a different regime than the right lane.

10.3.2 Traffic operations

Consider a situation with low demand. Then, slugs drive at their desired speed in the right lane. This speed is lower than the desired speed of the rabbits. Rabbits hence drive their desired speed and stay in the left lane(s). Both (type of) lanes have a different speed, and operate independently. That is why this state is called a two pipe regime.

If the density in the left lane(s) increases, the speed can decrease to values below the free flow speed of the right lane. Rabbits then choose to change lanes towards the right lane, since they will change to the fastest lane. This will increase the density on the right lane, and lower the speed. The density on the left lane(s) will decrease and the speed will increase. Thus, the difference in speeds between the right and the left lane(s) decreases. This process of changing lanes continues until the speed differences between the left and the right lane have decreased to zero. Then, the complete flow operates at one state, and this flow is called a one pipe regime.

10.3.3 Loading

The section above describes traffic operations at a continuous motorway stretch. Interesting phenomena occur at on-ramps. At an on-ramp, traffic merges onto the main road, but always into the right lane. Consequently, the rabbits are not in their desired lane. They need a distance to perform the additional lane change into the left, and faster, lane. If the density in the left lane already is high, the traffic in the left lane might become overcritical, and speeds might reduce. Note that this is happening *downstream* of the point of merging, namely at a point where the rabbits change towards the fast lane.

10.3.4 Consequences

Although the model of lane selection as proposed by Daganzo is simple, it does explain the following features observed in traffic.

- Boomerang effect
- Uneven lane distribution
- Capacity drop

10.4 Utility model

The theory of slugs and rabbits is a psychological theory which explains some phenomena. It can not yet directly be implemented in a model. The lane change model MOBIL, abbreviation for Minimizing Overall Braking Induced by Lane Changes, can. It describes for each time step whether or not a vehicle will change lanes. The model is explained in this section. The section first describes the idea of the model. Then, the model is formulated in terms of equations.

10.4.1 Model idea

The basic idea of the model is that for each of the lanes a *utility* is calculated. This utility is based on the following items (note: all of the utilities below have a different value for a different lane choice):

- Foreseen acceleration of the driver: the more it can accelerate the better it is
- Foreseen acceleration of the other drivers: one would prefer not to hinder others
- (For European driving:) how far right: the rules prescribe to keep right unless overtaking.

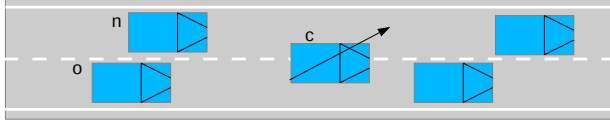


Figure 10.2: The lane changing vehicle and the surrounding vehicles. In this figure, the vehicle is considering a lane change to a left lane. If a lane change to the right lane is considered, vehicles in the other lane should be considered, which will be indicated with the same symbols

These utilities are calculated for each of the possible decisions: change left, change right or stay in current lane. Then, they are weighted per decision and summed. This gives the utility for a certain lane.

10.4.2 Model equations

The model is based on utility, calculated per lane, which we indicate by U_λ . Drivers take their own utility into account, as well as the utility of others. Figure 10.2 shows the other vehicles involved in a lane change. The lane changing vehicle is indicated by a c , the new follower by a n and the old follower by a o .

The total utility for a driver is considered a weighted sum of the utility for himself and the other vehicles:

$$U_{\text{tot}} = U_c + \mathcal{P} \sum_{i \in \text{other drivers}} U_i = U_c + p(U_o + U_n) \quad (10.1)$$

The utility for the vehicle is expressed by its instantaneous acceleration a , as computed using the IDM car-following model (see section 8.3.3). The utility U for vehicle i is then expressed as

$$U_i = a_i = a_0 \left(1 - \left(\frac{v}{v_0} \right)^\delta - \left(\frac{s^*(v\Delta v)}{s} \right)^2 \right) \quad (10.2)$$

For the interpretation of the variables, we refer to section 8.3.3.

A lane change is performed if the utility of the driver for the other lane is at least a_{th} higher than the utility of the driver in the current lane. The variable a_{th} acts as a threshold variable in this case: as long as the utility gain is lower than that threshold, a driver will not change lanes. From a behavioral point of view, a_{th} can be seen as the cost of lane changing, which can differ per driver.

European driving rules

In Europe, driving rules dictate to stay right unless overtaking. In the United Kingdom, the rule is to stay left unless overtaking. In the description here, we will refer to left and right for tight hand driving as in continental Europe; for changes in the UK system, change left and right in the following description.

Two changes are made to the model:

1. The utility in the right lane is maximised at the utility of the left lane. By that change, one accounts for the fact that overtaking at the right is not allowed.
2. A bias towards the right is introduced, a_{bias} . This variable has a value larger than 0, and shows how much utility people attach to keeping right. A lane change to the right is performed if

$$U^{\text{right}} - U^{\text{left}} \geq a_{\text{th}} - a_{\text{bias}} \quad (10.3)$$

A lane change to the left is performed if

$$U^{\text{left}} - U^{\text{right}} \geq a_{\text{th}} + a_{\text{bias}} \quad (10.4)$$

10.5 Integrated modelling

Usually, models for lane changing separate a desire to change lanes from the manoeuvre itself, which is for instance modelled by gap acceptance Gipps (1986). The model *MOBIL*, as described in 10.4, incorporates the longitudinal accelerations into the choice for the lane. Alternatively, the integrated model by Toledo Toledo et al. (2007, 2009) starts with the lane change decision as lead and determines the acceleration.

Intuitively, one might think that drivers prepare for a lane change in their acceleration, leave gaps for others merging into the traffic stream and only gradually adapt their headways after someone merged in front, relaxation. These concepts are incorporated in the *LMRS* model, the Lane Change model with Relaxation and Synchronisation (Schakel et al., 2012).

Recent experimental (Keyvan-Ekbatani et al., 2016) findings show that drivers have four distinct lane change strategies:

1. Speed leading: drivers choose a speed and in order to keep that speed, they change lanes
2. Speed leading with overtaking: drivers choose a speed, and change lanes to overtake. In contrast to the speed leading strategy, drivers will speed up in order to reduce the time of overtaking.
3. Lane leading: drivers choose a certain lane and adapt their speed to the traffic in that lane
4. Traffic leading: drivers claim they “adapt to the traffic”, i.e. they do not have a certain lane or speed in mind.

Drivers expect that they drive “as anyone else”, and they are not aware that other drivers can follow a different strategy.

Selected problems

For this chapter, consider problems: 2, A.3.5, A.4.3, A.5.2, 137, 138, 182, 184, 191, A.9.4, 250

Chapter 11

Macroscopic fundamental diagram

The idea of a Macroscopic Fundamental Diagram (MFD) or Network Fundamental Diagram (NFD) is that rather than at the level of a link, at the level of an *area* there exists a relationship between the number of travellers on the road and the average speed of these travellers. Moreover, it could be argued that the noise in the measurements might be less. For individual detectors, one will find deviations from the fundamental diagram, (both upward and downward) which creates high scatter. Geroliminis and Daganzo (2008) showed that if one averages all detectors over a large area almost all scatter disappears (see figure 11.1). From a mathematical point, this makes sense since it simply is the law of large numbers. But although the concept seems simple, the effect might be large.

The essence of an MFD is that a high density affects the traffic flow to even under capacity. This is in contrast to a single road with a bottleneck, where in case of a high demand, the outflow will be at capacity (or queue discharge rate). This internal congestion can only take place if the (tail of) the congestion influences the throughput. This is the case with spill back effects, e.g. a tail of the queue growing backwards and thereby influencing drivers which want to take an exit which does not pass the bottleneck. A very much simplified example of this is given by Daganzo (2007), which proposed a single ring road with entrances and exits everywhere, see fig 11.2.

In MFDs, some terminology is different (see table 11.1 for an overview). Accumulation (A) is the total number of vehicles in a network, which can be expressed as total number of vehicles or number of vehicles per roadway length. Note that since the roadway length is fixed, these two are proportional. The accumulation can be seen as an equivalent of density on a road.

Production (P) is the internal flow in the network. This can be computed by Edie's definitions for all links in the network (equation 1.8). Performance (\mathcal{P}) is the outflow of the network, which is the sum of the flow of the outgoing links. Geroliminis and Daganzo (2008) shows there is a strong relationship between the production and the performance. This relationship for empirical data is shown in figure 11.4. The ratio of production and performance is the length of the trip within the zone. (As a thought experiment: if one needs increases the trip length inside the zone by a factor two, the internal flow, and hence the production, needs to increase by a factor two before the same outflow, performance, is reached).

This chapter first discusses what could be a possible control application for the MFD, before continuing to conditions under which the MFD holds (section 11.2). Then, section 11.3 discusses a way to include the MFD into a simulation model, and the chapter ends with some recent developments.

Table 11.1: Variables for the MFD

Name	symbol	meaning
Accumulation	A	Number of vehicles in the network (veh, or veh/km)
Production	P	Internal flows in the network (veh/h)
Performance	\mathcal{P}	Outflow out of the network (veh/h)

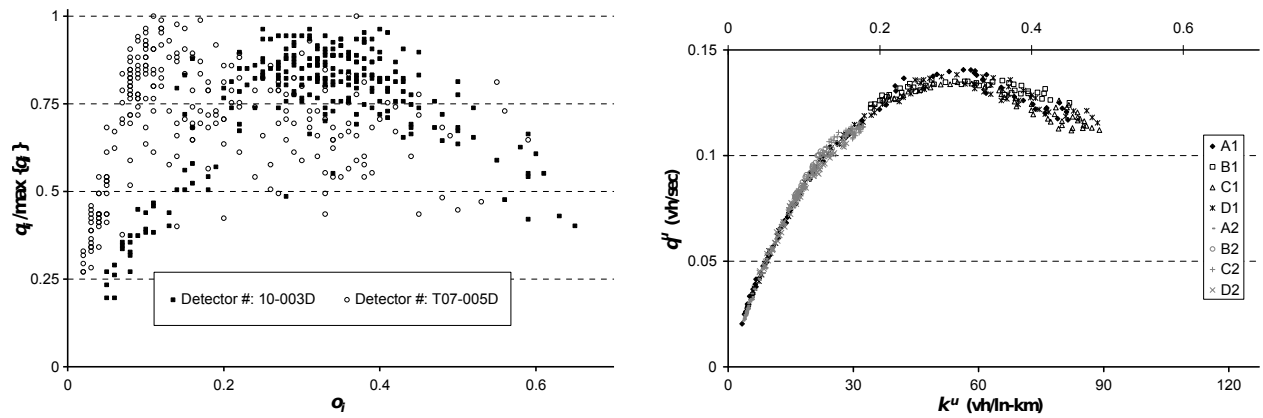


Figure 11.1: The first Macroscopic Fundamental Diagram constructed from data, from Geroliminis and Daganzo (2008).

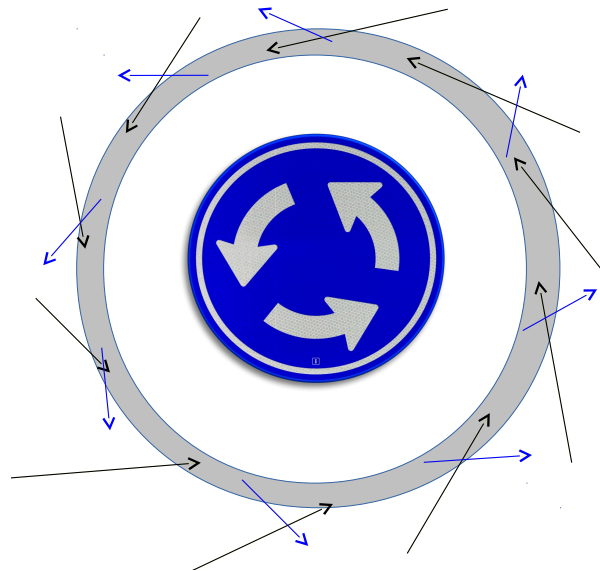


Figure 11.2: A simplified network congestion influences the outflow.

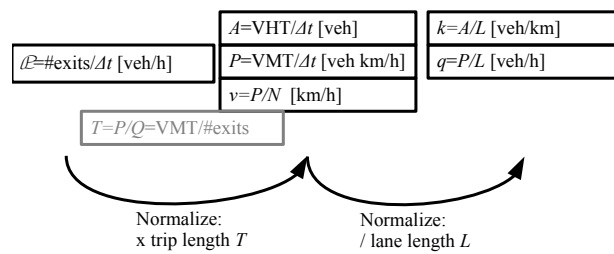


Figure 11.3: The relation between the different quantities related in the MFD

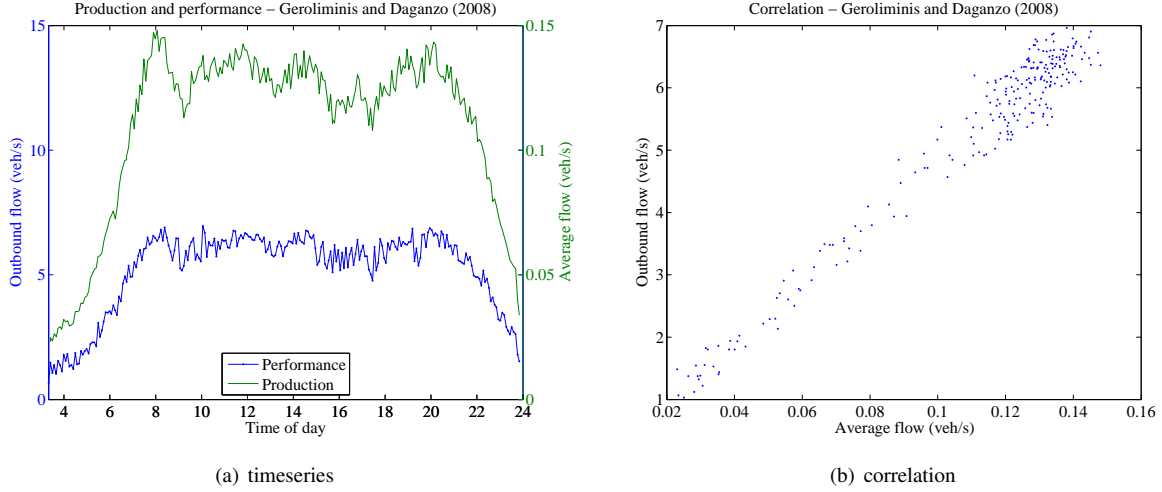


Figure 11.4: The relation between the production and the performance

11.1 Perimeter control

The idea behind perimeter control is as follows. As the production decreases with an increasing accumulation, it might be better to limit the accumulation in a zone, the so called protected network. Let's consider for the sake of simplicity the situation, with one zone which has this limitation, and storing vehicles outside the network will not affect traffic operations in the neighbouring zones (of course the waiting vehicles themselves are affected).

If we assume a constance trip length, for instance by assigning random exits around the ring road, the production will decrease as well. This causes an escalating effect of an further increasing accumulation and a further decreasing outflow. An example can be found in figure 11.5. This principle will now be discussed.

The top figure show the cumulative inflow curve (upper curve, indicated $A(t)$ – note that in this example, the original notation from (Daganzo, 2007) will be used), and the cumulative outflow curve without ($L(t)$) and with perimeter control ($L^*(t)$). The inflow curve is externally given, as is the MFD showing the production (outflow, G in this example) as function of accumulation (lower figure, n in the example, so the line is indicated $G(n)$). The accumulation in the system can be found by the difference between the inflow and outflow. Only the outflow at $t=0$ is specified, which equals 0, leading to the accumulation $n(0)$, which happens to be greater than the critical accumulation μ .

The dynamics of the outflow can now be predicted. In case of no perimeter control, the performance is governed by the MFD, which is the derivative of the outflow function. In the example $n(0) > \mu$, so the traffic is in a congested state, and the outflow can be read from $G(n)$. This outflow is lower than the inflow into the system, and as a consequence, the accumulation increases, leading to a decreasing outflow. Hence, the cumulative outflow curve $L(t)$ flattens. Once the accumulation increases to ω , the maximum number of vehicles in the road, the outflow reduces to 0.

Perimeter control entails limiting the inflow into the ring, and keep this at the level of the critical accumulation where the outflow is highest, i.e. not exceed μ . The inflow curve with the restriction is indicated with $A^*(t)$ in the figure. It starts with not letting any vehicles in until the accumulation is equal to μ . By consequence, the outflow increases over this time, since the accumulation becomes closer to μ , and hence the outflow closer to the maximum outflow γ . Once the accumulation is reduced to μ , the outflow is γ ; to maintain this number of vehicles, the same amount of vehicles are left into the system. Once the queue is solved, i.e. no more vehicles have to wait to get into the system, the perimeter control stops. The outflow curve constructed in this way is indicated as $L^*(t)$.

The perimeter control comes at a cost, the waiting time outside the network. This can be indicated in the figure as the area between lines A^* and A . The benefit is the higher outflow, which is the shaded area between L^* and L . Note that the benefits exceed the cost.

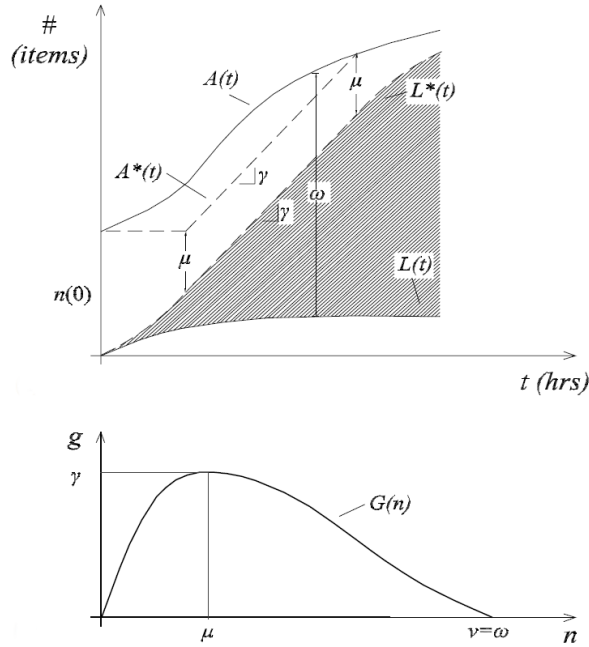


Figure 11.5: The effect of perimeter control in cumulative curves, figure from Daganzo (2007).

11.2 Traffic dynamics

A very strict claim on the application of the MFD is that it only holds if the traffic conditions are homogeneous throughout the network. In that case, all links in the area have a similar density, and the MFD simply is an average of all the same traffic states; the average then is that traffic state. In Cassidy et al. (2011) it has been shown what the averaging effects are in case a triangular fundamental diagram is assumed for the underlying links.

Figure 11.6 shows the effect of averaging two traffic states. If both states lie on the free flow branch, the average also lies on the free flow branch. If both lie on the congested branch, the average also lies on the congested branch. Only if one point lies on the congested branch and one point at the free flow branch, the average does not lie on either branch, but under the fundamental diagram. With a similar reasoning it can be shown that the average traffic state always lies *under* the fundamental diagram for one link if the fundamental diagram is concave.

One can continue this arguing and find that the larger the spread is, the further the average flow deviates from the flow which would match the average density according to the fundamental diagram. In an extreme case, some links are empty ($q=0$, $k=0$), and other links are jammed ($q=0$, $k=k_j$). All links then have a flow of 0, so the average flow also equals 0. However, the flow matching the average density, somewhere between $0 < k < k_j$ in the fundamental diagram is larger than 0.

11.2.1 Approaches to include the standard deviation

It hence makes sense to include the spread of the densities as second explanatory variable besides the average density.

One can show the effects of the network dynamics is by performing a traffic simulation study and analysing the results (Knoop et al., 2015). One of the simplest network setups is a Manhattan grid network (one way streets in a square grid) with periodic boundary conditions. Periodic boundary conditions mean that traffic exiting at the right of the network enters at the left and traffic from exiting at the top enters at the bottom and vice versa. The network structure is shown in figure 11.7.

When the traffic starts to run, various distributed bottlenecks become active. This is shown in figure 11.8b. After some time (figure 11.8d-f), traffic problems concentrate more and more around one location. The number of vehicles

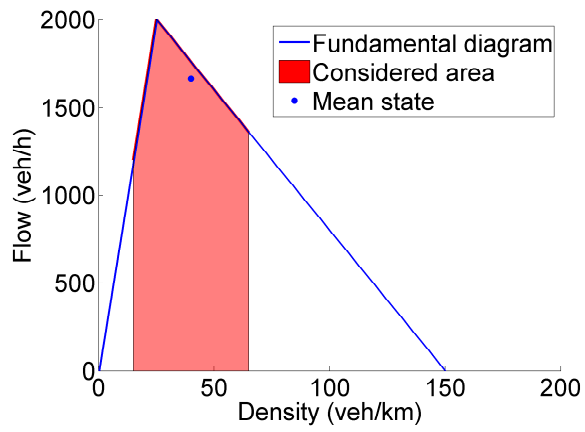


Figure 11.6: The construction of the average traffic state for two states on a triangular fundamental diagram.

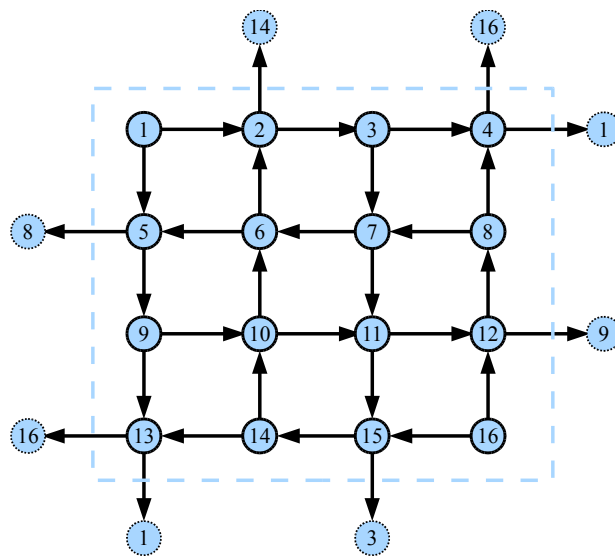
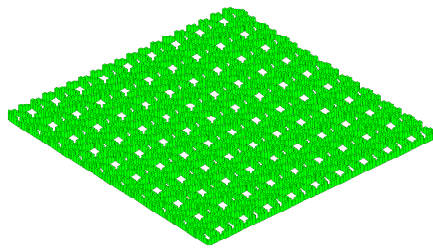
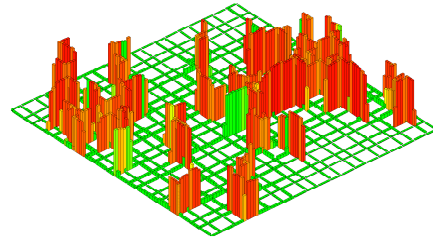


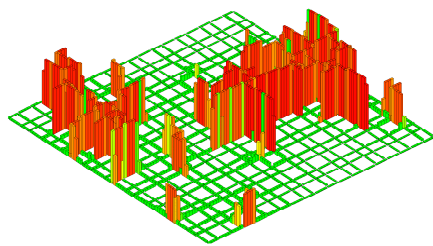
Figure 11.7: Illustration of a 4x4 grid network with periodic boundary conditions



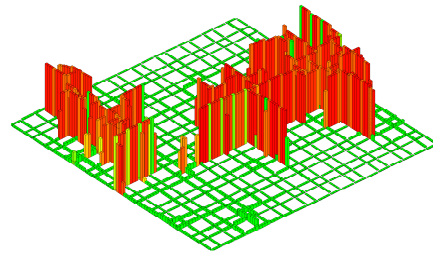
(a) start of the simulation



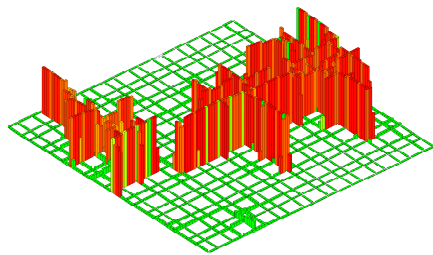
(b) 0.5 hour



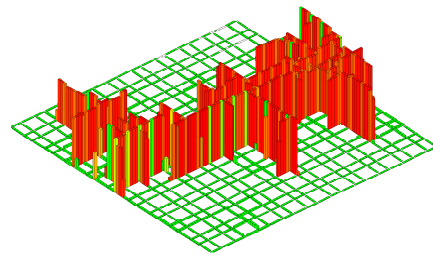
(c) 1 hour



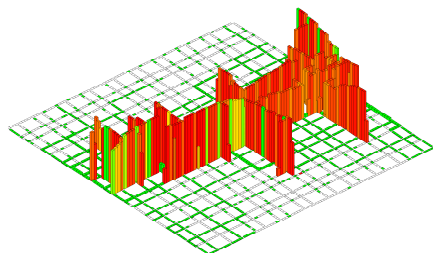
(d) 1.5 hour



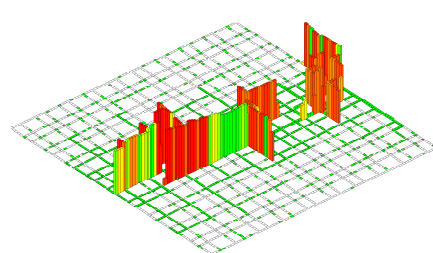
(e) 2 hour



(f) 3 hour



(g) 3.5 hour



(h) 4 hour

Figure 11.8: Evolution of the densities (bar heights) and speeds (colours) in the network

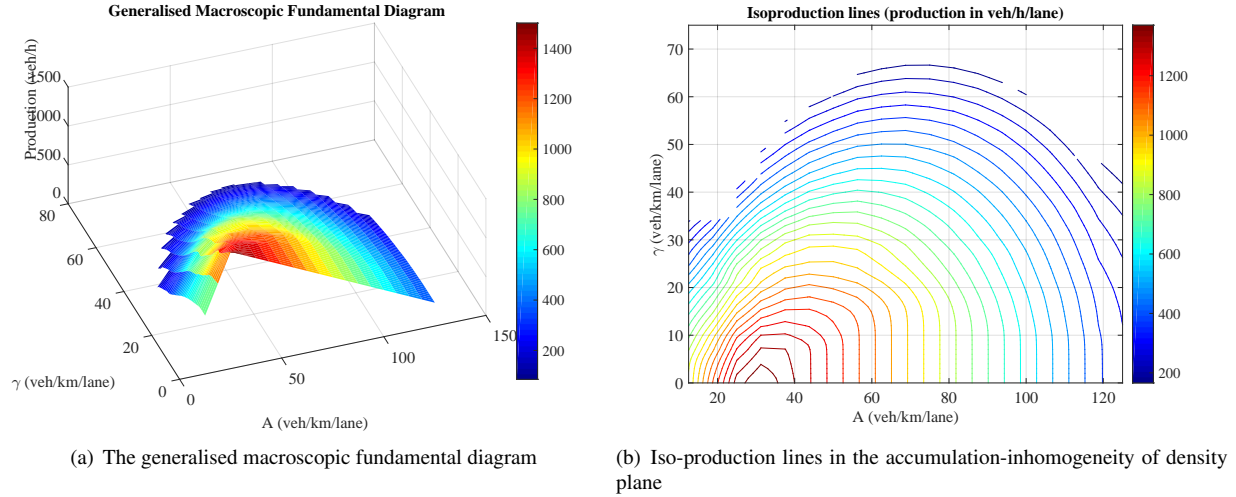


Figure 11.9: The generalised macroscopic fundamental diagram

in the rest of the network reduces, ensuring free flow conditions there. This complete evolution can be found in figure 11.8a-f.

This indicates that with this second explanatory variable, the traffic flow can be approximated reliably. We thus define a concept, the generalised fundamental diagram (GMFD) which predicts the production as function of the accumulation and the standard deviation of density (Knoop et al., 2015)

$$P = P(A, \sigma_A). \quad (11.1)$$

Figure 11.9(a) shows the GMFD. Figure 11.9(b) shows the same surface, but now in isoproduction lines. The production decreases once the inhomogeneity increases, and that this holds for every accumulation.

11.3 Simulation

Since there is a relation between the number of vehicles in a zone and the outflow, also a dynamic simulation model can be developed. This is a recent development, see e.g. Knoop and Hoogendoorn (2015) for the Network Transmission Model. In this model, an area is divided into zones, and the traffic flow is calculated using the MFDs.

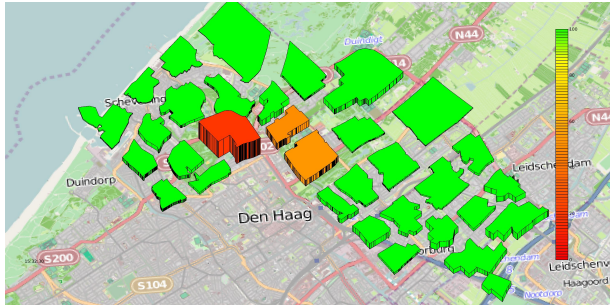
In each of the MFDs, the principle as described in the beginning of this section is implemented, where the accumulation determines the outflow. The interesting part of this concept is that, contrary to the isolated example in 11.1, the queuing outside the protected network also influences the traffic flow in that zone. Hence, there is a trade-off between letting vehicles into a protected zone, delaying the protected zone, or letting them wait outside, delaying the vehicles outside. Also, routing around the protected zone is an option, at the cost of more traffic outside (Hajiahmadi et al., 2013).

This model has been applied for the city of The Hague (Knoop et al., 2016), with a good result, showing that the rough approach works in giving the approximately right results for traffic states.

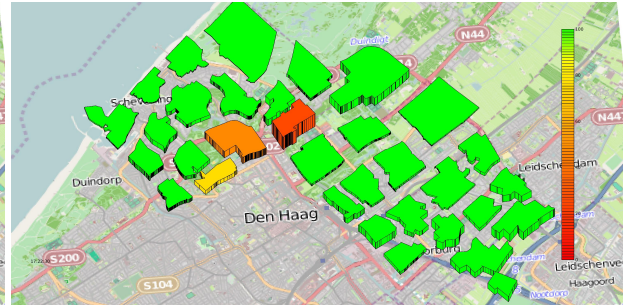
11.4 Recent insights

The field of the MFD is actively studied. The simulation models of which one example is described above in section 11.3 are actively studied, but there are other approaches as well. The division of space into different zones is actively studied, since one would like to have homogeneous areas, see Ji and Geroliminis (2012)

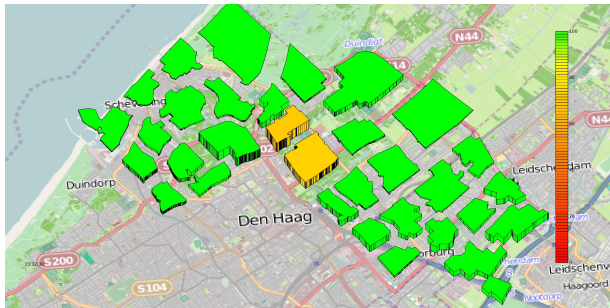
An interesting development is to estimate the MFD from scratch, without measurements. For fundamental diagrams, such estimates are possible. Laval and Castrillón (2015) uses an interesting technique to do the same for a



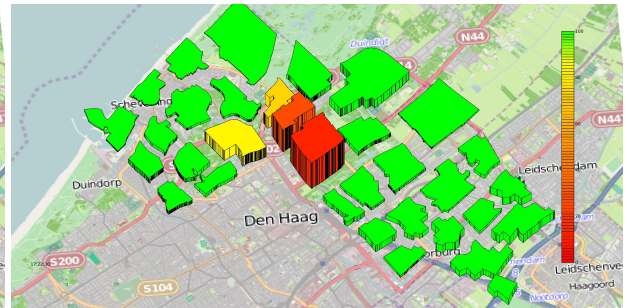
(a) Initial parameters, first part of simulation



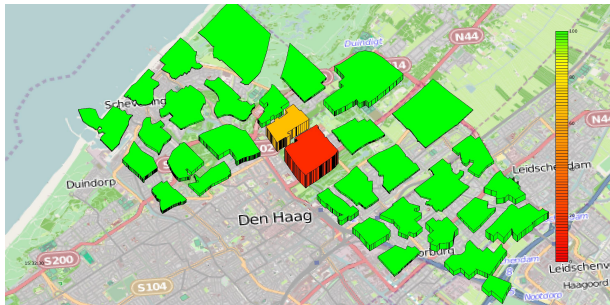
(b) Initial parameters, last part of simulation



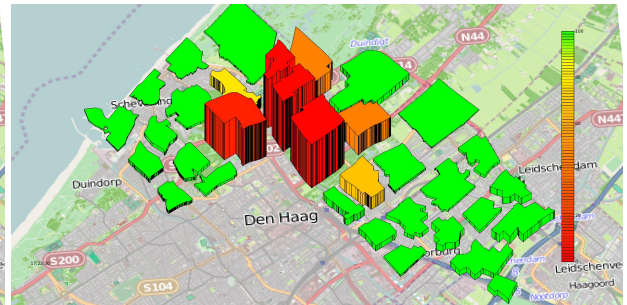
(c) Adapted parameters, first part of simulation



(d) Adapted parameters, last part of simulation



(e) Adapted parameters, accident, first part of simulation



(f) Adapted parameters, accident, last part of simulation

Figure 11.10: Screen shots of the simulation. The color indicates the speed relative to the free flow speed, and the height the accumulation, figure from Knoop et al. (2016)

zone, simplified to a ring road with random traffic lights. This paper follows other work, for instance by Leclercq and Geroliminis (2013).

Finally, the route length is not constant. Leclercq et al. (2015) indicates that the traffic patterns might lead to people using a different, non-shortest, route, thereby influencing the relationship performance-production. All in all, some aspects of the MFD still need studying, but the concept is perceived as promising.

Selected problems

For this chapter, consider problems: 26, 27, 86, 87, A.5.5, 157, 158, 159, 164, 203, 215, A.10.6

Chapter 12

Use of traffic models

Traffic simulation models are a very useful tool to assess the impact of a road design or a new traffic management measure. In assessing measures, we differentiate between ex ante and ex post analyses. This means respectively that the analysis is carried out before the measure is implemented in practice, or after. Especially in ex ante analyses, traffic models are very useful.

The traffic flow theory and proposed simulation tools as discussed in this reader can form a useful basis to perform these analyses. However, they need to be used with care. This chapter describes some steps a researcher or engineer needs to take before the models can be used. These steps are calibration (section 12.3) and validation (section 12.3) of the models. Section 12.2.2 discusses the stochasticity of models, and how to handle this. The last section discusses examples where it can go wrong. Before the steps are taken the goal of the model has to be defined, which will be explained in the following section.

12.1 Goal of the model

The goal of the model has to be defined in advance and the aspects the performance of the model will be judged upon also have to be defined in advance. This is called the measure of performance or measure of effectiveness. Examples of this measures of effectiveness are:

- average speed at (x,t)
- travel time
- delay

Even if the measure of performance has been set, it has to be determined how this will be measured. This is called the goodness of fit. This can be for instance the root mean square error of the travel time.

12.2 Type of models

Traffic models can be differentiated at different dimensions. First, we differentiate the level at which a model operates. Furthermore, the model might have one or more driver/vehicle types. Finally, another dimension is the stochasticity included.

12.2.1 Level

There are different levels at which one can simulate traffic. The levels considered in this course are

- Microscopically

- Macroscopically
- (Network level)

In case of microscopic simulation, one describes all vehicles. In case of macroscopic simulation, one describes the traffic states on the road. Hence, this is one level higher than the microscopic simulation. In chapter 11 the macroscopic fundamental diagram is introduced, which relates traffic variables at a network level (a level even higher than the road level). Also on this network level, simulations are possible, e.g. Knoop and Hoogendoorn (2014). In this reader, we only consider traffic simulations with dynamics. Often, in planning, static assignment models are used: these are not considered here.

The choice of the level of simulation depends on the requirements, for instance with regard to the:

- unknown items (e.g., effect of influencing driving behavior, connected vehicles)
- network size
- allowed time for the simulation

The most important reason to choose a microscopic simulation model is if one wants to analyse the effects of individual behaviour on the traffic operations.

12.2.2 Stochasticity

Many traffic simulation models are stochastic. That means that not all simulation *runs* are the same. The runs can be seen as representation of different days for which the same input conditions hold. Typical changes from run to run are:

- Moment of entry into simulation, i.e. headway.
- Car/driver specific:
 - driver type
 - routing information
 - equipped driver (connected)

To get a representative idea of the traffic situation, multiple random seeds (also called replications or iterations) are required. Generally, it is advised to use proper statistics to determine the right number of random seeds. A good way to assess this is to first test what the model needs to represent, the so called measure of effectiveness. In a few runs, determine the standard of this measure of effectiveness for various runs. Also determine the required accuracy of the measure of effectiveness for the study at hand. A very accessible is found in Driels and Shin (2004).

Let's consider an example. Suppose one wants to assess the average travel time in a simulation and one would like to know with 95% certainty that the calculated travel time does not differ more than 15% from the mean from the real. Several test runs show as initial values a mean travel time of 28 minutes (\bar{x}), and a standard deviation (variation between the different random seeds, not variation between the drivers) of 3 minutes (σ), which is the maximum allowed error (ϵ_{\max}). From statistics, we know that 95% of the observations fall within a margin of 1.96 standard deviations, so we choose a z -value of 1.96.

From statistics it is known that the bandwidth for the mean depends on the number of replications:

$$\epsilon_{\max} = \frac{zS}{\sqrt{n}} \quad (12.1)$$

In this equation, z is used to obtain the likelihood the observation is in between the bandwidth (1.96 in the example case). S is the standard deviation of the process, here approximated by the standard deviation of the test set σ , 6 minutes. n is the number of replications, to be determined. The maximum error is 5% of the mean of the process, here estimated by 5% of the mean of the test set, being 5% of 28 minutes, is 1.4 minutes.

Inversing equation 12.1 gives the equation for the required number of random seeds:

$$n \geq \left(\frac{zS}{\epsilon_{\max}} \right)^2 \quad (12.2)$$

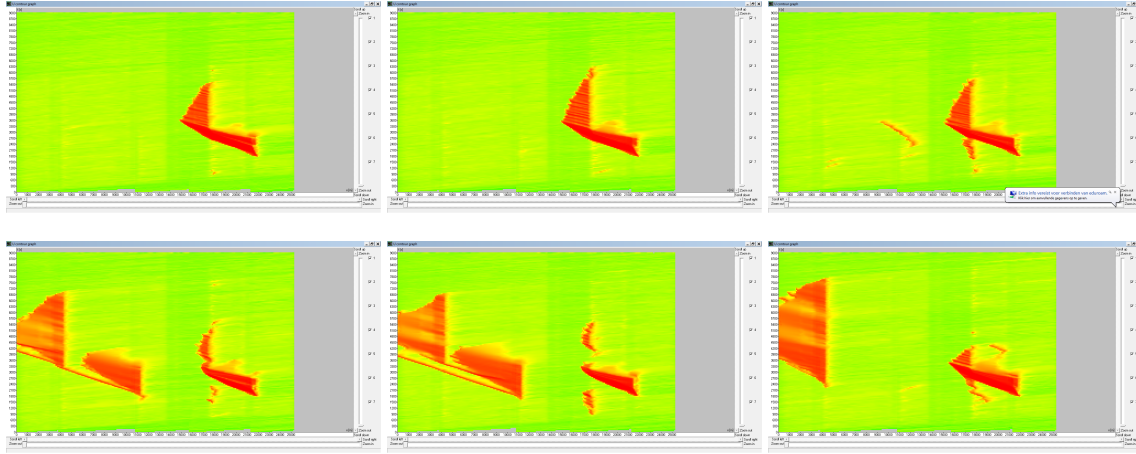


Figure 12.1: Examples of different random seeds in a simulation model. Colors indicate speed in a time-space plane (space is horizontal, time increases from bottom to top)

Filling the values for the example, we obtain:

$$n \leq \left(\frac{1.966}{4.2} \right)^2 \approx 70 \quad (12.3)$$

This process can be used. Note that the derivation assumes that the estimation for S is accurate, so one needs already a small set of replications to estimate this. Alternatively, one can check at the end whether the used number of replications also holds if S is re-evaluated based on all runs. Moreover, it is a stochastic process and the equations assume a normal distribution. They hence can only be applied for larger sets of replications.

Finally a note from what is being used in practice. Often, due to the long computation times of traffic simulation programs – especially microscopic simulation times – traffic engineers consider a “manual inspection” of the typical patterns, and use 10-15 replications. This will hence not give a statistically significant outcome.

12.2.3 Different user classes

Moreover, a traffic model can include different user classes. For instance, this could be trucks and passenger cars, but one can include more classes: different destinations, different aggressiveness of driving, different type of information.

12.3 Calibration

The goal of the calibration is to make the model representative to the reality. The background will be discussed in the next section. Section 12.3.2 will provide some techniques for calibration.

12.3.1 Use of calibration

Whereas some aspects of traffic are universal (conservation of vehicles), the driving behaviour is not constant. It might differ for instance per:

- Road layout
- Day of the week
- Weather condition
- Lighting condition

- Region/country
- Time of the day (including peak / non peak)

That also means that developers of the model cannot provide a model which can be used in any condition. Therefore, the user has to change the parameters in the model such that it fits the situation he wants to use the model for.

The calibration entails adapting the driving parameters such that the model is in agreement with reality. It is therefore essential that the user has data of traffic available to calculate the goodness of fit of the model.

For microscopic models, if the microscopic behaviour has to be represented correctly, it is needed that microscopic data is available. For an overview of the techniques and uses of microscopic calibration and validation, we refer to the thesis of Ossen (2008). Some microscopic models only aim at representing macroscopic characteristics. For these cases, the model can be calibrated using macroscopic data that uses macroscopic measures of performance. It can not be assumed, though, that the underlying microscopic properties are correct.

The end result of a calibration is a model including a parameter set which is representing the situation for which it has been calibrated. To test and check its predictive power for other situations, a validation (section 12.3) is carried out.

12.3.2 Techniques

The idea is to get the best performance of the model, i.e. optimizing the goodness of fit. In this section, two frequently used values will be discussed, being the root mean square error and the log-likelihood.

Root mean square error

An often used measure to indicate the quality of the simulation is the root mean square error, or RMSE. For instance the RMSE of the speeds at each time and space interval indicates how far the speeds are off “on average”. The root mean square error is the difference in speed (or in general: the indicator) squared, and then averaged over all observations, in most cases several observations over space and time. Of this average of squares, one takes the mean to get an value for the difference. This gives an indication how far the speeds are different from the base values.

Note that the RMSE of speeds is not always a good measure. For instance, speeds for the free flow branch, the traffic state can differ considerably, with an (almost) equal speed. Choosing density as predictor for a traffic state is more meaningful as representative of the traffic state. However, the core of the calibration process lies in which is the measure of performance the user wants to reproduce. If the user is satisfied if the speeds are correctly predicted and the traffic states are off, the RMSE of speeds can be a good way. Moreover, if there are stop-and-go waves which originate at random times, the RMSE of speed can be very far off if the waves are predicted in the “other phase” (i.e., start is predicted when traffic is stopped and vice versa). In that case, all speeds are wrong, and a simulation predicting no congestion would be better, although from a traffic flow perspective that is further from the truth. All in all, it lies in the requirements for the user: if the user really wants speeds, minimising the RMSE might be a good option.

Log-likelihood

For stochastic models, the model predicts the outcome of a certain traffic state with a probability. Let us denote the probability on a traffic state $P(S|\Pi)$. This depends on the parameters of the model, Π . The likelihood indicates how likely it is that the data is found given the model. Assuming independency between the observations, one can express the likelihood as:

$$L(\Pi) = \prod_{\text{All observed data}} P(S_{\text{observed}}|\Pi) \quad (12.4)$$

Theoretically, one likes to maximize the likelihood of the model giving the observations by adjusting the parameters. Hence, the optimal parameter set Π^* is found by:

$$\Pi^* = \arg \max_{\text{par set}} L(\Pi) \quad (12.5)$$

The likelihood is very small. That is because each datapoint contributes a multiplicative factor of 0 to 1 to the likelihood, being the probability that the model with that parameter set predicts that outcome. For many observations,

that value will be very small. For computational reasons, it might therefore be advisable to maximize the logarithm of the likelihood instead, also called the loglikelihood.

The loglikelihood \mathcal{L} is defined as

$$\mathcal{L} = \log L \quad (12.6)$$

Because the likelihood is a product of probabilities, the log likelihood changes into a sum of the logs of the probabilities:

$$\mathcal{L} = \log L = \sum_{\text{All observed data}} \log P(S_{\text{observed}}|\Pi) \quad (12.7)$$

12.3.3 Number of parameters

A higher number of parameters gives more degrees of freedom to fit the model to the data. However, this also comes at a risk of overfitting. One might choose the parameters to best fit the data, but the interpretation of the parameters could be wrong because the parameters are actually fitted random effects in the data rather than the underlying structure of the data.

For model developers, the advice is that a parsimonious model should be used – a model as simple as possible which represent the data. For model users, the advice is to only fit the parameters which can be estimated reliably and which have an influence on the data which is collected.

A typical example of where too many parameters are estimated is in one aims to calibrate a microscopic model, including all driver parameters, using macroscopic data. As is indicated in Ossen (2008), one cannot calibrate a microscopic model using macroscopic data since many combinations of parameters in the microscopic model lead to the same macroscopic traffic patterns. If one would like to calibrate the microscopic model nonetheless, one should refer to microscopic data.

12.4 Validation

The section describes the validation of a model. In the validation, is is tested how well the model is performing for the cases it is intended for.

12.4.1 Need of validation

The result of a calibration is a model and parameters which are optimized. The purpose of validation is checking whether the model indeed does as it is intended to. It could be that all data from the calibration fits perfect, but for the cases in validation there are other patterns. In that case the model is calibrated, but not validated. In general, the calibration consists of finding an optimal parameter set, for which no specific quality level needs to be given. For the validation, the goal of the model must be set, as well as a validity range.

The validity range is the range for conditions under which the model is working at a quality level defined by the user on beforehand. This validity range could be the same conditions as the validation, another day, another location, another country, another number of lanes – this is to be specified by the user. However, note that the model is only validated for those conditions the validation has been carried out for. For example, if the validation is carried out for a similar day on the same road layout, it is not necessarily a correct model for another road layout.

The essence of validation is to make sure the model indeed performs to the required level. Before that is done, no statements of the quality of the model can be made.

12.4.2 Data handling for calibration and validation

For calibration and validation different data sets should be used. This prevents for problems of overfitting: if the parameters are fit to the specific (random) properties of the data, this should not show in the validation.

If the validity range is different from the calibration, one data set could be used for the calibration and another dataset can be used for validation. That could for instance be two different locations. If no specific conditions could be identified, the data should at random be split in a part for calibration and validation. A typical distribution is to allow 2/3 for calibration and 1/3 for validation.

12.4.3 Techniques

As mentioned before, the first thing one needs to do is set the aims for the model: under which conditions the model needs to perform at which level. These are preferably intuitive measures; for instance a log-likelihood value is hard to interpret and hence not very useful.

The process then is straightforward: run the model with the correct input variables, and then consider the outcome in the chosen measure of performance and goodness of fit. To which extent does it meet the required (or desired) criteria.

For instance, we want to validate a macroscopic traffic flow model for another day than the day used for the calibration. Data is available for that day, showing the flows and the speeds. We require that with the right inflow, the RMSE of the speeds, measured at each km and aggregated over 5 minutes is not more than 5 km/h of the data. The inflow at the beginning of the road stretch is put into the model, the model predicts the speeds. These are compared with the data, and the RMSE of the speeds is calculated. If the RMSE is below 5 km/h, the model is validated. For a good overview of calibration and validation, see chapter 16 of Treiber and Kesting (2013).

12.5 Often made mistakes

In traffic engineering this often goes wrong. In this section, some examples are given.

The first, and most serious mistake is that uncalibrated models are being used. That could mean that a model is developed such that some behaviour is in there. For commercial micro simulation packages and drivers on freeways, that means that typical car-following behaviour is implemented, just as a lane change model. However, drivers drive differently all over the world and in different conditions. If one would simply implement a road layout and put it in the specific package assuming that the drivers drive as the developer put into the model, the risk of having a very wrong model is large. This risk is further enhanced by the fact that the vehicle trajectories look realistic. This is because the underlying car movements make sense. However, they are not necessarily true for the case at hand.

Calibrated but unvalidated models are also common in practice. Data is being collected and parameters of the model is optimized. However, without validation, one knows the model is the best prediction possible (although a risk of overfitting exists), but one does not know how good it is. It can be very far off the reality.

In microsimulation a vehicle demand is given. It can happen that the tail of congestion in the network is spilling back to the entry of the network. In that case, the demand cannot be put on the network due to the congestion. Various simulation programs then act differently. Some will not generate new vehicles, whereas others store the vehicles in “vertical queues”. Since it is generally not known what models do, it is best practice to avoid congestion spilling back to the network entry. Note that network entries also can be onramps halfway the network. In this case, one can consider elongating the onramp.

The final mistake commonly made is the validated models outside their validation range. For instance, a model could be validated for Dutch freeways with no slope at a speed limit of 100 km/h and dry weather conditions. That model, with those parameter settings, is then only validated for that range. A road in Italy, or road with slopes, or with a different speed limit or with different weather conditions would then fall outside the validation range.

Selected problems

For this chapter, consider problems: 163, 220, 222

Alphabetical Index

- acceleration fan, 50
- Accumulation, 89
- Binomial distribution, 10
- capacity, 26
- capacity drop, 55, 56
- Car-following models, 63
 - Newell, 63
- cell transmission model, 72
- characteristic curve, 48
- composite headway distributions, 13
- congested branch, 27
- congested state, 27
- Courtesy lane changes, 83
- critical density, 27
- Critical gap, 14
- critical speed, 27
- Cumulative curves
 - Oblique cumulative curves, 20
 - Slanted cumulative curves, 20
- cumulative curves, 17
- cumulative flow curves, 17
- Delay, 19
- Demand functions, 72
- density, 2
- Desired lane changes, 83
- Drake fundamental diagram, 28
- dual loop detectors, 4
- Edie's definitions, 5
- ex ante, 99
- ex post, 99
- Exponential headway distribution, 12
- First order macroscopic modelling, 71
- flow, 2
- Free flow, 59
- free flow capacity, 56
- free flow speed, 27
- Fundamental diagram, 26
 - Drake, 28
 - Greenshields, 27
 - Inverse lambda, 28
 - Smulders, 28
 - Triangular, 27
 - Truncated triangular, 28
 - Wu, 28
- gap, 1
- generalised fundamental diagram, 95
- Godunov scheme, 72
- goodness of fit, 99
- Greenshields fundamental diagram, 27
- gross space headway, 1
- gross time headway, 1
- Headway
 - composite headway distributions, 13
 - distributions, 12
 - Exponential distribution, 12
 - Gross space headway, 1
 - Gross time headway, 1
 - Negative binomial distribution, 12
 - Net space headway, 1
 - Net time headway, 1
 - Time headway, 9
- headway, 9
- Headway distribution, 9
- homogeneous, 7
- Hysteresis, 29
- instantaneous measurements, 5
- Instantaneous measuring, 5
- Integrated lane change modelling, 87
- intensity, 2
- inverse lambda, 28
- Inverse lambda fundamental diagram, 28
- iterations, 100
- jam density, 27
- Kerner's Three Phase Traffic Flow Theory, 58

- kinematic wave, 48
- lag gap, 15
- Lagrangian coordinates, 74
- Lane change model
 - Integrated modelling, 87
 - microscopic, 83
 - MOBIL, 85
 - Slugs and rabbits, 83
- Lane Flow Distribution, 83
- lead gap, 15
- LFD, 83
- Lighthill, Williams and Richards, 72
- Link Transmission model, 73
- local mean speed, 5
- local measurements, 4
- Local measuring, 4
- local stability, 53
- LWR, 72
- macroscopic, 1
- Macroscopic Fundamental Diagram, 89
- Macroscopic models
 - First order modelling, 71
- Macroscopic traffic models, 71
- Mandatory lane changes, 83
- Marcoscopic traffic description, 2
- measure of effectiveness, 99
- measure of effectiveness, 100
- measure of performance, 99
- Measuring principles, 4
 - Instantaneous, 5
 - Local, 4
- mesoscopic, 4
- Mesoscopic traffic description, 4
- Method of characteristics, 47
- MFD, 89
- microscopic, 1
- Microscopic lane change models, 83
- Microscopic traffic description, 1
- Minimizing Overall Braking Induced by Lane Changes, 85
- MOBIL, 85
- MoC, 47
- moving bottleneck, 40
- moving observer, 31
- Multi-class modelling, 77
- Negative binomial distribution, 12
- net space headway, 1
- net time headway, 1
- Network Fundamental Diagram, 89
- Network traffic description, 4
- Network Transmission Model, 95
- Newell's car following model, 63
- NFD, 89
- numerical diffusion, 77
- oblique cumulative curves, 20
- occupancy, 3
- one pipe regime, 85
- outflow capacity, 55
- overfitting, 103
- pace, 1
- Passenger car equivalent, 80
- passenger car unit, 80
- PCE, 80
- Performance, 89
- Perimeter control, 91
- platoon stability, 53
- Poisson distribution, 10
- Production, 89
- Protected network, 91
- $q = ku$, 25
- queue discharge rate, 55
- Rabbits, 83
- random seeds, 100
- relaxation, 87
- remote sensing, 5
- replications, 100
- root mean square error, 102
- shock wave, 35
- Shock wave theory, 35
- Slanted cumulative curves, 20
- Slugs and Rabbits, 83
- Smulders fundamental diagram, 28
- space headway, 1
- spacing, 1
- spatio-temporal measuring, 5
- spatio-temporal principles
 - spatio-temporal, 5
- stationary, 7
- stop-and-go waves, 46
- string stability, 53
- Submicroscopic traffic description, 4
- Supply functions, 72
- Synchronized flow, 59
- throughput, 2
- Three phase Traffic Flow Theory, 58
- three phase traffic flow theory, 29
- time mean speed, 5

- Traffic description
 - Marcoscopic, 2
 - Mesosopic, 4
 - Microscopic, 1
 - Network, 4
 - Submicroscopic, 4
- Traffic flow
 - stationary, 7
- Traffic flow models, 99
- traffic flow stability, 55
- Traffic Model
 - Discretisation, 72
- Traffic model
 - Demand functions, 72
 - Link Transmission model, 73
 - Supply functions, 72
- Traffic Models
 - Macroscopic traffic models, 71
- Traffic simulation
 - Network Transmission Model, 95
- traffic state, 26
- Traffic states
 - Free flow, 59
- trajectory, 1
- Travel time, 19
- Triangular fundamental diagram, 27
- Trucks, 77
- Truncated triangular fundamental diagram, 28
- two pipe regime, 85
- uncongested branch, 27
- uncongested state, 27
- validity range, 103
- Variables
 - Fundamental relationships, 25
- variables, 1
- vertical queuing model, 17
- volume, 2
- wave speed, 42
- Wave speed equation, 36
- Wu fundamental diagram, 28

Bibliography

- Ahn, S. and Cassidy, M. (2007). Freeway traffic oscillations and vehicle lane-change maneuvers. In Allsop, R. E., Bell, M. G. H., and Heydecker, B. G., editors, *Proceedings of the International Symposium of Transportation and Traffic Theory*, pages 691–710. Elsevier, Amsterdam.
- Aw, A. and Rascle (2000). Resurrection of the “second order” models of traffic flow. *SIAM Journal on Applied Mathematics*, 60:916–938.
- Bando, M., Hasebe, K., Nakayama, A., Shibata, A., and Sugiyama, Y. (1995). Dynamical model of traffic congestion and numerical simulation. *Physical Review E*, 51(2):1035. Copyright (C) 2007 The American Physical Society Please report any problems to prola@aps.org PRE.
- Brackstone, M. and McDonald, M. (1999). Car-Following: A Historical Review. *Transportation Research F*, 2:181 – 186.
- Carlson, R. C., Papamichail, I., Papageorgiou, M., and Messmer, A. (2010). Optimal motorway traffic flow control involving variable speed limits and ramp metering. *Transportation Science*, 44(2):238–253.
- Cassidy, M. and Bertini, R. (1999). Some traffic features at freeway bottlenecks. *Transportation Research Part B: Methodological*, 33(1):25 – 42.
- Cassidy, M., Jang, K., and Daganzo, C. (2011). Macroscopic fundamental diagram for freeway networks: Theory and observation. In *Proceedings of the 90th Annual Meeting of the Transportation Research Board*.
- Cassidy, M. J. and Rudjanakanoknad, J. (2005). Increasing the capacity of an isolated merge by metering its on-ramp. *Transportation Research Part B: Methodological*, 39(10):896 – 913. ISSN 0191-2615.
- Chiabaut, N., Leclercq, L., and Buisson, C. (2010). From heterogeneous drivers to macroscopic patterns in congestion. *Transportation Research Part B: Methodological*, 44(2):299 – 308. ISSN 0191-2615.
- Chung, K., Rudjanakanoknad, J., and Cassidy, M. J. (2007). Relation between traffic density and capacity drop at three freeway bottlenecks. *Transportation Research Part B: Methodological*, 41(1):82–95.
- Daganzo, C. (2007). Urban gridlock: Macroscopic modeling and mitigation approaches. *Transportation Research Part B: Methodological*, 41(1):49–62.
- Daganzo, C. F. (1994). The Cell Transmission Model: a Dynamic Representation of Highway Traffic Consistent With the Hydrodynamic Theory. *Transportation research part B*, 28B(4):269–287.
- Daganzo, C. F. (1995). Requiem for second-order fluid approximations of traffic flow. *Transportation Research Part B: Methodological*, 29:277–286.
- Daganzo, C. F. (1997). *Fundamentals of Transportation and Traffic Operations*. Pergamon.
- Daganzo, C. F. (2002a). A behavioral theory of multi-lane traffic flow. part i: Long homogeneous freeway sections. *Transportation Research Part B: Methodological*, 36(2):131 – 158. ISSN 0191-2615.

- Daganzo, C. F. (2002b). A behavioral theory of multi-lane traffic flow. part ii: Merges and the onset of congestion. *Transportation Research Part B: Methodological*, 36(2):159 – 169. ISSN 0191-2615.
- Drake, J. S., Schöfer, J. L., and May, A. (1967). A statistical analysis of speed density hypotheses. In Edie, L. C., Herman, R., and Rothery, R., editors, *Proceedings of the Third International Symposium on the Theory of Traffic Flow*. Elsevier North-Holland, New York.
- Driels, M. R. and Shin, Y. S. (2004). Determining the number of iterations for monte carlo simulations of weapon effectiveness.
- Dynasmart (2003). DYNAMSMART-X – User’s Guide. Technical report, University of Maryland.
- Fortuijn, L. G. H. and P., H. S. (2015). Turbo roundabouts: Comparing capacity estimation on gap and flow level. In *Proceedings of the 94th Annual Meeting of the Transportation Research Board*.
- Geroliminis, N. and Daganzo, C. F. (2008). Existence of urban-scale macroscopic fundamental diagrams: Some experimental findings. *Transportation Research Part B: Methodological*, 42(9):759–770.
- Gipps, G. P. (1986). A model for the structure of lane-changing descisions. *Tranportation Research Part B: Methodological*, 20:403–414.
- Godunov, S. K. (1959). A difference scheme for numerical computation of of discontinuous solutions of equations of fluid dynamics. *Math. Sb.*, 47:271 – 290.
- Greenshields, B. D. (1934). A Study of Traffic Capacity. *Proceedings Highway Research Board*, 14:448–477.
- Hajiahmadi, M., Knoop, V. L., De Schutter, B., and Hellendoorn, H. (2013). Optimal dynamic route guidance: A model predictive approach using the macroscopic fundamental diagram. In *Intelligent Transportation Systems- (ITSC), 2013 16th International IEEE Conference on*, pages 1022–1028. IEEE.
- Hall, F. L. and Agyemang-Duah, K. (1991). Freeway Capacity Drop and the Definition of Capacity. *Transportation Research Record: Journal of the Transportation Research Board No.1320*, pages 91–98.
- Heikoop, H., editor (2011). *Capaciteitswaarden Infrastructuur Autosnelwegen*. Dienst Verkeer en Scheepvaart.
- Helbing, D., Hennecke, A., and Treiber, M. (1999). Phase diagram of traffic states in the presence of inhomogeneities. *Physical Review Letters*, 82(21):4360.
- Helly, W. . (1959). Simulation of bottlenecks in single lane traffic flow. In *Proceedings of the Symposium on Theory of Traffic Flow*, pages 207– 238. General Motors Research Laboratories, Elsevier, New York.
- Hoogendoorn, S., Hoogendoorn, R. G., and Daamen, W. (2011). Wiedemann revisited. *Transportation Research Record: Journal of the Transportation Research Board*, 2260(1):152–162.
- Hoogendoorn, S. P. (2005). Unified approach to estimating free speed distributions. *Transportation Research Part B: Methodological*, 39(8):709–727.
- Ji, Y. and Geroliminis, N. (2012). On the spatial partitioning of urban transportation networks. *Transportation Research Part B: Methodological*, 46(10):1639–1656.
- Kerner, B. S. (2004). *The Physics Of Traffic: Empirical Freeway Pattern Features, Engineering Applications, And Theory*. Springer, Berlin.
- Keyvan-Ekbatani, M., Daamen, W., and Knoop, V. (2016). Categorization of the lane-change decision process on freeways. *Transportation Research part C*.
- Knoop, V., Tamminga, G., , and Leclercq, L. (2016). Network transmission model: Application to a real world city. In *proceedings of the 95th Annual Meeting of the Transportation Research Board*.

- Knoop, V. L. and Hoogendoorn, S. P. (2014). Network transmission model: a dynamic traffic model at network level. In *Transportation Research Board 93rd Annual Meeting*, number 14-1104.
- Knoop, V. L. and Hoogendoorn, S. P. (2015). An area-aggregated dynamic traffic simulation model. *European Journal of Transport and Infrastructure Research (EJTIR)*, 15 (2), 2015.
- Knoop, V. L., van Lint, H., and Hoogendoorn, S. P. (2015). Traffic dynamics: Its impact on the macroscopic fundamental diagram. *Physica A: Statistical Mechanics and its Applications*, 438:236–250.
- Knoop, V. L., Van Zuylen, H. J., and Hoogendoorn, S. P. (2009). *Proceeding of the International Symposium of Transportation and Traffic Theory*, chapter Microscopic Traffic Behavior near Accidents. Springer, New York.
- Koshi, M., Iwasaki, M., and Ohkura, I. (1981). Some findings and an overview on vehicular flow characteristics. In *Proceedings of the 8th International Symposium on Transportation and Traffic Theory*, pages 403–426. Univ. of Toronto Press, Toronto.
- Kotsialos, A., Papageorgiou, M., Diakaki, C., Pavlis, Y., and Middelham, F. (2002). Traffic flow modeling of large-scale motorway networks using the macroscopic modeling tool metanet. *Intelligent Transportation Systems, IEEE Transactions on*, 3(4):282–292.
- Laval, J. and Castrillón, F. (2015). Stochastic approximations for the macroscopic fundamental diagram of urban networks. In *Transportation Research Procedia*, volume 7, page 615630.
- Laval, J. A. (2011). Hysteresis in traffic flow revisited: An improved measurement method. *Transportation Research Part B: Methodological*, 45(2):385 – 391.
- Leclercq, L., Chiabaut, N., Laval, J. A., and Buisson, C. (2007). Relaxation Phenomenon After Lane Changing. *Transportation Research Record: Journal of the Transportation Research Board*, No. 1999, pages 79–85.
- Leclercq, L. and Geroliminis, N. (2013). Estimating mfd in simple networks with route choice. In Hoogendoorn, S. P., Knoop, V. L., and Van Lint, H., editors, *Proceedings of the 20th International Symposium on Transportation and Traffic Theory*.
- Leclercq, L., Parzani, C., Knoop, V. L., Amourette, J., and Hoogendoorn, S. P. (2015). Macroscopic traffic dynamics with heterogeneous route patterns. *Transportation Research Part C: Emerging Technologies*, 59:292–307.
- Lighthill, M. J. and Whitham, G. B. (1955). On Kinematic Waves. II. A Theory of Traffic Flow on Long Crowded Roads,. *Proceedings of the Royal Society of London. Series A, Mathematical and Physical Sciences*, 229(1178):317 – 345.
- Newell, G. (2002). A simplified car-following theory: a lower order model. *Transportation Research Part B: Methodological*, 36(3):195–205.
- Newell, G. F. (1993). A simplified theory of kinematic waves in highway traffic, part ii: Queueing at freeway bottlenecks. *Transportation Research Part B: Methodological*, 27(4):289 – 303.
- Oh, S. and Yeo, H. (2012). Estimation of capacity drop in highway merging sections. *Transportation Research Record: Journal of the Transportation Research Board*, 2286(1):111–121.
- Ossen, S. J. L. (2008). *Longitudinal Driving Behavior: Theory and Empirics*. Trail thesis series, Delft University of Technology.
- Payne, H. J. (1971). Models of freeway traffic and control, mathematical models of public systems. *Simulation Council Proceedings Series*, 28(1):51–61.
- Pueboobpaphan, R. and van Arem, B. (2010). Understanding the relation between driver/vehicle characteristics and platoon/traffic flow stability for the design and assessment of cooperative cruise control. In *Proceedings of the 89th Annual Meeting of the Transportation Research Board*.

- Richards, P. I. (1956). Shock waves on the highway. *Operations Research* 4, 4:42 – 51.
- Schakel, W. J., Van Arem, B., and Knoop, V. (2012). Lmrs: An integrated lane change model with relaxation and synchronization. In *Proceedings of the 91st Annual Meeting of the Transportation Research Board*.
- Schreiter, T., Van Lint, H., Yuan, Y., and P., H. S. (2010). Propagation wave speed estimation of freeway traffic with image processing tools. In *Proceedings of the 89th Annual Meeting*.
- Smulders, S. (1989). Control of freeway traffic flow. *CWI Tract*, 80.
- Srivastava, A. and Geroliminis, N. (2013). Empirical observations of capacity drop in freeway merges with ramp control and integration in a first-order model. *Transportation Research Part C: Emerging Technologies*, 30:161–177.
- Toledo, T., Koutsopoulos, H. N., and Ben-Akiva, M. (2007). Integrated driving behavior modeling. *Transportation Research Part C: Emerging Technologies*, 15(2):96 – 112. ISSN 0968-090X.
- Toledo, T., Koutsopoulos, H. N., and Ben-Akiva, M. (2009). Estimation of an integrated driving behavior model. *Transportation Research Part C: Emerging Technologies*, 17(4):365 – 380. ISSN 0968-090X.
- Transportation Research Board, (2000). Highway Capacity Manual. Technical report.
- Treiber, M., Hennecke, A., and Helbing, D. (2000). Congested traffic states in empirical observations and microscopic simulations. *Physical Review E*, 62(2):1805.
- Treiber, M. and Kesting, A. (2013). *Traffic Flow Dynamics; Data, Models and Simulation*. Springer.
- Treiber, M., Kesting, A., and Helbing, D. (2006). Delays, inaccuracies and anticipation in microscopic traffic models. *Physica A: Statistical Mechanics and its Applications*, 360(1):71–88.
- Van Lint, J., Bertini, R. L., and Hoogendoorn, S. P. (2014). Data fusion solutions to compute performance measures for urban arterials. In *Symposium Celebrating 50 years of Traffic Flow Theory 2014 FTF Summer Meeting, Portland (USA), 11-13 August, 2014*. TRB.
- van Lint, J. W., Hoogendoorn, S. P., and Schreuder, M. (2008). Fastlane: New multiclass first-order traffic flow model. *Transportation Research Record: Journal of the Transportation Research Board*, 2088(1):177–187.
- Van Wageningen-Kessels, F. L. M. (2013). *Multi-class continuum traffic flow models: Analysis and simulation methods*. Ph.D. thesis, Delft University of Technology.
- Wiedemann, R. (1974). *Simulation des Strassenverkehrsflusses*. Heft 8 der Schriftenreihe des ifv, Universitt Karlsruhe.
- Wu, N. (2002). A new approach for modeling of Fundamental Diagrams. *Transportation Research Part A: Policy and Practice*, 36(10):867–884. Doi: DOI: 10.1016/S0965-8564(01)00043-X.
- Yperman, I., Logghe, S., Tampère, C. M. J., and Immers, B. (2006). Multicommodity link transmission model for dynamic network loading. In *Proceedings of the 85th Annual Meeting of the Transportation Research Board*.
- Yuan, K., Knoop, V., and Hoogendoorn, S. (2015a). Capacity drop: A relation between the speed in congestion and the queue discharge rate. In *Proceedings of the 94th Annual Meeting of the Transportation Research Board*.
- Yuan, Y. (2013). *Lagrangian Multi-Class traffic State Estimation*. Ph.D. thesis, Delft University of Technology.
- Yuan, Y., Van Wageningen-Kessels, F., Van Lint, H., and Hoogendoorn, S. (2015b). *Proceedings of Traffic and Granular Flow 2011*, chapter Two modeling and discretization choices for Lagrangian multi-class first-order traffic flow model and their related (dis-)advantages. Springer.
- Zhang, H. M. (1999). A mathematical theory of traffic hysteresis. *Transportation Research Part B: Methodological*, 33(1):1 – 23.

Appendix A

Test questions

A.1 Problem set 1

A.1.1 Short questions

A road has a capacity of 2000 veh/h, a free flow speed of 120 km/h, a critical density of 25 veh/km and a jam density of 150 veh/km.

Exercise 1. *Draw a realistic fundamental diagram in the with the above properties, both in the flow-density plane and in the speed-density plane; indicate how speed can be found in the flow-density diagram. (4 points)*

Exercise 2. *Describe briefly (100 words) the assumptions in Daganzo's theory of slugs and rabbits (3 points)*

Exercise 3. *What are cumulative curves, and how are they constructed? (1 point)*

Exercise 4. *What is a vertical queuing model and how is this related to cumulative curves (2 points)*

Exercise 5. *What is higher, the space mean speed of the time mean speed? Why? (1 point)*

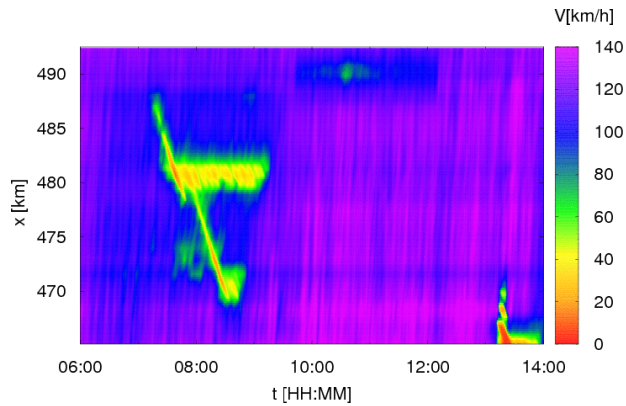
Exercise 6. *How can the space mean speed be calculated from individual local speed observations v_i . Give an equation. (1 point)*

A.1.2 State recognition

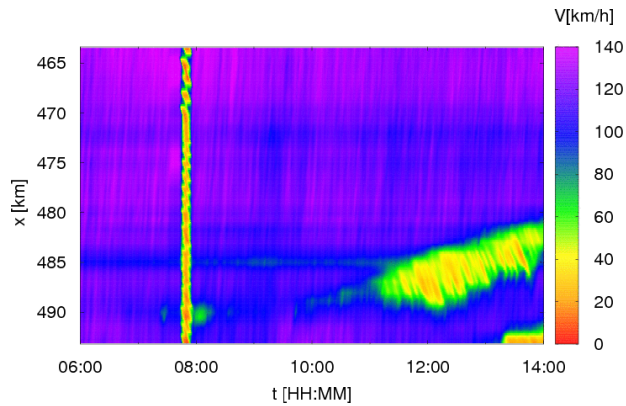
Exercise 7. *What are the phases according to three-phase traffic flow theory? How are they characterised? (2 points)*

Below, you find some traffic state figures from www.traffic-states.com. For each figure, indicate:

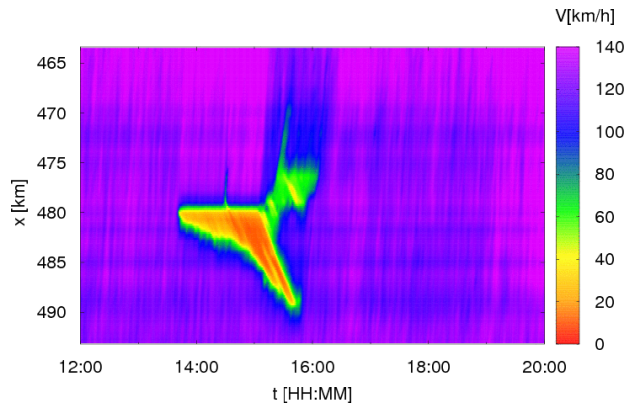
1. The driving direction (top-down or bottom-up) and explain why based on traffic flow theory (0.5pt per figure, spread over b-d) and
2. the traffic characteristics present, and the most likely causes for these (6 pt, spread over b-d)



Exercise 8.
(up to 10.00 am) (2 points)



Exercise 9.
(3 points)



Exercise 10.
(3.5 points)

A.1.3 Simulation model

Exercise 11. Explain briefly (indication: 100 words) Newells car-following model. Also plot a space-time diagram indicating these properties. (3 points)

Exercise 12. Name the three types of (in)stability in traffic flow, and explain briefly their effect (50 words and 1 graph per type) (3 points)

Exercise 13. Can multi-anticipation improve stability? Which type and how? (3 points)

Exercise 14. How can lane-changing cause a breakdown? (50 words) (1 point)

Exercise 15. *How can lane-changing prevent a breakdown? (Hint: use the lane distribution.) (2 points)*

A.1.4 Moving bottleneck

Imagine a truck drivers strike in France on a 3-lane motorway from time $t=t_0$. For the road you may assume a triangular fundamental diagram with a capacity of 2000 veh/h/lane, a critical density of 25 veh/km/lane and a jam density of 125 veh/h/lane. Suppose there is no traffic jam at $t < t_0$, and a constant demand of 5000 veh/h. Assume the truck drivers drive at 30 km/h, not allowing any vehicle to pass.

Exercise 16. *Calculate is the maximum flow on the road behind the trucks? (3 points)*

Exercise 17. *Sketch the traffic flow operations in a space-time diagram. Pay attention to the direction of the shock-wave, and note the propagation speeds of the other waves. (3 points)*

After a while, the trucks leave the road.

Exercise 18. *Sketch again the traffic operations in the space time diagram. Do this until the traffic jam is solved (if applicable), or until the traffic states propagate linearly if demand does not change. (3 points)*

Exercise 19. *Calculate the speed at which the tail of the queue propagate backwards? (1 point)*

Exercise 20. *In the plot of question 2, draw the trajectory of the vehicle arriving at the tail of the queue at the moment the strike ends (Use a different colour or style than the shockwaves). (1 point)*

Exercise 21. *What is the speed of the vehicle in the jam? (1 point)*

A.1.5 Marathon Delft

Imagine a marathon organised in Delft. There are 30.000 participants, starting at a roadway section which is 25 meters wide.

Exercise 22. *Give a realistic estimate for the capacity of the roadway in runners per hour. Base your answer on the width and headway of a runner*

Exercise 23. *Calculate how long it would take for all runners to start? (1 point)*

Suppose the runners have uniform distribution of running times from 2.5 to 4.5 hours, and all run at a constant speed.

Exercise 24. *Given your earlier assumptions, calculate the minimum required width of the road halfway the track to avoid congestion? For reasons of simplicity, you may assume that they all start at the same moment (instead of your answer at question 5b). (5 points)*

A.2 Problem set 2

A.2.1 Short open questions

Exercise 25. *Explain why Kerner claims that in his three phase theory there is no fundamental diagram (indication: 25 words) (1 point)*

Exercise 26. *What is a Macroscopic Fundamental Diagram (indication: 25 words)? (1 point)*

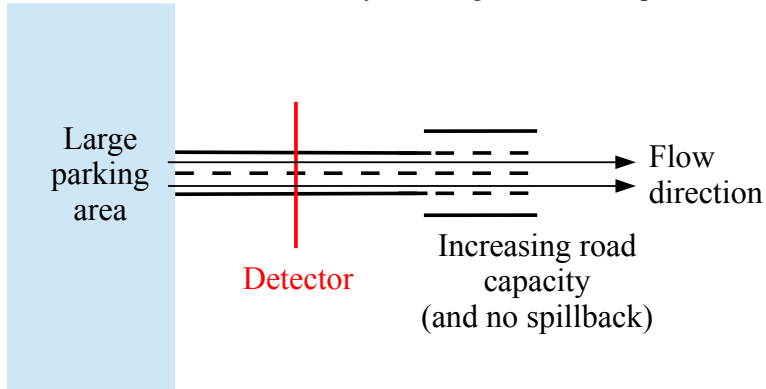
Exercise 27. *What are similarities and differences of a Macroscopic Fundamental Diagram compared to a normal fundamental diagram? Explain based on the underlying phenomena (indication: 75 words). (2 points)*

Exercise 28. *Explain in words the how the flow in from one cell to the next is calculated according to the Cell Transmission Model (indication: 100 words; equations can be useful, but need to be explained). (2 points)*

Exercise 29. *What do we mean with Lagrangian coordinates in macroscopic traffic flow simulation? Which variables are used? Why is this an advantage over other systems? (indication: total 100 words) (3 points)*

A.2.2 Leaving the parking lot

Consider the situation where many cars are gathered at one place, and they can only leave over one road.



The above figure shows a simplified representation of the road layout. There is a detector at the red line, in the two-lane road stretch. Downstream of the detector the road widens and there are no further downstream bottlenecks.

Exercise 30. Explain what the capacity drop is (be precise in your wording!). (1 point)

Exercise 31. How large is the capacity drop? Give a typical interval bound. (1 point)

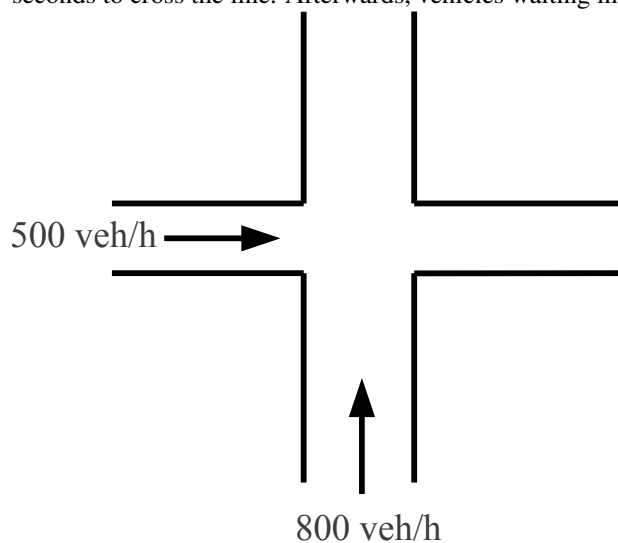
Exercise 32. Sketch the traffic flow at the detector (indicated in the figure) as function of the demand (in veh/h, ranging from 0 to three times the road capacity) from the parking lot. (2 points)

Exercise 33. Explain the general shape you draw in the previous question. (1 point)

Exercise 34. Give some rough estimates for values in your graph. (1 point)

A.2.3 Traffic lights

Consider a junction with a traffic light with equal green time g , and a clearance time of 2 seconds (i.e., the time needed to clear the junction; during this time, both directions are red). If the traffic light turns green, the first vehicle needs 3 seconds to cross the line. Afterwards, vehicles waiting in the queue will follow this vehicle with a 2 second headway.



Exercise 35. What is the fraction of time traffic is flowing over the stop line per direction as function of the cycle time c ? (2 points)

Exercise 36. *What is the maximum flow per direction as function of the cycle time? In your equation, what are the units for the variables? (3 points)*

Suppose traffic flow from direction 1 is 500 veh/h and traffic from direction 2 is 800 veh/h, and suppose a uniform arrival pattern.

Exercise 37. *What is the minimum cycle time to ensure that no queue remains at the end of the cycle? Does an approach with vertical queuing models yield the same result as shockwave theory? Why? (3 points)*

This cycle time is fixed now at 120 seconds. We relax the assumption of uniform distribution to a more realistic exponential arrival pattern.

Exercise 38. *To which distribution function for the number of arrivals per cycle (N) does this lead? Name this distribution (1 pt). (1 point)*

The probability distribution function of X is given by:

$$f(k; \lambda) = \Pr(X = k) = \frac{\lambda^k e^{-\lambda}}{k!}, \quad (\text{A.1})$$

with $e \sim 2.71828\dots$) and $k!$ is the factorial of k . The positive real number λ is equal to the expected value of X , which also equals the variance.

Assume there is no traffic waiting when the traffic light turns red at the beginning of the cycle.

Exercise 39. Express the probability p that there are vehicles remaining in the queue for direction 2 when the traffic light turns red at the end of the cycle in an equation ($p = \dots$). Write your answer as mathematical expression in which you specify the variables. Avoid infinite series. There is no need to calculate the final answer as a number (3 points)

Exercise 40. Argue whether this probability is higher or lower than if a uniform arrival process is assumed (1 point)

A.2.4 Car-following model

Consider the IDM car-following model, prescribing the following acceleration:

$$\frac{dv}{dt} = a_0 \left(1 - \left(\frac{v}{v_0} \right)^4 - \left(\frac{s^*(v, \Delta v)}{s} \right)^2 \right) \quad (\text{A.2})$$

with the desired distance s^* as function of speed v and speed difference Δv :

$$s^*(v, \Delta v) = s_0 + vT + \frac{v \Delta v}{2\sqrt{ab}} \quad (\text{A.3})$$

Exercise 41. Explain in words the working of this car-following; i.e. comment on the acceleration. (3 points)

Another car-following model is the relatively simple car-following of Newell.

Exercise 42. How does the Newell car-following model work? (indication: 50 words) (1 point)

Exercise 43. Name two weak points of both car-following models (IDM and Newell) (2 points)

Exercise 44. Give two reasons to choose the IDM model over Newell's model (2 points)

Exercise 45. Give two reasons to choose Newell's model over the IDM model (2 points)

A.2.5 Pedestrians in a narrow tunnel

We consider a pedestrian flow through a narrow tunnel, which forms the bottleneck in the network under high demand. The tunnel is 4 meters wide and 20 meters long. You may assume that the pedestrians are distributed evenly across the width of the tunnel. The pedestrian flow characteristics are described by a triangular fundamental diagram, with free speed $v_0 = 1.5 \text{ m/s}$, critical density $k_c = 1 \text{ P/m}^2$ and jam density $k_j = 6 \text{ P/m}^2$ (P stands for pedestrian).

Exercise 46. Draw the fundamental diagram for the tunnel. What is the capacity of the tunnel expressed in P/min ? (2 points)

Between 11-12 am, the average flow through the tunnel is $q = 180 \text{ P/min}$.

Exercise 47. Assuming stationary conditions, what is the density in the tunnel expressed in P/m^2 ? (2 points)

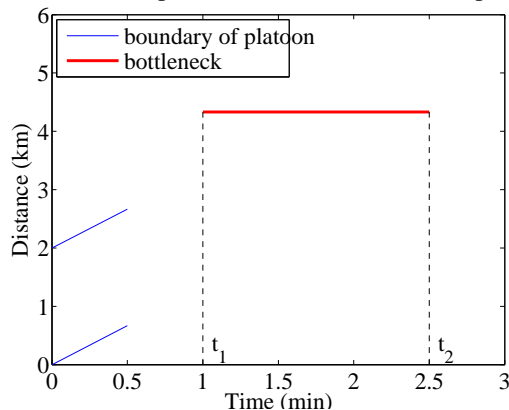
A.2.6 Moving bottleneck with different speeds

Consider a two-lane road with traffic in opposing directions. Assume a triangular fundamental diagram with a free speed of 80 km/h , a critical density of 20 veh/km and a jam density of 120 veh/h . At $t=0$ there is a platoon of 30 vehicles on the road with equal spacing in the section $x=0$ to $x=2 \text{ km}$. There are no other vehicles on the road. In this question, we will consider the effect of a speed reduction to 15 km/h .

Exercise 48. Calculate the density on the road in the platoon. Indicate the conditions in the fundamental diagram. Make a clear, large drawing of the fundamental diagram such that you can reuse it for indicating states in the remaining of the question. (1 point)

In each of the following subquestions, consider these initial conditions and no other bottlenecks than introduced in that subquestion – i.e., there never is more than one bottleneck.

Suppose there is a local, stationary bottleneck where drivers have to pass at 15 km/h from time t_1 to t_2 . The figure below shows the position and the duration compared to the platoon in the space time plot.



Exercise 49. Sketch the resulting traffic operations in a space-time plot. Also sketch some trajectories in the plot, using a different color or style. Indicate how you construct the diagram (i.e., indicate how you get the lines, angles, and distances in the plot). There is no need to calculate the exact traffic states. Additional information: the combination of speeds and the fundamental diagram will lead to congestion. (4 points)

Suppose there is a temporal speed reduction to 15 km/h for a short period of time over the whole length of the road at the same time. You may assume the platoon to be completely on the road.

Exercise 50. Sketch the resulting traffic operations in a space-time plot. Also sketch some trajectories in the plot, using a different color or style. Indicate how you construct the diagram (i.e., indicate how you get the lines, angles, and distances in the plot). (2 points)

Suppose there is a large tractor moving in the opposite direction of the traffic at 5 km/h from x_1 to x_2 . This wide vehicle causes vehicles that are next to it to reduce speed to 15 km/h. The speed (5 km/h) is lower than the speed of the shock wave at the tail of the queue in question b

Exercise 51. Sketch the resulting traffic operations in a space-time plot. Also sketch some trajectories in the plot, using a different color or style. Indicate how you construct the diagram (i.e., indicate how you get the lines, angles, and distances in the plot). (4 points)

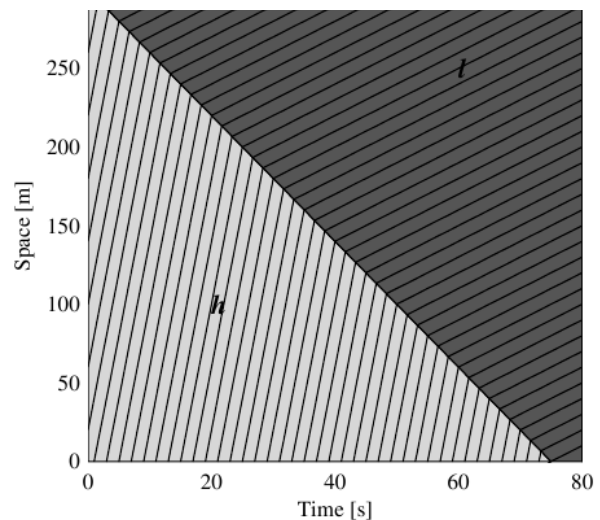
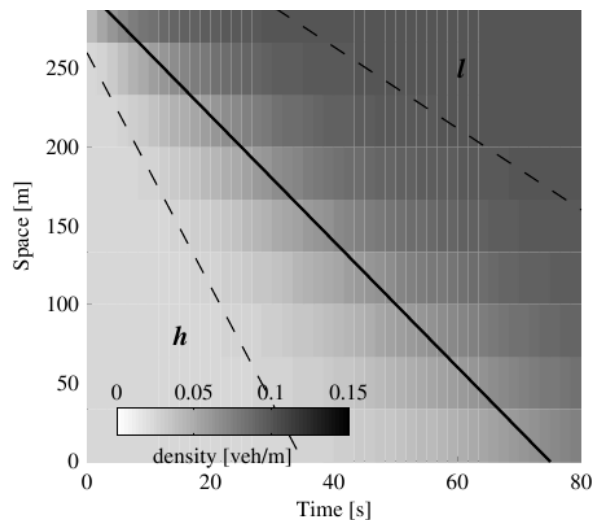
Suppose there is a large tractor moving in the opposite direction of the traffic at 50 km/h. This wide vehicle causes vehicles that are next to it to reduce speed to 15 km/h. The tractor speed (50 km/h) is higher than the speed of the shock wave of the tail of the queue in question b.

Exercise 52. Sketch the resulting traffic operations in a space-time plot. Also sketch some trajectories in the plot, using a different color or style. Indicate how you construct the diagram (i.e., indicate how you get the lines, angles, and distances in the plot). (Hint: it can help to consider a finite tractor length, but it is not necessary) (5 points)

A.3 Problem set 3

A.3.1 Short open questions

Below, two simulation results of a homogeneous congested area spilling back upstream are plotted. You see a high density, congested area, indicated with h downstream of $x=0$ at $t=0$, and a low density, uncongested area, indicated by l . The driving direction is up. One of the figures plots the results of a simulation in Eulerian coordinates and one of a simulation in Lagrangian coordinates.



Exercise 53. Explain which of the two is Eulerian and which one Lagrangian. (1 point)

Exercise 54. Give the two main advantages of using Lagrangian coordinates. (2 points)

Exercise 55. Explain what a pce value is. (30 words) (1 point)

Exercise 56. How does the pce value of trucks depend on the speed, qualitatively (i.e., does it increase, decrease, ...). Give your reasoning

Exercise 57. How does the pce value of trucks depend on the speed, qualitatively (i.e., does it increase, decrease, ...). Give your reasoning (2 points)

A.3.2 Multi-leader car-following models

Consider the IDM car-following model, prescribing the following acceleration:

$$\frac{dv}{dt} = a_0 \left(1 - \left(\frac{v}{v_0} \right)^4 - \left(\frac{s^*(v, \Delta v)}{s} \right)^2 \right) \quad (\text{A.4})$$

In this equation, v is the speed of the following vehicle, v_0 a reference speed, s the distance headway and s^* a reference distance headway as function of speed v and the difference in speed with the leader, Δv :

$$s^*(v, \Delta v) = s_0 + vT + \frac{v \Delta v}{2\sqrt{ab}} \quad (\text{A.5})$$

In this equation s_0 is a desired distance at standstill, and a is a reference acceleration and b is the maximum comfortable braking.

Exercise 58. Explain in words the working of this car-following model; i.e. comment on the acceleration. Only comment on equation A.4. (indication: 50 words) (2 points)

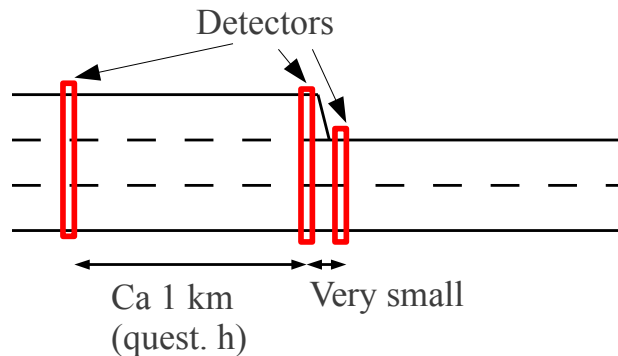
Exercise 59. Explain in words what is meant with multiple-leader car-following models. Only comment on the multi-leader part. (indication: 50 words) (1 point)

Exercise 60. Reformulate the IDM model into a multiple-leader car-following model by including two leaders. Give your reasoning, and, for all points, formulate those reasonings into equations. (3 points)

Exercise 61. Formulate the generalised car-following IDM model considering n leaders (3 points)

A.3.3 Measuring the speed at a cross section

Consider the following road layout with a lane drop from 3 to 2 lanes; traffic is flowing left to right.



The demand, as well as the flow at the downstream detector, is given in the figure below. The speed at the detector, located just upstream (you may assume no spacing between the bottleneck and the detector) of the bottleneck, is as follows.

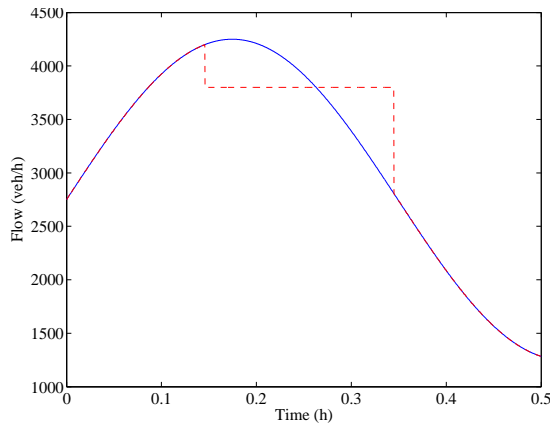
In the question, you might need values from the graph. Slightly misreading the graph is not a problem, but *mention the values you directly read from the graph and where you find these*.

Exercise 62. In figure a with the flow and the demand, which line is the demand and which line the flow. Argue why (1 point)

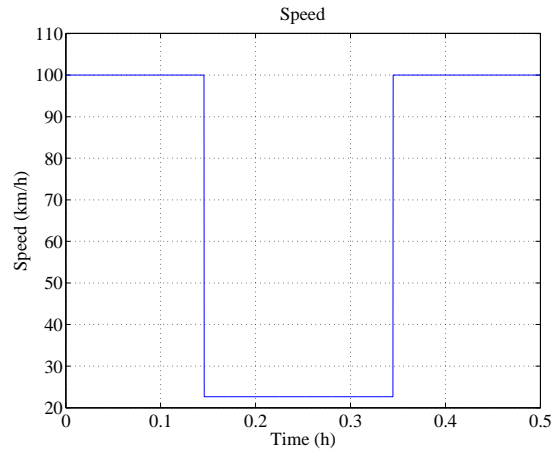
Exercise 63. Give the free flow capacity (and the reasoning how you find it) (2 points)

Exercise 64. Give the queue discharge rate. (and the reasoning how you find it) (2 points)

Assume the fundamental diagram per lane is the same for all lanes, at all locations in this setting.



(a) Flow and demand



(b) Speed

Exercise 65. Explain why can this situation not be described with a triangular fundamental diagram. (1 point)

Exercise 66. Draw the simplest fundamental diagram possible for the three lane section (aggregated over all lanes). Explain how you find the values for the relevant points, and give calculate them. (5 points)

Exercise 67. On you answer sheet, sketch the demand as function of time (i.e., copy the above figure, indicate the times of speed change in the graph - no points given) and in the same graph, sketch the resulting flow at the detector. Pay attention to the times at which the flow changes compared to the time of the speed changes. (2 points)

Now the delay is analysed by slanted cumulative curves.

Exercise 68. Explain the offset you choose. (1 point)

Exercise 69. Sketch the slanted cumulative curve of the flow and the demand for the situation at hand. (2 points)

Exercise 70. Indicate in the figure how you can determine the delay. (1 point)

Now a second detector is constructed approximately 1 km upstream of the bottleneck.

Exercise 71. Sketch the demand as function of time (i.e., copy the second figure of this question, indicate the times of speed change in the graph - no points given) and in the same graph, sketch the resulting flow at this second detector. Pay attention to the times at which the flow changes compared to the time of the speed changes. (2 points)

We now relax the assumption of all traffic states at the fundamental diagram to a more realistic situation (i.e., including demand and supply variations). In this situation, We measure the one-minute aggregated (harmonically averaged) speeds during one month.

Exercise 72. Sketch a probability distribution or histogram of these speeds. Explain the shape (2 points)

A.3.4 Moving bottleneck

Consider a two-lane motorway. Assume a triangular fundamental diagram with a free flow speed of 80 km/h, a critical density of 25 veh/h/lane and a jam density of 150 veh/km/lane. The inflow is stationary at 2000 veh/h.

Exercise 73. Draw the fundamental diagram and calculate the capacity of the road stretch²

Consider a wide vehicle (special transport) driving slowly is entering the road. There are no overtaking possibilities. This creates congestion, of which the tail happens to stay at the same position.

Exercise 74. Calculate the flow in the jam. (Hint: you can use the speed of the shockwave at the tail of the queue)¹

Exercise 75. Calculate the density in the jam.²

Exercise 76. Calculate the speed of the special transport.²

After 5 km, the truck leaves the road.

Exercise 77. Construct the space-time diagram of this situation, from before the moment the truck enters the road to after the moment the traffic situation is stationary. Explain how you find the speed of the solving of congestion; you may re-use the figure you created in a.4

Exercise 78. At the maximum queue length, how many vehicles are in congestion¹

A.3.5 Multi-lane traffic flow

Exercise 79. Give the names of two regimes according to Daganzo's theory of slugs and rabbits (only names are required). (1 point)

Below, you find a Google Earth image of the A1 motorway near Bathmen. Consider the right to left (east to west) direction



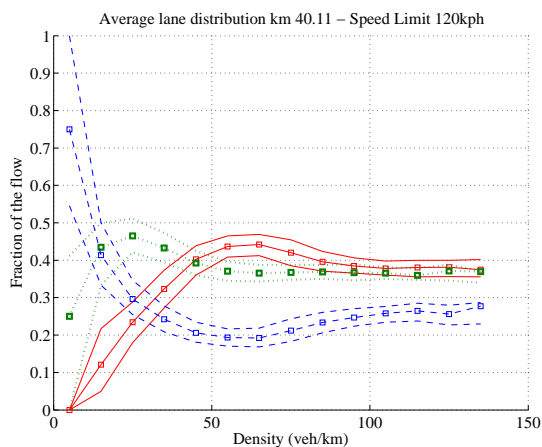
Exercise 80. To which of the regimes of question a) does the situation in the figure resemble most. Explain why (2 points)

There are 4 trucks and 7 passenger cars (including one delivery van) in the image. The fraction of passenger cars in the density is hence $7/11$.

Exercise 81. What would you expect from the fraction of passenger cars in the flow: is this higher, lower or equal to $7/11$. Motivate your answer 2 points

Exercise 82. Calculate the fraction of the is passenger cars in the flow. Assume reasonable speeds for the different vehicle types in your answer – state your assumptions clearly. (4 points)

Below, a figure of a lane flow distribution for a three lane road in the Netherlands is given.



Exercise 83. In the figure, which color matches which lane. Argue why (1 point)

Exercise 84. Describe briefly (100 words) the assumptions in Daganzo's theory of slugs and rabbits (3 points)

Exercise 85. Using Daganzo's theory of slugs and rabbits, explain the differences in flow between most used lane (blue) and the least used lane (red) at a density of 75 veh/km. (2 points)

A.4 Problem set 4

A.4.1 Short questions

Exercise 86. What does a Macroscopic Fundamental Diagram describe? Make sure your answer shows clearly the differences between an MFD and a fundamental diagram. (2 points)

Exercise 87. What is qualitatively the effect of inhomogeneity in the network on the MFD? (No explanation needed) (1 points)

Exercise 88. In Lagrangian coordinates, the fundamental diagram is often expressed in spacing (horizontal) - speed (vertical) form. Sketch a fundamental diagram in the spacing-speed plane (2 points)

A.4.2 From car-following to a fundamental diagram

The optimal velocity model is a car-following model specifying the acceleration a as follows:

$$a = a_0(v^* - v) \quad (\text{A.6})$$

In this equation, v is the speed of the vehicle, and a_0 a reference acceleration (tunable parameter, constant for a specific vehicle-driver combination). v^* is determined as follows:

$$v^* = 16.8(\tanh(0.086(\Delta x - 25) + 0.913)) \quad (\text{A.7})$$

In this equation, Δx is the distance (in meters) between the vehicle and its leader.

Exercise 89. Explain qualitatively the working of this car-following model; i.e. comment on these two equations. (2 points)

Exercise 90. What are the conditions for which a fundamental diagram holds? (1 point)

Exercise 91. Derive the expression a fundamental diagram (flow as function of density) for these conditions using the OVM model⁴

Exercise 92. What are the values capacity, free speed and jam density (either derive the value or use you graphical calculator to determine this – you may round numbers to the precision of your liking...) (1 point)

Exercise 93. Argue whether the values in the previous question are reasonable for the spacing/speed relationship? If so, for what conditions (urban, freeway...?) If not, can you change the parameters (numbers) of the model (A.6 and A.7) to get a proper fundamental diagram (if so: what are reasonable numbers). Show in your answer that you understand the traffic operations, and/or the model working.

A.4.3 MOBIL lane change model

Consider the mobil lane change model. A driver c has several options: change lanes to the left, to the right or stay in his current lane. For each of the options a total utility (denoted U_{tot}) can be calculated.

$$U_{\text{tot}} = U_c + p \sum_{i \in \text{other drivers}} U_i \quad (\text{A.8})$$

The utility for the driver i U_i is assumed to be its instantaneous acceleration, as computed using a car-following model (the Intelligent Driver Model – although the specific model is not relevant for the question). The driver is assumed to take the option with the highest utility.

Exercise 94. Explain the working of the model in words (2 points)

Exercise 95. What value for p can be expected (1 point)

A situation like this can be observed in practice



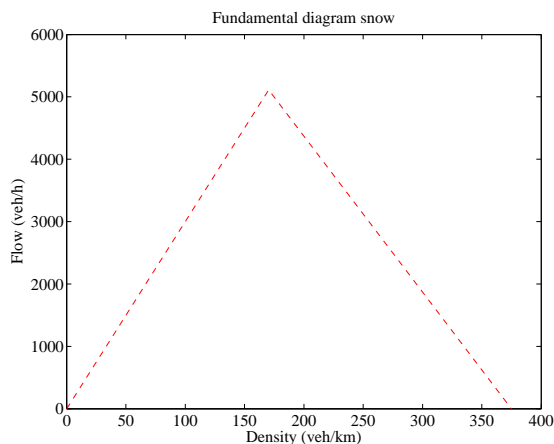
Exercise 96. Does the MOBIL lane change model explain this? Reasoning from the model, explain how (if it does explain) or why (if it does not explain). (2 points)

A.4.4 Snow plow

During a winter night, a 30 cm snow covered a three lane motorway fell. Traffic is still moving.



This changes the traffic operations. Assume a triangular fundamental diagram. The free flow speed reduces to 30 km/h, the jam density to 125 veh/km/lane. The capacity is 5000 veh/h.



A truck spins and cannot move further, thereby blocking the road completely, not allowing other vehicles to pass. This leads to a traffic jam. The inflow is 1000 veh/h.

Exercise 97. Draw the resulting traffic operations in a space time plot and in the fundamental diagram. Calculate all shock wave speeds. (4 points)

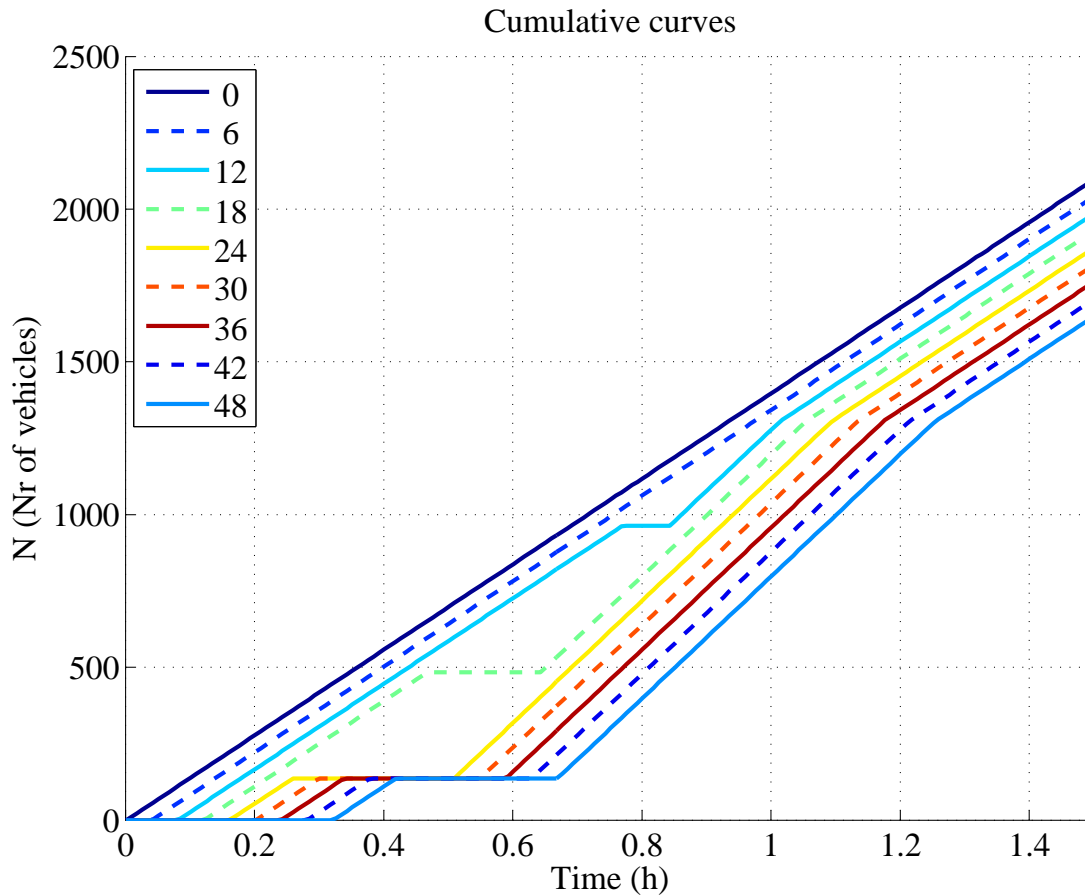
A snow plow comes to free the vehicles that are stuck. After freeing the vehicles, the snow plows clear two of the three lanes of the motorway. Thereby, they drive at 5 km/h on the motorway. The capacity of vehicles passing the snow plough on the left lane is 2000 veh/h. The inflow on the road is 1000 veh/h.



Exercise 98. *Sketch the traffic operations in a space-time plot and in the fundamental diagram. Explain how you construct the graphs. (No point given here for the beginning, discussed in question b) (5 points)*

A.4.5 Cumulative curves

The graphs show cumulative curves for different locations along the road. The legends shows the distances in km from the beginning (i.e., upstream end) of a road. For the remainder of the question, reasoning is more important than exact readouts from the graph. When using graph readouts, please state so explicitly and *note the values you read from the graph*.



Exercise 99. Explain the traffic state, mention a possible cause (e.g., “different speed limits for different sections”, “peak hour jam”) and explain why³

Exercise 100. Estimate the total delay encountered here³

Exercise 101. Sketch the traffic situation in space-time (shock waves – no trajectories needed). Estimate the location of changes in traffic states.³

Assume a triangular fundamental diagram.

Exercise 102. Estimate, from the given curves, give the free speed, capacity, critical density and jam density⁴

A.4.6 Crown jewels in the tower

We consider an exhibition with the most important piece an object in a small glass show case in the middle of the room. Visitors do not have a preference to see a particular side of the piece. The room is 15 meters long and 6 meters wide.

Exercise 103. Explain why a larger glass show case can increase the capacity of the exhibition room, in terms of visitors per unit of time²

The exhibitor has chosen for a show case of 3x1 meters.

Exercise 104. Estimate the capacity of the room, measured in visitors per minute; base your answer on a reasonable watching time for the piece of art and state the assumptions explicitly⁴

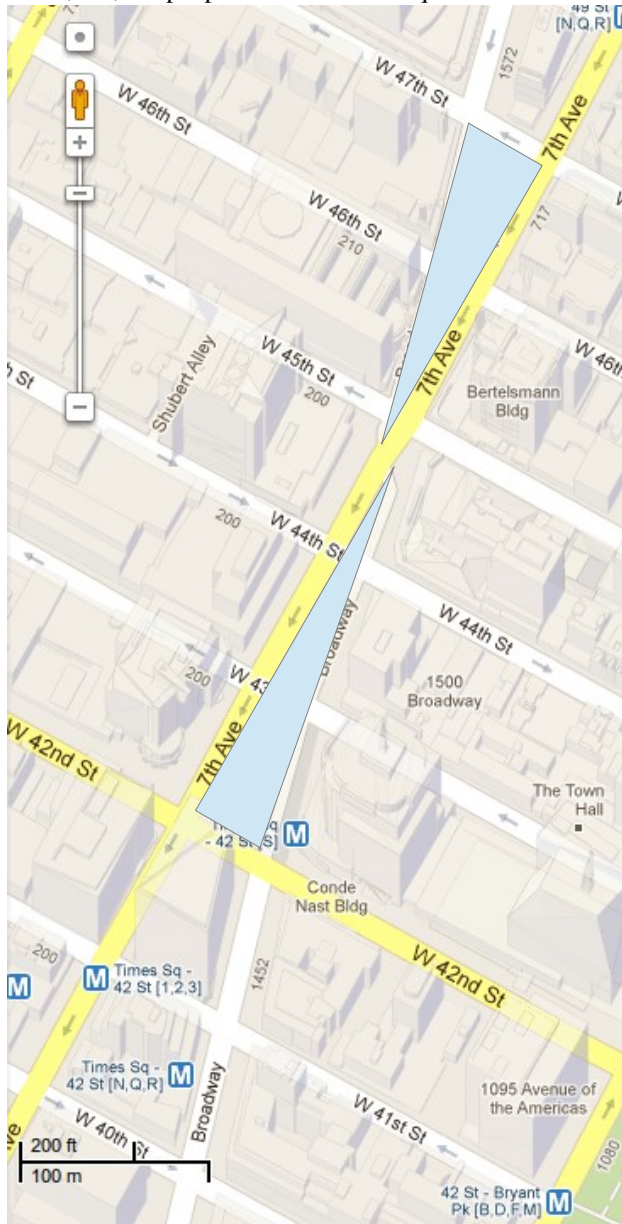
An alternative design is considered. Instead of the visitors walking by the art, the visitors can stand on a moving walkway (like in the airport), which is constructed at each side of the glass. Visitors step at the moving walkway at the beginning of the room, and step off at the end. They are not allowed to walk backwards on the moving walkway.

Exercise 105. *What is the capacity of the room in this case. Base your answer on (explicitly stated) reasonable assumptions on distance and speed.*³

A.5 Problem set 5

A.5.1 Short questions

Below, you find a google maps image of New York; Times Square is shaded in blue. The municipality of NY claimed that 1,000,000 people were at Times Square at the start of the new year (1 January 0h00).



Exercise 106. *From a traffic flow perspective, comment on this claim. (2 points)*

Exercise 107. *How can synchronized flow be recognized? (1 point)*

Exercise 108. *Sketch the three phases of traffic flow in a flow-density diagram, and give the names (2 points)*

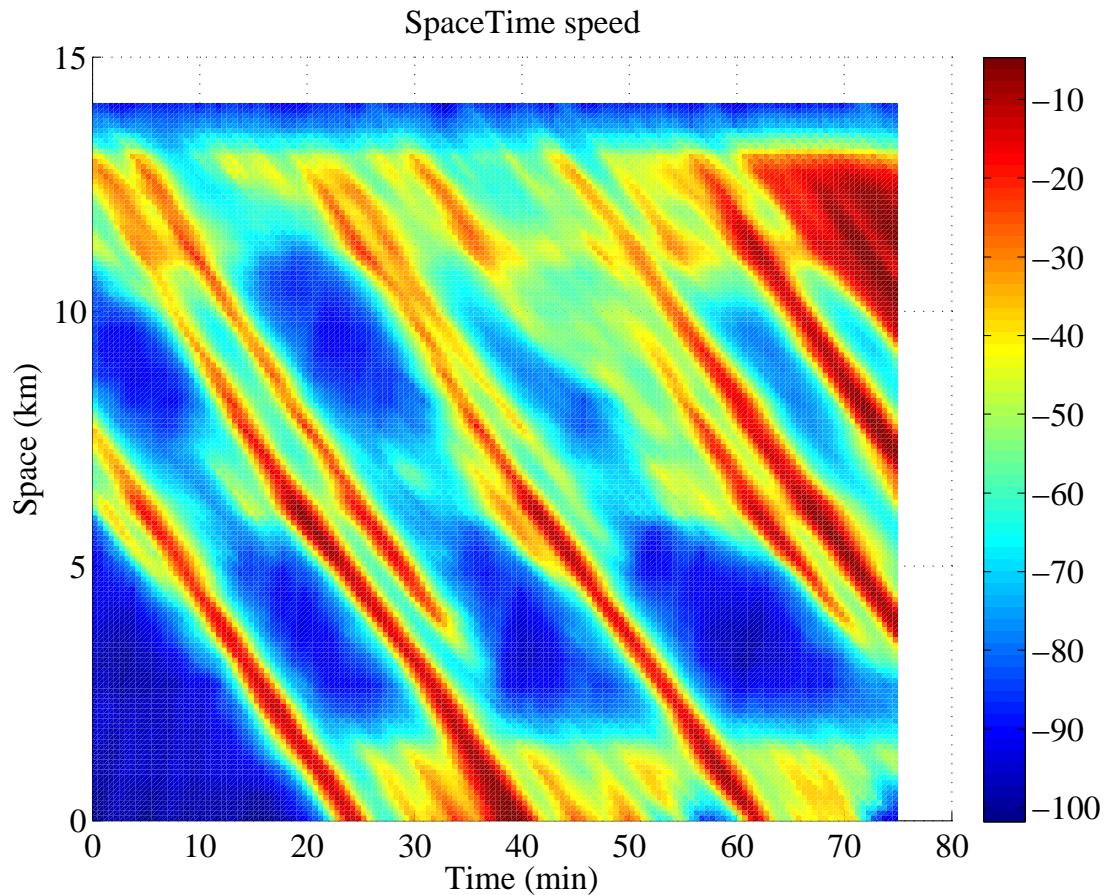
Exercise 109. *Comment on the concept of capacity in the three phase traffic flow theory (1 point)*

Exercise 110. *How are Lagrangian coordinates for traffic defined (i.e., what is special on the the definition of the coordinates; how do they differ from Eulerian coordinates?) (1 point)*

Exercise 111. *What the main mathematical advantage of the Lagrangian coordinate system? (1 point)*

A.5.2 Motorway traffic operations

Below, you find a speed contour plot of traffic operations at a motorway (the negative speeds are plotted for color representation: units are in km/h, so blue is 100 km/h and red is (almost) standstill). (if you are color blind and cannot see the colors – please ask!)



Exercise 112. Explain which direction traffic is flowing from the graphs¹

Exercise 113. Name the two main traffic phenomena you see - and briefly describe what is happening.²

Exercise 114. What are the three different levels of stability, and what do they mean?²

Exercise 115. Comment on the stability of traffic for this day³

Exercise 116. What traffic states can occur according to the theory of slugs and rabbits. Give the names and a short description (10-20 words per state)²

Exercise 117. Modelling a multi lane Dutch motorway, how does this theory in resulting traffic differ from the Mobil lane change model for moderately dense (undercritical) traffic?²

A.5.3 Car-following

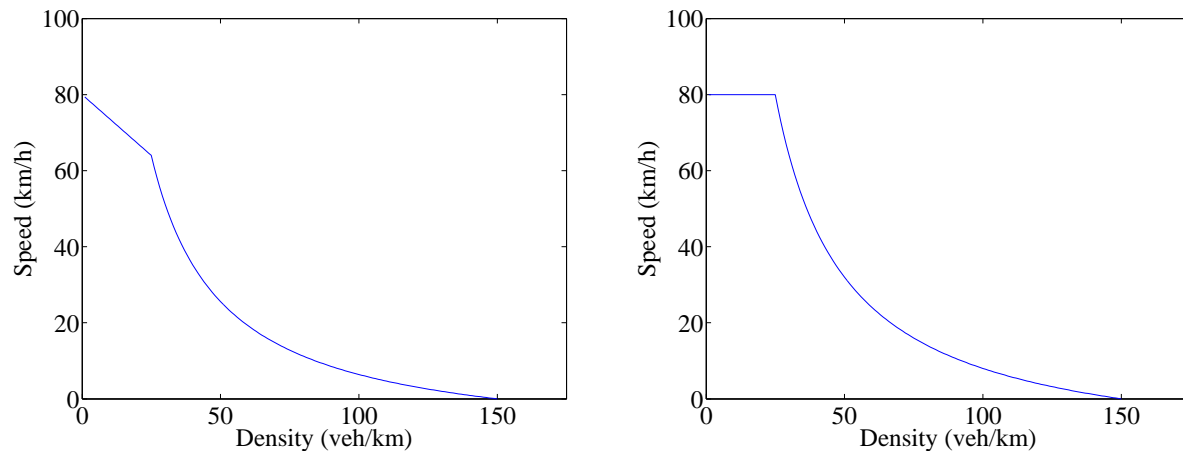
A fundamental diagram only holds in stationary and homogeneous traffic conditions.

Exercise 118. Explain the terms stationary and homogeneous (indication: 20 words each) (2 points)

From a car-following model the fundamental diagram can be derived.

Exercise 119. Can a car-following model be derived from the fundamental diagram? If so, explain how. If not, explain why not. (2 points)

The two speed-density relationships shown below relate to a triangular fundamental diagram and Smulders fundamental diagram



Exercise 120. Which figure is which fundamental diagram. Why? (1 point)

Exercise 121. Draw the corresponding flow-density and speed-flow curves for Smulders fundamental diagram (in your drawing, put attention to (or indicate) the values or slopes at several critical points at the ends of lines or at turning points)³

A.5.4 Partial road blocking near a signalised intersection

Upstream of a signalised intersection the road is partially blocked by a crane (see below figure for illustration). Assume that between the crane and the intersection, all four lanes can (and will) be used if needed. That means that the length between the crane and intersection is longer than in the images.



During the red phase, the tail of the queue spills back further than the crane. During the green phase, the queue dissipates completely. Throughout this question, assume a fundamental diagram which is concave (not triangular).

Exercise 122. Sketch the fundamental diagrams. Give typical values for the characterizing points. (2 points)

Use this diagram throughout this question.

Exercise 123. Sketch the traffic operations in a space time plot, starting at the moment the traffic light turns red and ending at the moment the traffic light turns red again. Also indicate all states in the fundamental diagram. Only consider traffic states upstream of the traffic light.⁸

Exercise 124. Draw the (moved) cumulative curves upstream of the traffic jam and downstream of the traffic light (2 points)

Exercise 125. How could you get the total delay from this for all vehicles together (explain, but no need for calculations) (1 point)

Exercise 126. Comment qualitatively on the effect of the distance between the intersection and the crane on the delay (2 points)

The workers move the crane downstream in order to reach a building further downstream. They can only do so when there is no queue downstream. Assume they start when the queue is dissolving and traffic flows past the crane, but the queue is not dissolved completely yet, and assume a speed for the movement. The fundamental diagram does not change due to the movement (i.e., you may use the FDs of question a)

Exercise 127. Sketch the traffic states in the flow-density plane, from the moment the crane moves until the queue is completely dissipated (you may assume the traffic light stays green, and assume the distance to the traffic light is large enough that the crane can keep moving until the traffic jam is solved). (4 points)

A.5.5 Network Fundamental Diagram

Exercise 128. What variables are related to each other in the Network Fundamental Diagram. Give the names and explain the terms (more than one answer possible) (2 points)

Exercise 129. Sketch a typical NFD (1 point)

Exercise 130. How is this shape different from a regular fundamental diagram. Explain briefly why (20 words). (1 point) –

Exercise 131. *Comment on the traffic mechanism behind the right hand side. Show in your answer that you understand the difference in traffic mechanism with the fundamental diagram (1 point)*

A traffic engineer suggests to limit the access to the central business district, a part of the road network with many companies.

Exercise 132. *Explain using the NFD why this can be beneficial even though the stopped vehicles need to wait and experience delay. (3 points)*

A.6 Problem set 6

Exercise 133. *Explain what a car-following model does in general (1 point)*

A.6.1 Short questions

The pce value of a truck is claimed to be 2 for a road without queue warning systems.

Exercise 134. *Explain what a pce value is (indication: 30 words). (1 point)*

A study shows that by installing queue tail warning systems the capacity of the road increases. The factor by which it increases is 1.05 for passenger cars and 1.09 for trucks, meaning it can handle 5% more cars and 9% more trucks

Exercise 135. *Based on the information above, calculate the new pce value for trucks for the road with queue warning systems. (3 points)*

Exercise 136. *Traffic simulation in Lagrangian coordinates has the advantage that there is less numerical diffusion. Explain in your own words what this means – indication 50 words. (1 point)*

The total utility U for the mobil lane change model is given by:

$$U_{\text{tot}} = U_{\text{own vehicle}} + p \sum_{i \in \text{other drivers}} U_i \quad (\text{A.9})$$

In this equation, the utility for each driver is determined by its instantaneous acceleration, given by a car following model. This utility can be calculated for the situation with lane change ($U^{(\text{lane change})}$), as well as without lane change, ($U^{(\text{no lane change})}$). For European driving, vehicle will change to the right if $U^{(\text{change to the right})} > (U^{(\text{no lane change})} - a_{th})$ and to the left if $U^{(\text{change to the left})} > (U^{(\text{no lane change})} + a_{th})$. In these equations, a_{th} is a threshold which should be exceeded to perform a lane change.

Exercise 137. *What is a reasonable value for a_{th} – explain why. (1 point)*

Exercise 138. *What would be a reasonable range for the parameter p – explain why. (1 point)*

Consider a fundamental diagram for pedestrian flow in the flow-density plane.

Exercise 139. *What are the units, as well as the minimum and maximum values at the axes? (2 points)*

A.6.2 Bridge opening

Consider a two lane motorway, with a capacity of 5000 veh/h and a queue discharge rate of 4500 veh/h. On this motorway, the free flow speed differs from the critical speed.

Exercise 140. Sketch a fundamental diagram for the motorway in the flow-speed (!) plane.²

Exercise 141. Indicate reasonable values for the (i) free flow speed, (ii) critical speed, (iii) critical density and (iv) jam density.³

Assume the fundamental diagram holds. The demand is constant at 3500 veh/h. The bridge opens at $t=1h$ and is opened for 15 minutes.

Exercise 142. Sketch the cumulative curves for the inflow and outflow.²

Exercise 143. Calculate the maximum number of vehicles in the queue.¹

Exercise 144. Calculate the total delay of all vehicles combined.³

In the remainder of the question, assume a Greenshields fundamental diagram with a capacity of 5000 veh/h, and a critical density of 60 veh/km.

A further detailed description of the traffic situation uses a so called *acceleration fan*.

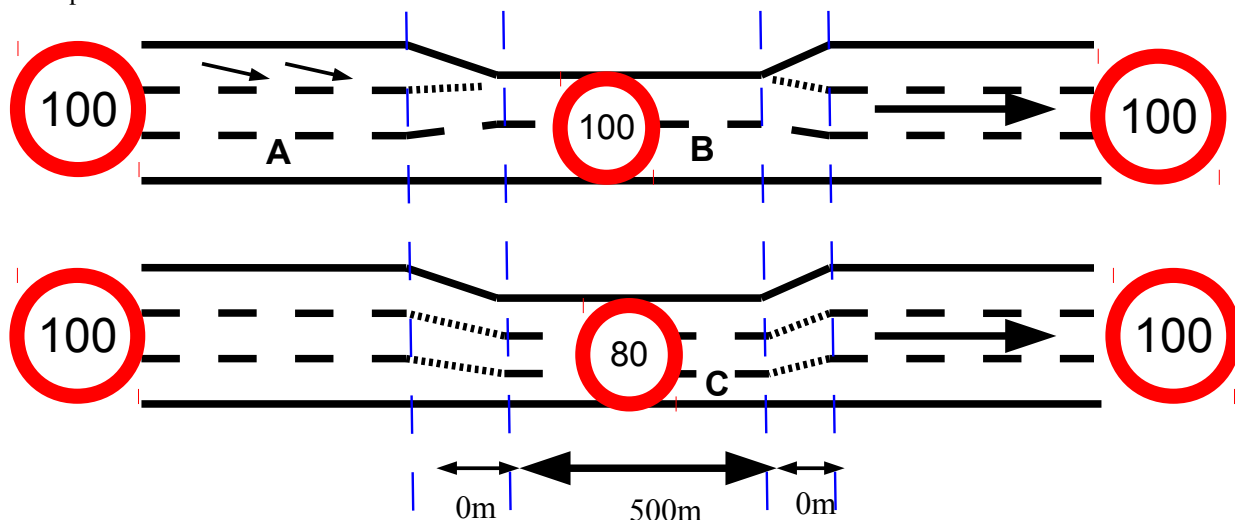
Exercise 145. Explain in your own words what is an acceleration fan.¹

Exercise 146. Under this assumption, sketch the flow 500 meters downstream of the bridge as function of time from the moment of the bridge closing (i.e., when the vehicles can flow again); also provide a reference value at the vertical axis.³

Exercise 147. Calculate when the flow starts to change in the graph above (hard question: 2 instead of 4 points).²

A.6.3 Variable road layout

Consider a 3 lane motorway with a 100 km/h speed limit. The road has a narrower part of a limited length (a bridge, 500 meters long), which can be used as two lane stretch with 100 km/h speed limit, or as three lane stretch with 80 km/h speed limit.



Throughout the question you may assume a triangular fundamental diagram for all road types. For the wide lanes, the critical density is 25 veh/km/lane and the jam density is 125 veh/km/lane. Assume the width of the lanes does not influence the congested branch.

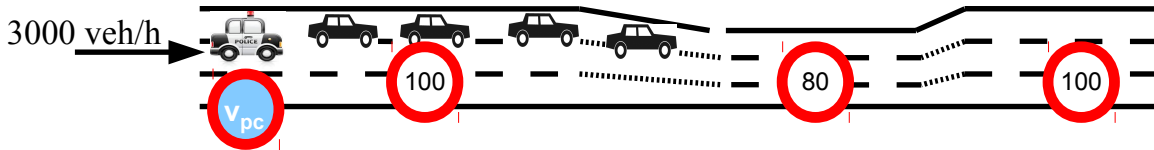
Exercise 148. *Sketch the fundamental diagrams (aggregated over all lanes) for the three parts (all in one figure): three wide lanes, two wide lanes and three narrow lanes: parts A, B and C in the figure above. (2 points)*

Exercise 149. *Calculate the capacity of the three lane narrow road section. (2 points)*

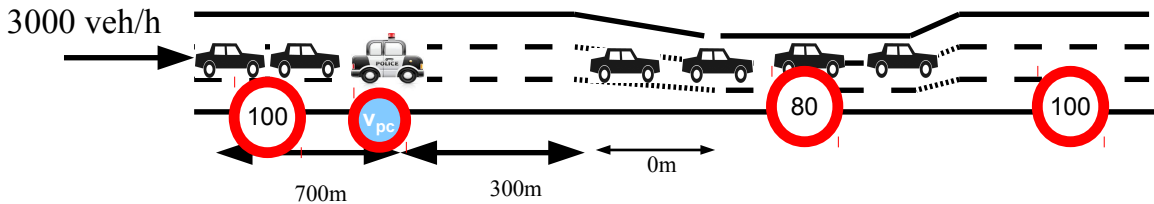
The road authority switches dynamically between the three narrow lanes and the two wide lanes.

Exercise 150. *Explain why this dynamic switching is beneficial for the delays (i.e., why does this give less delays than choosing one layout permanently) (indication: 50 words). (1 point)*

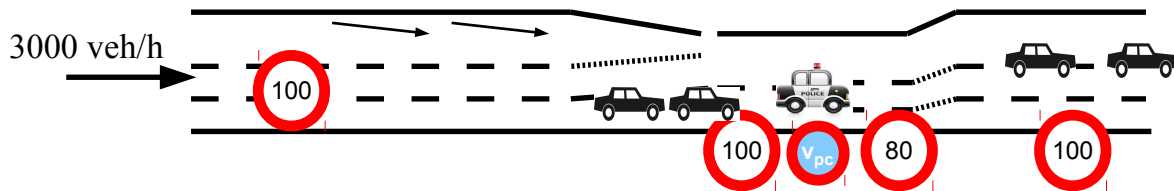
During switching, the road needs to have an empty stretch of 300 meters (because one cannot change the lanes at which vehicles are driving). The road authority wants to do so by insert a *pace car* into the traffic stream starting 1000m upstream of the switching part. This should drive at an appropriate speed (v_{pc}) to create this gap (the gap should be downstream of the pace car after this has travelled 700m). Consider the situation of switching from 3 lanes to 2 lanes. The demand is 3000 veh/h. For illustration purposes, the process is also shown in figures below.



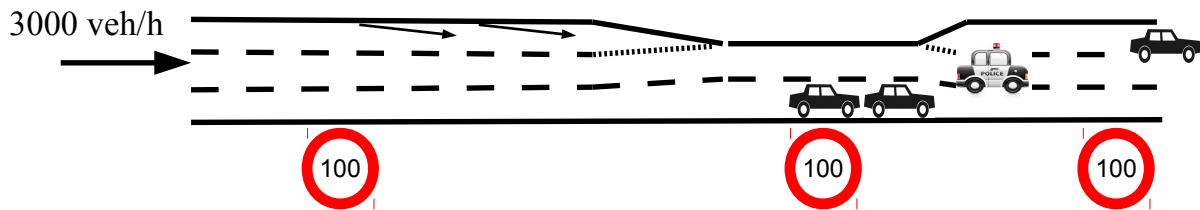
In normal conditions a pace car is introduced, driving at a speed v_{pc}



After 700 m driving, the pace car has a gap in front of 300 m. The last vehicle of the platoon downstream of the pace car is 300 downstream of the pace car, at the location of the change of layout



Upstream of the pace car, the road switches to a 2 lane road with a 100 km/h speed limit



If the pace car is out of the narrow section, it adapts its speed to the speed limit if not limited by traffic. Otherwise, it adapts its speed to the vehicles in front.

Exercise 151. Calculate the speed at which the pace car needs to drive. (1 point)

The pace car acts hence as moving bottleneck, and will continue driving at this speed throughout the bridge section, and then (instantaneously) speed up to the free speed.

Exercise 152. Indicate the traffic states in the flow density diagram and sketch traffic states in the space-time diagram (and relate them to each other using shock wave theory). (no vehicle trajectories needed) (hard question: 6 points awarded for 9.5 points). Tip for sketching: choose the demand low in your graph (for simplicity you may assume other flows to be higher). If you did not find an answer for the question above, assume it is driving 60 km/h. (6 points)

A.6.4 Traffic stability

Exercise 153. Give the name of the mild congestion located at a bottleneck location in Kerner's three phase traffic flow theory (1 point)

In the flow-density plan, this is an area rather than a line.

Exercise 154. Link this to the Wiedeman car-following principle. (indication: 100 words) (2 points)

A.6.5 Levels of description

One can argue that there are three levels at which traffic can be described: microscopic, macroscopic, and network-level. On the microscopic level, traffic behaviour can be indicated by a spacing-speed diagram.

Exercise 155. Sketch this diagram. (2 points)

Exercise 156. Sketch the matching diagram in the flow-density plane; indicate how the values for this graph can be obtained from the previous graph. (2 points)

Exercise 157. Give is the name for the flow aggregated on network level (1 point)

Exercise 158. Give the name for the density aggregated on network level (1 point)

Exercise 159. Sketch the matching Network Fundamental Diagram for the network level in the same graph as the fundamental diagram of question b, and briefly comment on the difference (50 words).2

A.7 Problem set 7

A.7.1 Short open questions

Upstream of an junction is a controlled intersection.

Exercise 160. Which distribution is likely to describe the number of arrivals per time interval (i.e., flow) on the main road near this junction (and downstream of the controlled intersection)? Name and explain briefly why (no need to comment on the equations of the distribution functions). (2 points)

Exercise 161. Argue why traffic instability can only occur under platoon instability. (2 points)

Traffic dynamics can be described by linking three variables, usually indicated by x , N , and t .

Exercise 162. Describe the physical meaning of $N(x,t)$. (1 point)

Exercise 163. Describe the difference between calibration and validation of a traffic model. (Indication: 40 words) (2 points)

Exercise 164. Which relationship is described by the macroscopic fundamental diagram. In your answer, make sure to be specific enough that the answer does not apply for the fundamental diagram. (There is no need to comment on the shape, traffic process leading to the shape or to name specific terms – indication: 25 words) (1 point)

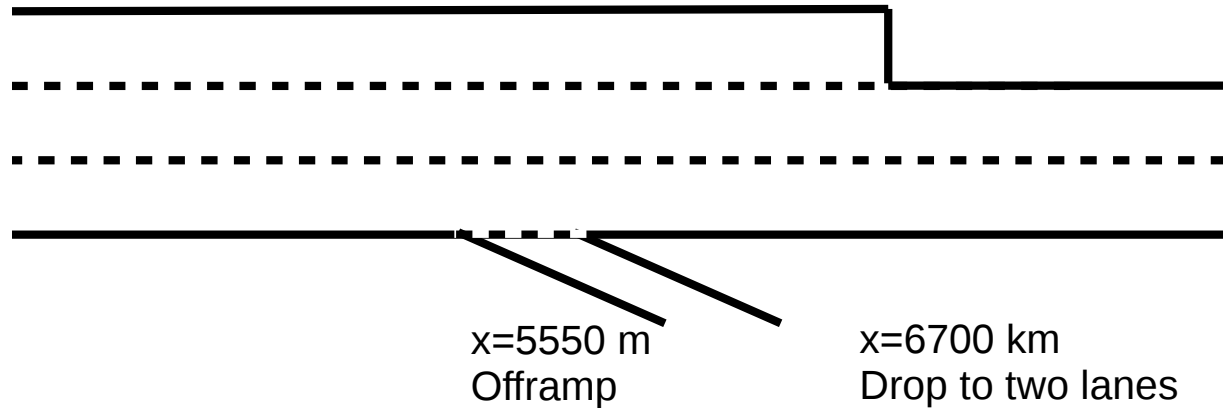
For pedestrian traffic, a typical value for the capacity which can be found in a handbook is 1.22.

Exercise 165. What are the units for this capacity. (1 point)

Exercise 166. What is the physical meaning of these units? (1 point)

A.7.2 Cumulative curves

Consider the following road layout:

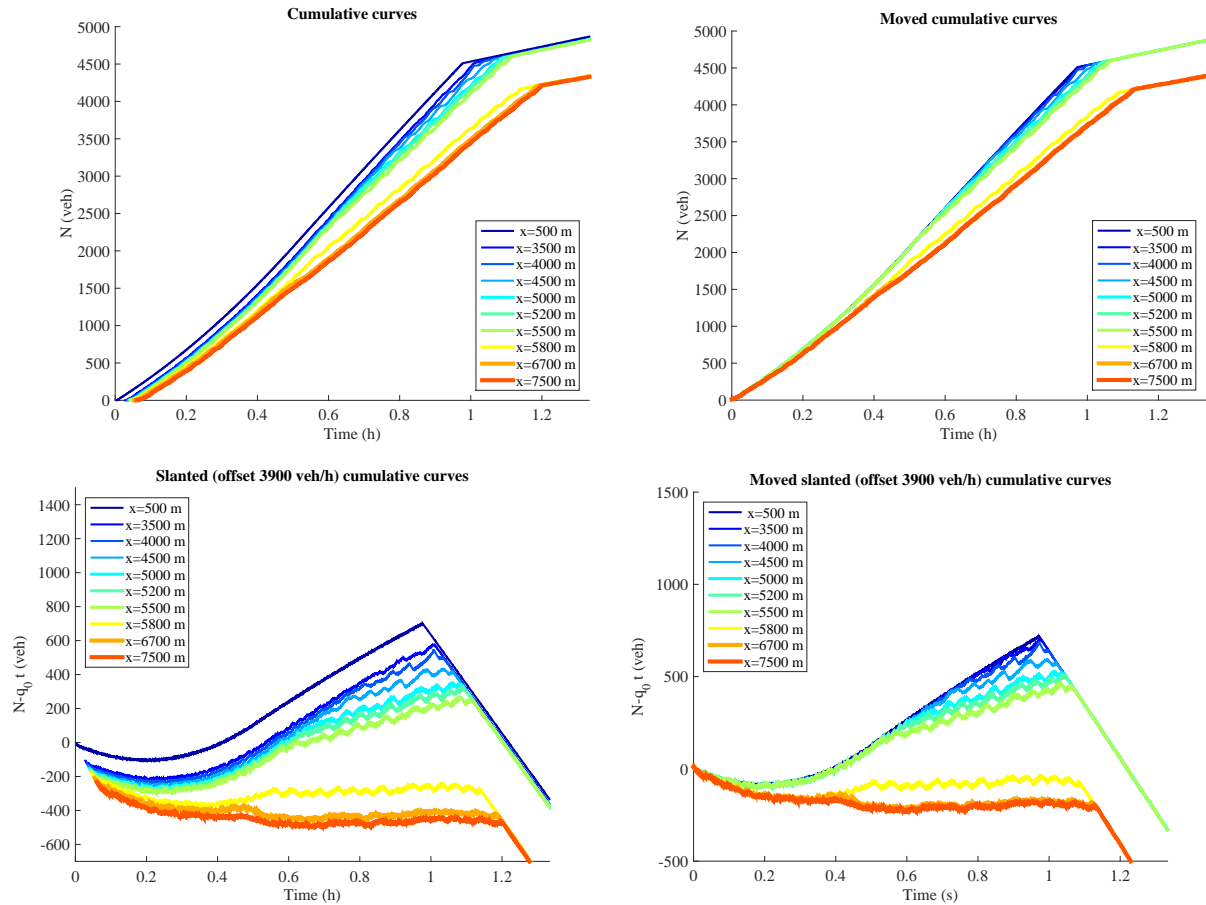


A three lane road has an offramp just downstream of 5500m, and a lane drop at approximately 6700m.

Cumulative counts are obtained from Fosim.

Exercise 167. *Name the two main limitations of using cumulative curves for delay determination in real world conditions. (2 points)*

On the next page, you find the cumulative curves, the moved cumulative curves (i.e., corrected for the free flow travel time), the slanted cumulative curves (offset 3900 veh/h), and the slanted moved cumulative curve (i.e., corrected for the free flow travel time). (If you cannot differentiate colors, raise your hand to get explanation on the lines!)



Exercise 168. Describe the traffic operations (or sketch the traffic operations in space-time): This should show: is there an temporal bottleneck? Why does congestion end (demand or supply)? Where is the head and tail of the queue approximately. Also indicate what information you use to get to this conclusions. (3 points)

Exercise 169. Estimate the (free flow) capacity of the bottleneck in veh/h from the curves. (2 points)

Exercise 170. Estimate the capacity drop in veh/h from the curves. (2 points)

The total delay due to the queuing is determined by summing the delays for all vehicles.

Exercise 171. Argue whether the delay would differ if a vertical queuing model for the bottleneck was used, and if so, would the delay be less or more with a vertical queuing model. (2 points)

A.7.3 Macroscopic traffic variables in case of different vehicle classes

Suppose there are two classes of vehicles, fast vehicles driving 120 km/h and slow vehicles moving at 90 km/h. At the entrance to the road ($x=0$), an equal number of each type of vehicles is measured under a total flow of 1000 veh/h (so 500 veh/h each). *For some subquestions you might need answers of earlier subquestions, which you could not answer. In that case, assume an answer, state so on your answer sheet and continue with the assumed answers.*

Exercise 172. Calculate the density on the road. Base your answer on the density of the slow vehicles and the fast vehicles. (3 points)

Exercise 173. Calculate the space mean speed. (2 points)

Exercise 174. Calculate the time mean speed. (2 points)

Exercise 175. Give the equation for Edie's generalised definition of density. (1 point)

There is an observer moving at 60 km/h.

Exercise 176. Calculate the flow of fast moving vehicles passing this observer. (3 points)

Exercise 177. What is the time mean speed (absolute to the road, not relative to the observer) of the vehicles moving this observer (hard question: 3.5 points, yielding 2 points) (2 points)

Exercise 178. Will the flow of slow moving vehicles passing the moving observer be larger than, equal to or lower than the flow of the fast moving vehicles passing the moving observer. Argue (rather than calculate) why. (2 points)

The capacity of the road is, independent of the vehicle class, 2000 veh/h, and the jam density is, independent of the vehicle class, 125 veh/km. Assume the car-following behavior of both classes can be described by Newell's car-following model.

Exercise 179. Draw (not sketch) the fundamental diagrams for the two vehicle classes (2 points)

Exercise 180. If we take the fast vehicles as reference, what is the pce value (or fce, "fast car equivalent") of the slow vehicle (so expressed in units of fast vehicles) (1 point)

Exercise 181. Give the car-following model equation for the fast vehicle, including the values of the parameters for the fast vehicles (only the free flow branch is needed). (3 points)

Consider these traffic operations at a two lane road. According to a lane selection model, all fast vehicles stay left and all slow vehicles stay right.

Exercise 182. What is the name of this model (only the name is needed – no reasoning). (1 point)

Now consider a different traffic state. Once traffic goes into the congested state, the fast cars move to the fastest lane.

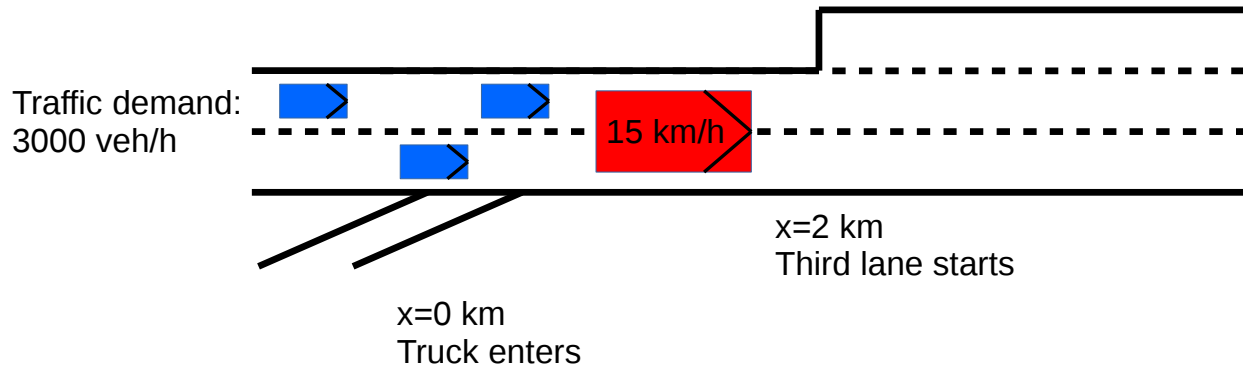
Exercise 183. Give the name of this state called according to three phase traffic flow theory. (1 point)

We now relax (read: ignore) the assumption of an equal number of vehicles at the inflow and the 1000 veh/h inflow. So we consider the general case of these vehicle classes, their fundamental diagrams, and this lane selection model.

Exercise 184. Indicate in the flow-density diagram (combined for all lanes and vehicle classes) in which areas points can be found (if Edie's definitions were used). (3 points)

A.7.4 Slow truck on the motorway

Consider a road for which on all of the lanes a triangular fundamental diagram holds with a critical density of 25 veh/km, a capacity of 2000 veh/h and a jam density of 125 veh/km. There is a two-lane road for a length of $x < 2$ km, and with an extra third lane for $x > 2$ km. The traffic demand is 3000 veh/h. At $t=0$ a wide truck (special transport) joins the road from $x=0$, driving at 15 km/h. This truck blocks two lanes, so in the two lane section, there are no overtaking possibilities: see figure.



Exercise 185. Sketch the traffic operations (both in space-time and in flow-density) for the time up to the moment the truck reaches the three lane section. (5 points)

After the truck reaches the downstream section, vehicles can overtake. The capacity point lies at $k=60$ veh/km and $q=2600$ veh/h for the whole roadway.

Exercise 186. Sketch the traffic operations (both in space-time as in flow-density) from the moment the truck reaches the three lane section. Sketch the slopes of the waves which occur from that moment, but do not consider possible waves which start later. (5 points)

A.8 Problem set 8

A.8.1 Short open questions

Exercise 187. Give the name of the distribution describing the headway distribution if the arrival process of vehicles is independent. (1 point)

A particular distribution function describes the number of vehicles per aggregation interval well if the flow on the road is high.

Exercise 188. Give the name of this distribution. (1 point)

The lane flow distribution is the ratio of the flow in a lane over the total flow.

Exercise 189. Express the relative flow in lane i f_i as function of the average headways $\langle h_i \rangle$, which are given for all lanes i on a motorway (3 points)

The theory of slugs and rabbits states there are two types of cars/drivers on the road. Assume they both have a pce value of 1.

Exercise 190. Give the meaning of the letters pce (give the full words). (1 point)

Consider the theory of slugs and rabbits. The demand (in veh/h) of slugs is equal to the demand of rabbits. Assume a two-lane road operating below critical density at all lanes.

Exercise 191. What is the distribution of the flow over the lanes in free flow conditions (qualitatively – no numbers are needed)? Give your reasoning. (2 points)

Exercise 192. Explain how stop-and-go waves emerge. Use, name, and describe the two most relevant levels of stability in your answer. (3 points)

Exercise 193. Explain why in the three phase theory of Kerner there is not one value for capacity. (1 point)

One of the advantages of using Lagrangian coordinates is that traffic predictions do not have “numerical diffusion”.

Exercise 194. Explain in your own words what “numerical diffusion” is. (1 point)

A.8.2 Microscopic effects on the fundamental diagram

Exercise 195. Give the conditions under which the fundamental diagram holds. (1 point)

When aggregating traffic, a better fundamental diagram can be found if instead of a rectangular area in space-time a parallelogram is used.

Exercise 196. Explain why, discussing free flow conditions as well as congested conditions. In your answer, also indicate the slopes of the edges of the parallelogram. (3 points)

Traditionally, the density is calculated at one moment in time over a road section, and the flow is calculated over a time period at one location.

Exercise 197. Give the name for the definitions used to express flow and density for an area in space-time. Equations are not needed. (1 point)

During acceleration, one could observe deviations from the fundamental diagram. Consider multi-anticipation, i.e. drivers adapting their speed not only on the leader, but also on vehicles further downstream. This influences amongst others transitions from a congested state to capacity.

Exercise 198. Describe for this transition the effect of multi-anticipation on hysteresis and sketch the effect of these changes in the flow-density plane (also show the normal FD in this graph as reference).⁴

A.8.3 Prediction of downstream conditions

The number of lanes on a freeway reduces from 3 to 2 to 1, as sketched below.



The one lane section forms an active bottleneck. Assume throughout this question a triangular fundamental diagram, equal for each of the lanes, with a free flow speed of 100 km/h.

In the three lane part, a driver is driving in congestion due to the reduction to one lane. His speed is 8 km/h and he estimates the gross spacing to his predecessor in the same lane at 11m. (If you are at one part unable to find the correct answer, assume one, state so clearly, and continue with the next part of the question).

Exercise 199. Assuming homogeneous conditions, calculate the flow through the bottleneck. (4 points)

Exercise 200. Calculate the jam density for the three lane part. Hint: use the capacity of the three lane part. (4 points)

Exercise 201. Calculate the speed of the vehicles in the two lane section. (3 points)

Changes of inflow can lead to a changing traffic state. Adapting inflow can then make the traffic state stationary (i.e. constant over time). Consider one of these stationary situations, with congestion spilling back to somewhere in the three lane section

Exercise 202. Sketch the flow (aggregated over all lanes) as function of space for this situation. (1 point)

Consider all possible stationary situations, which have a different accumulation (i.e., nr of vehicles in the area).

Exercise 203. Sketch the traffic production (here, average internal flow in veh/h) as function of the accumulation. Values are not needed in the sketch. (2 points)

A.8.4 Demonstration of police cars

The police are planning a demonstration by which they drive 30 km/h on all lanes of the motorway. In practice, the police cars travel as normal vehicles in the traffic stream before the demonstration. And at $t=0$, they slow down instantaneously to 30 km/h. During the demonstration (the slow driving), there are no overtaking possibilities. In this question, the traffic state upstream of the police cars is referred to as “congestion”. See the figure below for an idea.



In this question we consider the following variables:

1. The duration of the demonstration d
2. the demand (assumed constant throughout the demonstration), q_{in} .

After the demonstration, the police cars instantaneously accelerate to the free flow speed.

Assume a triangular fundamental diagram with a free flow speed of 80 km/h, a capacity of 2000 veh/h/lane (indicated C) and a jam density of 150 veh/h/lane. Consider a two lane road with no on and off ramps.

Exercise 204. Sketch the traffic states in space-time and in the flow density plane for a high demand (demand is higher than the flow in congestion). (6 points)

Exercise 205. Calculate the flow in the congestion. (3 points)

Exercise 206. Sketch the moved cumulative curves for the inflow and the moved cumulative curves for the outflow with the demonstration. Consider the inflow point upstream of any queue, and the outflow point downstream of any queue. Consider time frame from well before the demonstration to well after any queue. (4 points)

Exercise 207. Show that the total delay (D) is given by the equation $D = (1/2) * d^2 * q_{in} * C / (C - q_{in})$. (4 points)

Exercise 208. What happens to the delay if the demand approaches capacity? Explain from a traffic flow perspective why. (3 points)

Exercise 209. Sketch the traffic states in space-time and in the flow density plane for a demand lower than the flow in congestion (2 points)

Exercise 210. Argue whether the equation for the delay still holds in this case (1 point)

Exercise 211. Give the reasoning why the delay is quadratic as function of duration of the demonstration (3 points)

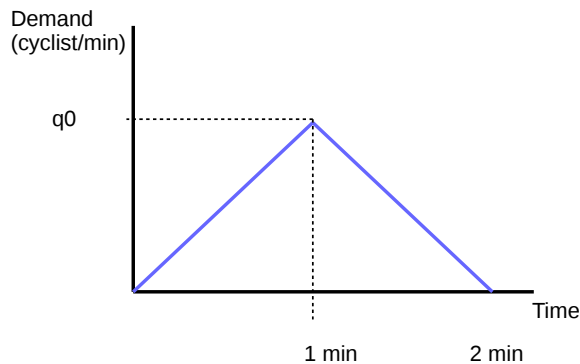
A.8.5 Stairs for cyclists at Delft train station

Currently, the station in Delft has an underground bike parking. To get to the street level, the cyclists need to dismount, and walk their bicycle up the stairs. See the picture below. Assume all cyclists do so with the bike at their right. The figures below give an impression of the site, although not at peak demand



Exercise 212. Calculate the capacity for this site based on an assumption of headway between people walking their bike. (3 points)

In the peak hour, a train arrives. Suppose 300 passengers leave the train station by bike using these stairs. Suppose the difference between the first passenger leaving the bike parking and the last one is 2 minutes. Assume a triangular demand pattern at the bottom of the stairs:



Exercise 213. Calculate the value for q_0 in this pattern. (3 points)

Assume the capacity C is lower than q_0 . Number the cyclists $1 \dots N$ in order of leaving the bike parking. The cyclist with the highest delay due to queuing is N_E .

Exercise 214. Derive the equation for N_E as function of C and q_0 . Give your reasoning. (If you are unable to give the equation, points can be awarded for a description of the construction.) (4 points)

A.9 Problem set 9

A.9.1 Short questions

The Macroscopic Fundamental Diagram relates the average density to the average flow.

Exercise 215. Give the name for the term used to indicate the average flow. (1 point)

Exercise 216. On a particular road the Greenshields fundamental diagram holds, with a free flow speed of 80 km/h and a jam density of 100 veh/km. Does this determine the capacity with no further assumptions? If so, calculate. If not, why not. (3 points)

Exercise 217. *Describe what an acceleration fan is. (2 points)*

On a road, traffic is measured using loop detectors at a cross section. For each aggregation period the flow is given as output, as well as the time mean speed of traffic passing that detector. Then, densities are computed from the speed and flow, and a relation between speed and flow is plotted.

Exercise 218. *Explain whether there is a bias in the densities; if yes, explain which and why; if no, explain why not. (3 points)*

Exercise 219. *Traffic in a model is locally stable. Can the platoons be unstable? Explain why or why not. (2 points)*

Exercise 220. *Explain when and why “random seeds” are needed (approximately 100 words, no equations needed). (2 points)*

A.9.2 Car-following in fog

Helly’s car-following model is given by the following equations:

$$a = \alpha \Delta v + \beta (s - s^*) \quad (\text{A.10})$$

$$s^* = x_0 + vT \quad (\text{A.11})$$

In this equation, a is the acceleration, v denotes the speed, Δv the difference in speed between the leader and its predecessor, s the spacing. Parameters in the model are α , β , x_0 and T . The interpretation of the parameters, and the meaning of s^* is left to the students. For reasons of simplicity, the time dependence and reaction time are ignored in this question.

Exercise 221. *Derive the equation of the fundamental diagram, $q=q(k)$, from the above equation for the congested branch. Hint: use the relation $v=v(s)$ in the derivation.*⁴

The model can be calibrated and validated.

Exercise 222. *Explain what is the value of validating the model (i.e., what can a validated model be used for, which cannot be done with a non-validated model). (1 point)*

The following parameters are found to fit the traffic best:
 $\alpha = 0.3\text{s}^{-1}$, $\beta = 0.08\text{s}^{-2}$, $x_0 = 20\text{m}$, $T = 1\text{s}$. (In this line, s means second and m meter). Besides the car-following part, also a free speed is required to derive a full fundamental diagram. This is found to be 30 m/s.

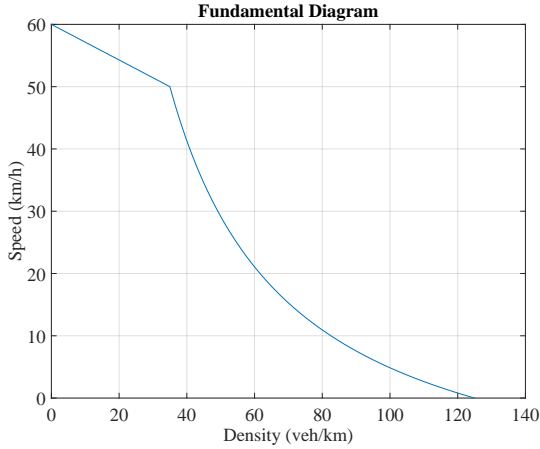
Exercise 223. *Compute the capacity of the road in veh/h (hard question) (2 points)*

The Dutch government recommends drivers in fog: “Half the speed, double the space headway to the predecessor”. Suppose everyone takes this advice.

Exercise 224. *Compute the capacity of the road in the fog. You may (but do not need to) relate this to question 2c; in case you did not find an answer to that question, assume an answer and state so explicitly. (3 points)*

A.9.3 Cleaning the road

Consider a one-lane road for which the following fundamental diagram holds:



This is a well-known fundamental diagram.

Exercise 225. Give the name of the shape of this fundamental diagram.(1 point)

Exercise 226. Compute the capacity of the road.(2 points)

Exercise 227. Sketch the fundamental diagram in the flow-density plane.(1 point)

A cleaning car enters the road to clean the road, driving at 15 km/h.

Exercise 228. Compute the maximum flow upstream of the cleaning car using the given fundamental diagram.(2 points)

The inflow to the road is 1200 veh/h; the cleaning car enters the road at $x=1$ km and leaves at $x=2$ km. Overtaking is not possible.

Exercise 229. Construct the traffic state using shockwave theory: i.e., sketch the traffic operations in the flow-density plan and in space-time(6 points)

A.9.4 Mobil lane changing model

The Mobil lane change model describes whether drivers change lanes or not. The equations for a European system (keep right unless overtaking) are given by the following equations. The utility for a driver is given by:

$$U_{\text{tot}} = U_c + \mathcal{P}(U_o + U_n) \quad (\text{A.12})$$

The utility is calculated for each lane. Acceleration is considered as utility, and subscripts indicate the current vehicle (c), the old follower (o) and the (potential) new follower (n). A lane change to the right is performed if

$$U_{\text{tot}}^{\text{right}} - U_{\text{tot}}^{\text{left}} \geq a_{\text{th}} - a_{\text{bias}} \quad (\text{A.13})$$

A lane change to the left is performed if

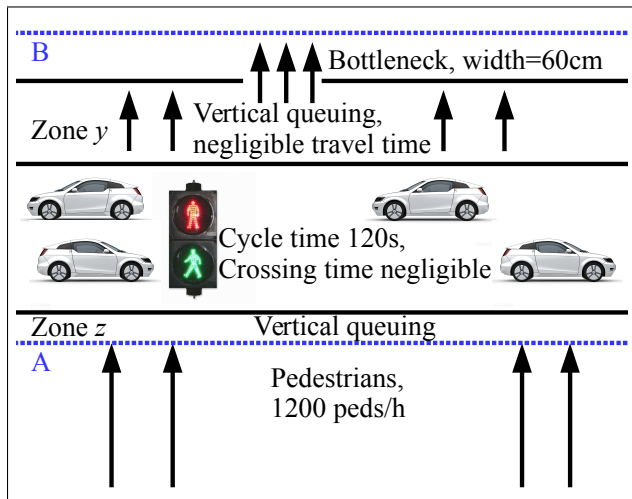
$$U_{\text{tot}}^{\text{left}} - U_{\text{tot}}^{\text{right}} \geq a_{\text{th}} + a_{\text{bias}} \quad (\text{A.14})$$

Exercise 230. Explain the working of the Mobil lane change model in words (approx 100 words); in your answer, include an interpretation for \mathcal{P} . (3 points)

Exercise 231. Give approximate values (including units) for a_{th} and a_{bias} , and reason why (3 points)

A.9.5 Pedestrians at a traffic light

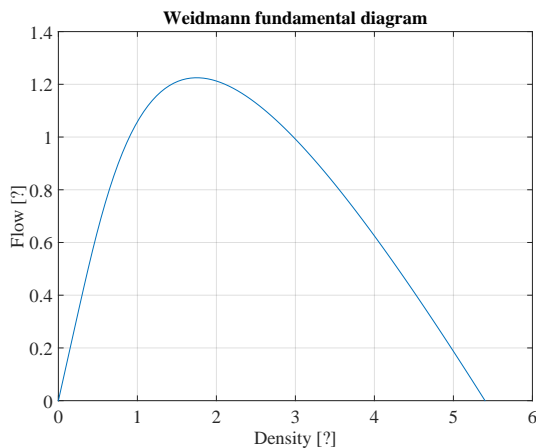
Consider pedestrians approaching the traffic light at a busy intersection. The pedestrians arrive independently at the traffic light at a flow of 1200 peds/h. The cycle time is 120 seconds. Assume all pedestrians cross the road simultaneously (next to each other) in negligible time and then the traffic light turns red again. (So the pedestrian traffic light is red for 120 seconds, then all pedestrians cross instantaneously and the traffic light turns red again instantaneously). A sketch of the situation is found below:



Exercise 232. Give the name of the distribution of the number of pedestrians arriving per red time. (1 point)

Exercise 233. How many pedestrians cross during a green phase. (2 points)

Weidmann proposed the following fundamental diagram for pedestrians.



Exercise 234. Give the units for the values at the axes. (2 points)

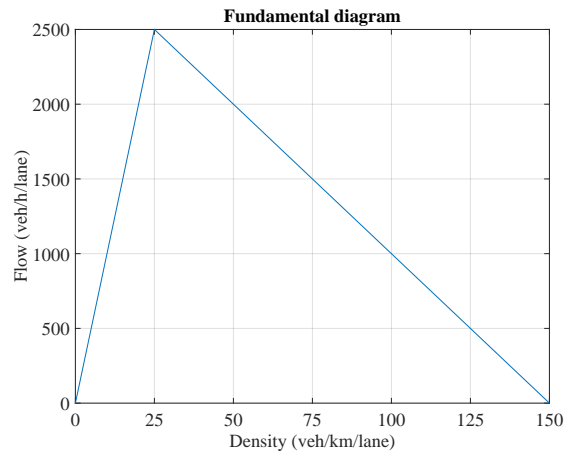
The pedestrians cross (simultaneously) during the green phase and arrive at the other side. After a short (negligible) distance, the sidewalk has a bottleneck of 60 cm wide. Assume that the Weidmann fundamental diagram holds. You may assume this bottleneck has no length (e.g., a door on the sidewalk).

Exercise 235. Calculate how long would it take the pedestrians to pass the bottleneck. (3 points)

Exercise 236. Sketch the moved cumulative curves for this situation (inflow at the blue dashed line "A", outflow at the blue dashed line "B") for a period of one cycle. Start your sketch just before the moment the traffic light is green, i.e. the pedestrians are about to cross the road. Hint: at that moment, how many pedestrians have then crossed line A and not line B? (3 points)

A.9.6 Hysteresis

On a road the following fundamental diagram holds under equilibrium conditions.



However, due to the delayed reaction of drivers, hysteresis occurs. Copy the fundamental diagram to your answer sheet.

Exercise 237. In the fundamental diagram, sketch which path the traffic states make in the transition from congestion to capacity and back. Argue why. (2 points)

Exercise 238. Draw (not sketch) the fundamental diagram in the speed-spacing plane. (3 points)

Exercise 239. Sketch the hysteresis of question a in the fundamental diagram in the speed-spacing plane. (1 point)

A.10 Problem set 9

A.10.1 Short questions

Consider a road where vehicles are arriving independently.

Exercise 240. Give the name for the distribution of the number of vehicles arriving within a time interval on this road. (1 point)

The pce value of a truck is claimed to be 2 for a road without queue warning systems.

Exercise 241. Explain in your own words what a pce value of two means. (1 point)

A study shows that by installing queue tail warning systems the capacity of the road increases. The factor by which it increases is 1.05 for passenger cars and 1.09 for trucks, meaning it can handle 5% more or and 9% more trucks.

Exercise 242. Based on the information above, calculate the new pce value for trucks for the road with queue warning systems (3 points)

Traffic simulation in Lagrangian coordinates has the advantage that there is less numerical diffusion.

Exercise 243. Explain in your own words what numerical diffusion in traffic simulation is. (1 point)

Exercise 244. Explain what is meant by local instability in traffic. (1 point)

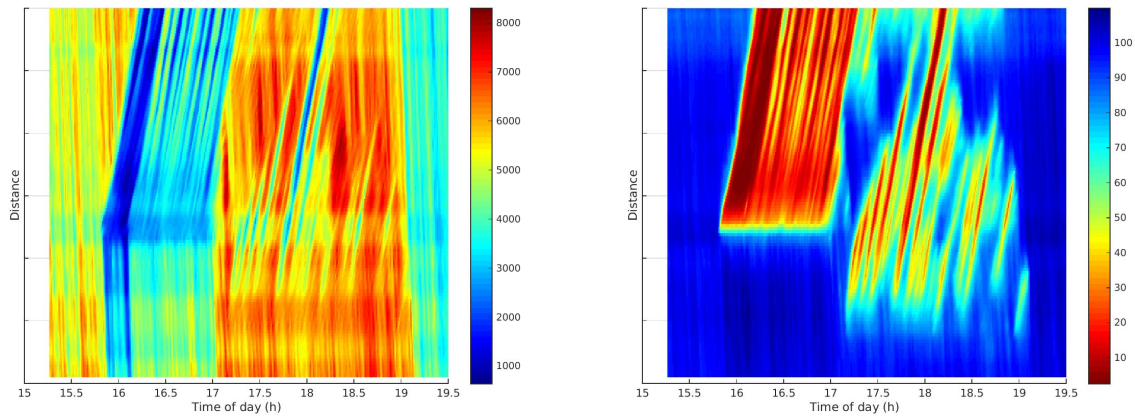
Exercise 245. Can a stationary tail of the queue occur due to a moving bottleneck? If so, explain how. If not, explain why not. (2 points)

Someone claims traffic on a road is behaving according to a Greenshields fundamental diagram with free flow capacity=2000 veh/h, critical density = 20 veh/km and $k_{jam}=150$ veh/km.

Exercise 246. Is this possible? If so, sketch the fundamental diagram in the speed-density plane and comment on the construction; if not possible, argue why. (2 points)

A.10.2 Traffic flow properties

Consider the following flow contour plot (left) and speed contour plots (right):



Exercise 247. Derive in which direction traffic is flowing (2 points)

The spatial scale is lacking.

Exercise 248. Reason what is the length of the road shown in the figure. Base your answer on traffic properties. (2 points)

Exercise 249. Does traffic at this day exhibit a capacity drop? If so, estimate the capacity drop, and explain how you find it. If not, explain how a capacity drop would show. For clarity, hand in the graphs in which you indicate the various observation points. (2 points)

A.10.3 Speeds

Consider a road with slugs and rabbits

Exercise 250. What are the behavioural assumption(s) with regard to lane choice for rabbits in Daganzo's theory of slugs and rabbits. (1 point)

Traffic is in a two-pipe regime, and the speed of rabbits is 100 km/h and the speed of slugs is 80 km/h. Instantaneously on the the road, the amount of slugs and rabbits is equal.

Exercise 251. Compute which fraction of flow is rabbits. (2 points)

Exercise 252. Compute the time mean speed. (2 points)

Exercise 253. Explain how the mean speed can be computed using Edie's generalised definitions. Equations only do not suffice; explanation of the working of the equations is needed. (2 points)

A.10.4 Analyse a car-following model

For car-following, the following model is being proposed (Helly model):

$$a(t) = \alpha (v_i(t - \tau) - v_{i-1}(t - \tau)) + \beta (x_{i-1}(t - \tau) - x_i(t - \tau) - s_0 - T v_i(t - \tau))$$

In this model, x denotes the position, v denotes the speed and a denotes the acceleration, all evaluated at a time t or $t - \tau$ ($\tau > 0$ representing a reaction time); subscripts i and $i - 1$ indicate the current vehicle or its leader, respectively. Further parameters of the model are s_0 and T , as well as sensitivity parameters α and β .

Exercise 254. Explain the working of this model in words.(2 points)

Exercise 255. Sketch the congested branch of the fundamental diagram in the speed-spacing plane. To do so, first derive this relationship in mathematical expressions.(5 points)

Due to hysteresis not all traffic states are on the fundamental diagram.

Exercise 256. Sketch in the speed-spacing plane how traffic states move in the fundamental diagram, i.e. indicate hysteresis. Motivate your answer.(2 points)

The fundamental diagram can be transferred to the flow-density plane.

Exercise 257. Derive this relationship mathematically.(2 points)

A.10.5 Traffic light

Consider a road at an intersection. The traffic can be described with a triangular fundamental diagram with a capacity of 1500 veh/h, a free flow speed of 50 km/h and a wave speed of -15 km/h. The inflow is 1000 veh/h.

Exercise 258. Sketch the fundamental diagram in the flow-density plane.(1 point)

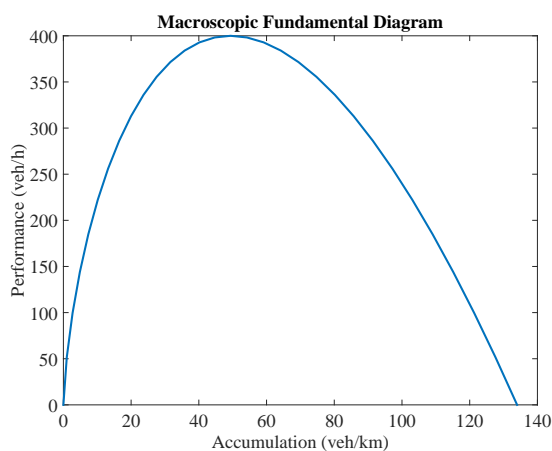
Exercise 259. Compute the jam density. (2 points)

At $t=0$, the traffic light turns red for 2 minutes. Then, the traffic light turns green for 0.5 minute, after which the traffic light turns red again for 1 minute. Afterwards, the traffic light stays green.

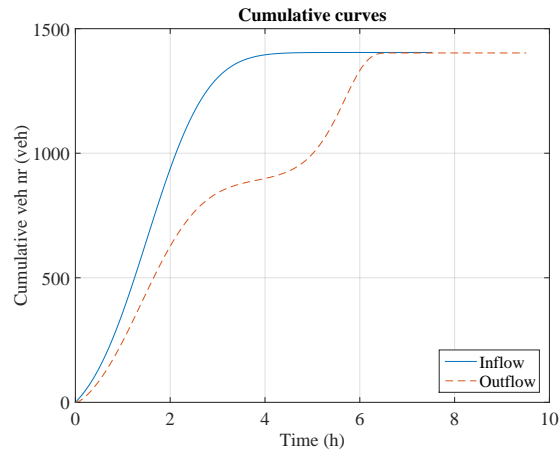
Exercise 260. Using shockwave theory, sketch the traffic states in the space-time diagram and show the states and waves in the flow density diagram. Comment on how you find the lines. (9 points)

A.10.6 Macroscopic Fundamental Diagram

For a zone the following Macroscopic Fundamental Diagram holds:



The performance on the vertical axis indicates the outflow out of the zone; the total road length in the network is 3.8 km. Assuming homogeneous and stationary traffic conditions, the following cumulative inflow and outflow curves are obtained:



The inflow curve is a result of (exogenously given) demand.

Exercise 261. Sketch the inflow pattern as flow over time; estimate the maximum flow into the road. (2 points)

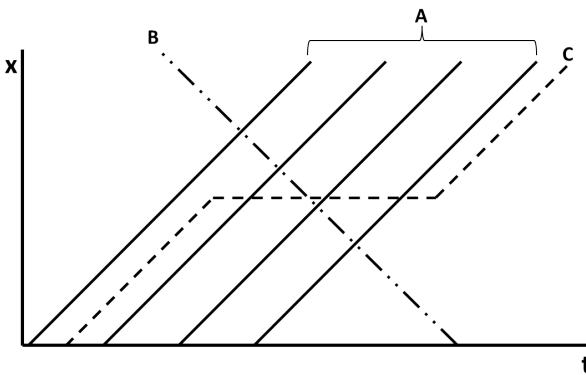
Exercise 262. Explain the shape of the outflow curve; in particular, include a description of the process underlying the shape from $t=2h$ to $t=5h$. (3 points)

Exercise 263. Explain how perimeter control can reduce delay. (2 points)

Exercise 264. Sketch in the graph the amount of total delay that can be reduced; comment on your construction. (2 points)

A.10.7 Non-vehicular traffic

Consider the trajectories of pedestrians in this figure:



The trajectory of pedestrian C is temporarily horizontal.

Exercise 265. Does this imply he is standing still? Argue why. (1 point)

Pedestrian traffic can be described with the social force model

Exercise 266. Give a conceptual description of the model (equations are not needed); in your answer, include whether the model is microscopic or macroscopic. (3 points)

Appendix B

Solutions to test questions

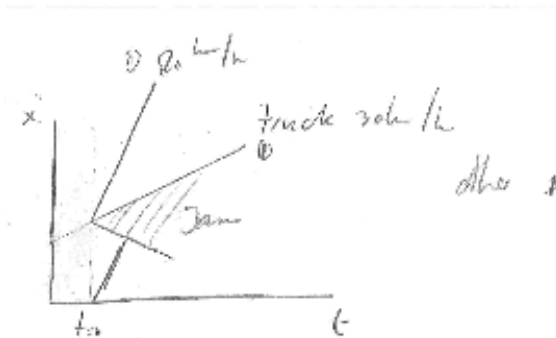
- 1** Note that there is a capacity drop here, so the fundamental diagram should either contain a capacity drop (e.g., inverse λ) or be curved.
- 2** Slugs stay always in the right lane (1) Rabbits choose the fastest lane (1) Free speed of rabbits is higher than the free speed of slugs (1)
- 3** A count of the number of vehicles over time at one location (1).
- 4** A model describing the inflow and outflow of the vehicles, with a restriction on the maximum outflow rate. The queues will not occupy any horizontal space (1). This is basically two cumulative curves, inflow and outflow, at one location, in which the angle of the outflow is maximized at capacity (1).
- 5** Time mean speed, since the faster cars are weighted higher (1)
- 6** $u = 1 / \sum_i (1/v_i)$
- 7**
1. Free flow \Rightarrow free driving + speed
 2. Synchronized flow \Rightarrow equal speeds in both lanes, speeds < 70 km/h
 3. Wide Moving Jams \Rightarrow backwards travelling waves, v very low.
(1 point for names, 1 for definitions)
- 8** Down-top \Rightarrow stop-and-go wave travelling backwards (0.5) Stop -and-go wave (0.5) and a local bottleneck at 482 (0.5) causing an area of synchronised flow (congestion) (0.5)
- 9** down-top. Finer structure within the congested part. (0.5) Moving bottleneck (0.5) \Rightarrow structure moves upstream (1) Data error at 8am (1)
- 10** down-top, from the shockwave speeds (0.5) Incident (1) Synchronized flows (and stop-and-go waves) (1) Moving bottleneck after resolving (1)
- 11** Trajectory of vehicle is its leaders' trajectory delayed in time (1) and moved backwards in space (1).
- 12**
1. Follower-leader (local) \Rightarrow over reaction on disturbance in one leader-follower pair
 2. Platoon \Rightarrow disturbance grows in a platoon
 3. Traffic flow \Rightarrow space between platoons is insufficient, so a disturbance in a platoon causes a delay in the next platoon

13 Yes. Smoothing (1) of disturbances improves platoon stability (1). Thereby, the amplitudes of a disturbance are reduced (1).

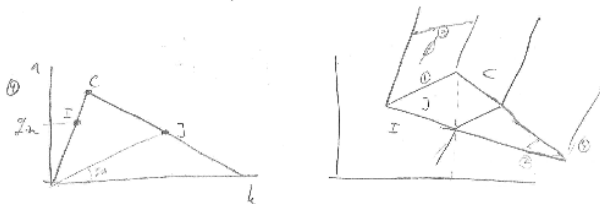
14 A slower vehicle can merge into another lane, which causes a disturbance, growing to a breakdown (1)

15 Now the lane distribution is uneven (1). If vehicles change towards lanes with lower densities, a jam might be prevented (1).

16 Use the triangular fundamental diagram. For the congested branch, the equation is $q = 2000 - 2000/100 \cdot (k - 25)$. From the speed we $q = kv = 30k$. Solving this set of equations (1), we find $k = 50$, and thus the flow of $30 \cdot 50 = 1500$ veh/h (1)



17 Starting with shockwave theory can be rewarded with 1 pt.



18 in I: flow 5000 veh/h, and density 62.5 veh/km, using the equation for the congested branch used in e (1 point). In J: $q = 4500$ veh/h, $k = 150$ veh/km. $W_j = -500/87.5 = -5.7$. So it moves with 4.7 km/h upstream (1).

20 Already in drawing

21 Speed is equal to the truck speed, 30 km/h. (1)

22 Width of a runner 75 cm (1 point for 50-100 cm), headway 1.5 sec (1 point for 0.9 2 seconds). 25 meters / 0.75 = 33,3 runners per roadway (both this, and the rounded values are correct). The capacity is $33,3/0,75 \times 3600 = 73,200$ pedestrians per hour.

23 $30,000/79,200 \times 60 \text{ min/h} = 23 \text{ min}$. (1)

24 Halfway: 1 hour duration of the passing of all runners (1) 30,000 runners in 1 hour -> $30,000/60 = 500$ runners per min. (1) Assumed earlier: 75 cm width, 1.5 second headway capacity $1/(0.75 \times 1.5) = 0,89 \text{ ped/m/s} = 53 \text{ ped/m/min}$ (1) The required width: $500/53 = 9,4 \text{ meters}$. (1)

25 The congested branch is not a line, but an area (1)

26 An MFD relates the average density in an area, the accumulation, to the average flow in the area

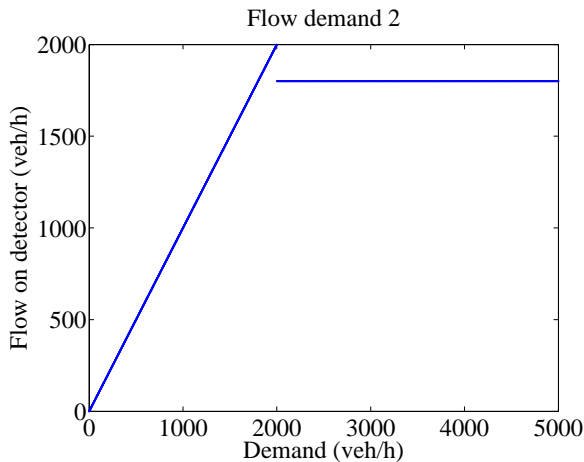
27 The MFD is flattened at the top compared to the regular FD (1). This is due to averaging effects: the top can only be reached if *all* links are operating at capacity. If some have a over-critical density and some an under-critical, the average density can be critical, but the flow is less than at capacity (1).

28 The CTM is a numerical scheme to calculate traffic flows in a macroscopic way (0.5), based on demand of the upstream cell and supply of the downstream cell(0.5). The flow is the minimum of both (0.5); demand is increasing with density up to the critical density and remains constant afterwards, supply starts at capacity and starts decreasing from capacity (0.5)

29 Lagrangian coordinates are used in macroscopic traffic flow description. Instead of fixing coordinates at moments in space, the coordinates go with the traffic (1). Variables used in this system are hence time, *vehicle number* (1) and speed. This is an advantage since the representation of traffic flow equations is more accurate (no numerical diffusion) (1)

30 The maximum flow on the road before the onset of congestion is higher than the flow of vehicles driving out of congestion. (0.5) This phenomenon of drivers keeping a larger headway after a standstill is called the capacity drop. (0.5)

31 Approximately a few to sometimes 30% is claimed



32 (1 for shape + 1 for capacity drop):

33 the flow equals the demand (0.5), but is never higher than the capacity, and it will not decrease (no over-critical densities) (0.5). Capacity drop explained if present.

34 Capacity is approximately 2000 veh/h/lane (1500-2500: 0.5 pt, possibly lower if urban roads are assumed and explained), so 4000 veh/h for the roadway (0.5)

35 Effective green: $(g - 3)$ seconds per direction (0.5). The cycle time is $c = 2(g + 2)$ (0.5). Thus, $g = (c/2) - 2$ (0.5). Relative green time: $2 \frac{g-3}{c} = 2 \frac{c/2-5}{c}$ (0.5) $= 1 - \frac{10}{c}$.

36 Relative green time per direction is half that of the total relative green time: $\frac{1}{2}(\frac{1}{2}point)(2points) - \frac{5}{c}$ (1). The flow when effective green is $3600(sec/h)/2(s/veh)=1800$ vehicles per hour, or $1/2$ vehicle per second (either flow value: 1 point). The flow per direction is thus $1/2(\frac{1}{2}point)(2points) - \frac{5}{c}$ with flow in veh/s and c in seconds or $1800(\frac{1}{2}point)(2points) - \frac{5}{c}$ with flow in veh/h and c in seconds. (1 point)

37 Both methods will yield the same answer, since not the queue length, but the flow is asked. (1) Most vehicles come from direction 2, so the green time (still equal) should be based on direction 2 (1). Using the equation from the last question, we have $1800(\frac{1}{2} - \frac{5}{c}) = 800$ (0.5). Solving this for c yields $\frac{1}{2} - \frac{5}{c} = \frac{8}{18} = \frac{4}{9}$. So $\frac{5}{c} = (\frac{1}{2}point)10$, so $c = 50$ seconds(0.5).

38 Poisson distribution

39 The cycle time is 120 seconds. The expected number of vehicles in a cycle is $120/60 * 800/60 = 160/6 = 26.7$ (0.5) so $\lambda = 26.7$ (0.5) 120 seconds cycle time, so 60 seconds per direction. 5 seconds are lost (2 s clearance time and 3 s startup loss), so 55 seconds leading to $\text{floor}(55/2)=27$ vehicles at maximum through a green phase (0.5). The probability of an overflow queue is the probability that the number of cars arriving is 28 or larger, $P(X \geq 28)$ (0.5); this can be calculated by $1 - P(X \leq 27)$ (0.5). This is calculated as $p = \sum_{k=0}^{27} \frac{26.7^k e^{-26.7}}{k!}$ (0.5)

40 The spread of a Poisson arrival process is larger(0.5), so the probability of having overflow queues is larger(0.5; only with correct reasoning)

41 Vehicles accelerate in principle with acceleration a , but this reduces when they approach their desired speed (1) or if they approach their desired distance (1). The desired distance increases with speed.

42 It is a translation of the leaders' trajectory (0.5), translated forward in time by a fixed value τ and back in space by Δx (0.5).

43 Choose two:

- Drivers are considering multiple vehicles ahead
- Drivers are unable to judge perfectly speed and gap
- Drivers are not changing acceleration continuously
- There is also interaction with lane-changing

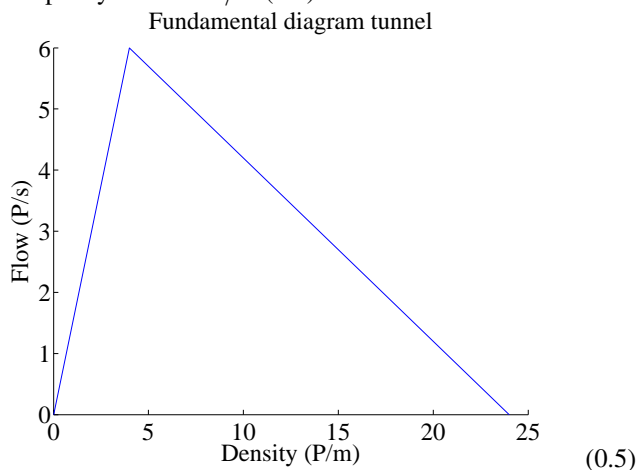
44 Choose 2:

- It better captures the non-equilibrium conditions.
- There is a possibility that stop-and-go waves form (instabilities).
- Drivers have a finite acceleration

45 Choose 2 (1 point per good answer):

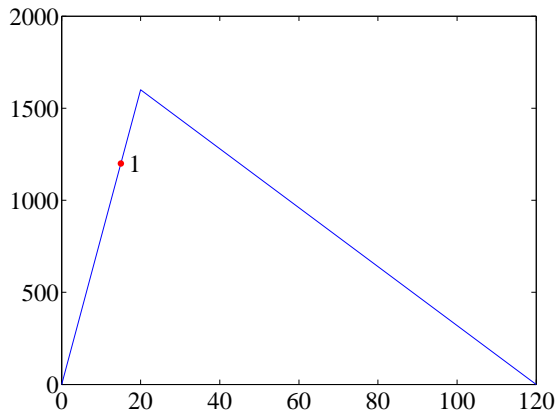
- In the IDM, drivers will, unrealistically, never reach their desired speed, not even if the distance is larger than the desired distance
- It has less parameters to calibrate – more realistic
- It is better understandable

46 Convert the densities to tunnel-wide properties. The critical density then is $4P/m$ and the jam density $24P/m$. (1) The capacity is $vk=6 P/s$. (0.5)



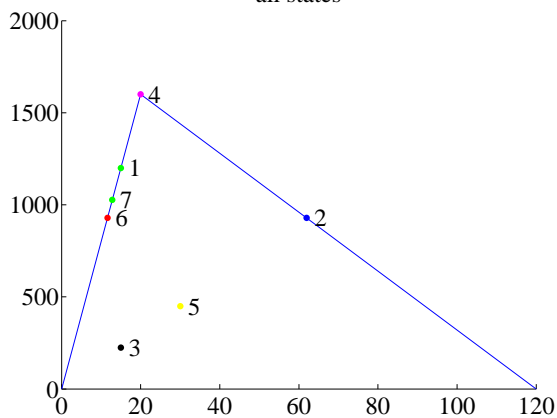
47 180P/min = 3 P/s (unit conversion: 0.5). Undercritical (of course, the tunnel is the bottleneck!), so $v=v_f$. $k = q/v=3/1.5=2$ P/m (0.5). That is 2 pedestrians per meter length, so 0.5 pedestrians per m^2 (1)

48 30 vehicles in a 2 km section, so the density is 15 veh/km. (0.5)
initial states



(figure: 0.5);

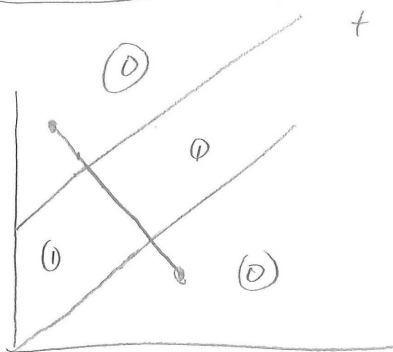
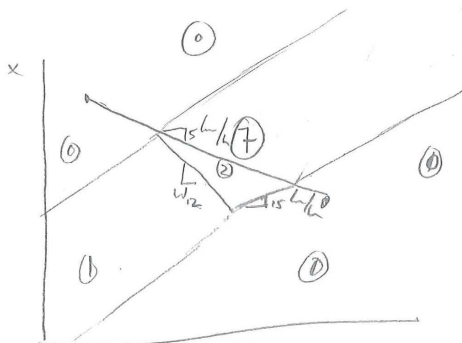
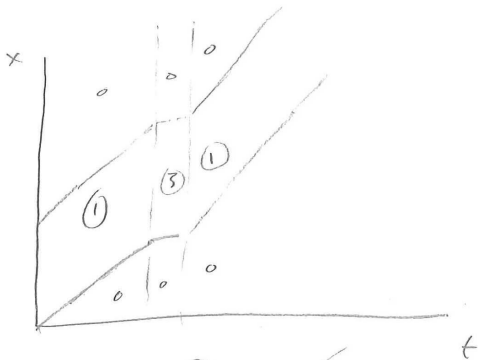
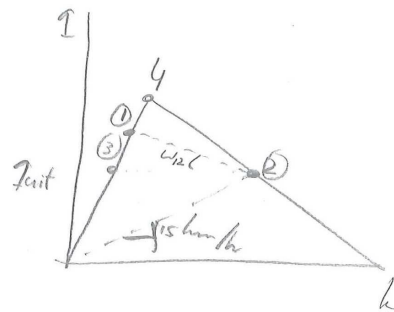
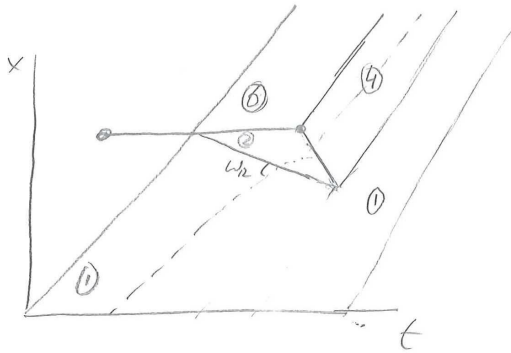
49 Draw a line with an slope of 15 km/h up in the fundamental diagram. You find the intersection with the congested branch at point 2. (0.5 point) The flow is lower than the initial conditions, so congestion occurs. (given)
all states



(0.5 points)

For the xt-plot we start with the bottleneck at a constant x from t_1 to t_2 . This causes traffic state 2 to occur. The boundary moves backwards with $w_{1,2}$, which is the same as the angle in the fundamental diagram between state 1 and 2. (0.5). Downstream, the flow is the same as the capacity in 2, but in free flow (state 6) (0.5). After removal of the bottleneck, there are capacity conditions (0.5) and the shock waves propagate with speeds equal to the angle 2-4 and 1-4 (0.5 combined). From t_1 there also is a shock wave separating state 1 and 6, moving with a speed equalling the slope of line 1-6 in the FD (0.5). Trajectories: 0.5.

All xt-plots are found in the next figure



50 Since it is temporal, the density remains constant (1 point). This leads to the construction of point 3 at the intersection of the line with a slope of 15 km/h and the density of 15 veh/km (0.5, including showing this point in the graph). Trajectories 0.5.

51 It is given that the tractor moves back very slowly, so we start at the situation comparable to b/. That means there will be a congestion state at the fundamental diagram where people drive 15 km/h (0.5), state 2 in the graph. The moving vehicle forms a boundary in shockwave theory (1), separating state 2 from another state where traffic moves out of the queue. By using the speed of the tractor, we find state 7 (0.5) as outflow state. After the tractor leaves the road, traffic is at capacity (0.5) and restores just like in question c (0.5).
fundamental diagram (0.5) & trajectories: (0.5)

52 The tractor forms a moving bottleneck, and the boundary between two traffic states (0.5). It separates the initial traffic state 1 from another traffic state where vehicles travel at 50 km/h (1). Constructing this in the fundamental diagram is done by drawing a line with a slope of 50 km/h down from point 1. We find the traffic state next to the tractor at this point (0.5), drawing point 5 in fundamental diagram: 0.5. The end of the tractor has a similar effect of a boundary (0.5) moving with 50 km/h. Constructing this in the fundamental diagram gives back point 1 (0.5). So at both ends, we have traffic state 1 (1), and next to the truck state 5 (no points for that). There are no other shock waves. Trajectories move either straight on, or are delayed a bit next to the tractor. (0.5)

53 The left one is Eulerian. It shows numerical diffusion. Moreover, the grid structure in time and space is clearly visible, whereas in Lagrangian coordinates the grids follow a fixed time and the vehicles (trajectories are visible in the right figure) (1 point for one of the explanations)

54 The representation of traffic flow equations is more accurate (no numerical diffusion) (1); also, the calculations are more efficient since it is not needed to consider both the upstream and downstream cell as with Eulerian coordinates (e.g., CTM) (1)

55 The relative amount of space (in time! -0.5 if not mentioned) that a non-passenger car vehicle occupies on the road

56 Trucks are longer, which influences the pce value. If the pce is the ratio of the length + net headway, assuming the same net headway the pce value increases with decreasing speed.

57 Trucks are longer, which influences the pce value. If the pce is the ratio of the length + net headway, assuming the same net headway the pce value increases with decreasing speed.

58 Vehicles accelerate in principle with acceleration a , but this reduces when they approach their desired speed (1) or if they approach their desired distance (1). The desired distance increases with speed.

59 In regular cf-models, the drivers react on actions by their leader. In multiple-leader models, drivers take several leaders into account in determining their action

60 Calculate for both leaders the desired distance:

$$s_1^*(v, \Delta v) = s_0 + vT + \frac{v \Delta v}{2\sqrt{ab}} \quad (\text{B.1})$$

and

$$s_2^*(v, \Delta v) = s_0 + 2 * vT + \frac{v \Delta v}{2\sqrt{ab}} \quad (\text{B.2})$$

Note that the desired distance to the second leader has twice the speed component.(1) Each of these will lead to an acceleration:

$$a_1 = a_0 \left(1 - \left(\frac{v}{v_0} \right)^4 - \left(\frac{s_1^*(v, \Delta v)}{s} \right)^2 \right) \quad (\text{B.3})$$

$$a_2 = a_0 \left(1 - \left(\frac{v}{v_0} \right)^4 - \left(\frac{s_2^*(v, \Delta v)}{x_2 - x_0} \right)^2 \right) \quad (\text{B.4})$$

(1) (Note the desired distance to the second leader is compared with the distance between the second leader and current vehicle) These have to be combined into one acceleration (0.5). For safety, we choose the minimum acceleration rather than for instance the mean:

$$\frac{dv}{dt} = \min\{a_1, a_2\} \quad (\text{B.5})$$

(0.5)

61 This basically is the same as the 2-leader model. First formulate the desired distance to the n-th leader

$$s_n^*(v, \Delta v) = s_0 + nvT + \frac{v \Delta v}{2\sqrt{ab}} \quad (\text{B.6})$$

(1) Then calculate the resulting acceleration for each of them:

$$a_n = a_0 \left(1 - \left(\frac{v}{v_0} \right)^4 - \left(\frac{s_n^*(v, \Delta v)}{x_n - x_0} \right)^2 \right) \quad (\text{B.7})$$

These have to be combined into one acceleration (0.5). For safety, we choose the minimum acceleration rather than for instance the mean:

$$\frac{dv}{dt} = \min\{a_n\} \quad (\text{B.8})$$

(0.5)

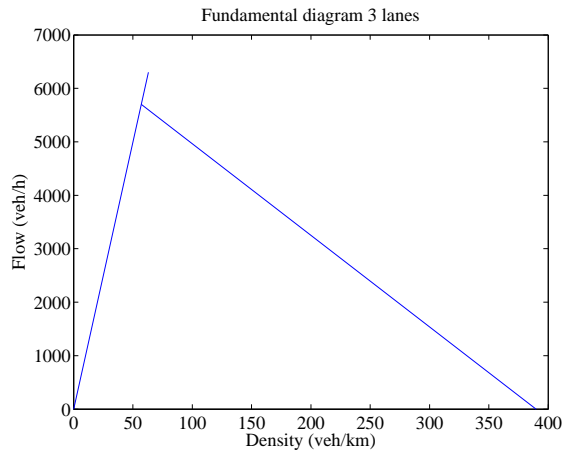
62 The edgy line is the flow, since the demand will never exceed the flow

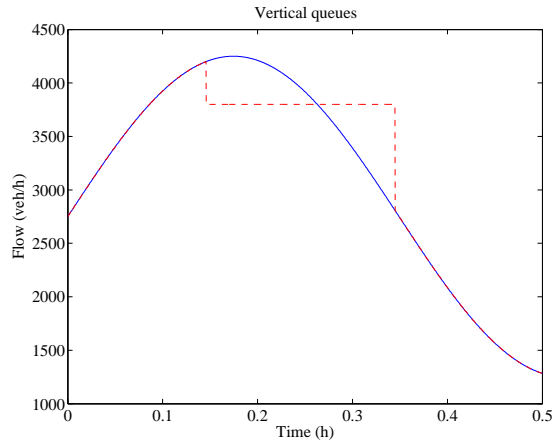
63 The free flow capacity can be found by the flow at the upstream detector before congestion sets in (1), so 4200 veh/h (read from the graph at the time congestion sets in)(1)

64 The queue discharge rate can be found by the flow after congestion has set in (1), so 3800 veh/h (1)

65 The free flow capacity is higher than the queue discharge rate, i.e., there is a capacity drop (1 for either explanation)

66 The FD should have a capacity drop (see previous questions), so the simplest is to assume an inverse lambda shaped FD (0.5 pt either by naming or in drawing) The free flow capacity is found in question a: 3x2100 veh/h. Also the free flow speed is known (from the speed figure): 100 km/h (0.5 for both combined). This gives the free flow branch (0.5 point for drawing). The density matching the queue outflow rate can be found on the free flow branch, by looking up the density for the queue outflow rate (0.5). $Kc = qc/v_{free} = 1900/100 = 19$ veh/km. (multiply by 3 for the 3-lane section (1)). Furthermore, it is known that with a flow of 2 lanes x 1900 veh/h/lane (the flow through the bottleneck), the speed is 22,6 km/h (read from graph) (1 pt), which gives a density of $3800/22.6 = 168$ veh/km (0.5 pt). Now, the congested branch can be constructed. We find the wave speed $w = \Delta q / \Delta k = ((3*1900) - (2*1900)) / (3*19 - 168) = -17$ km/h. The jam density is found by $k_j = Kc - qc/w = 3*(19 - 1900/-17.1) = 390$ veh/km (0.5 pt).

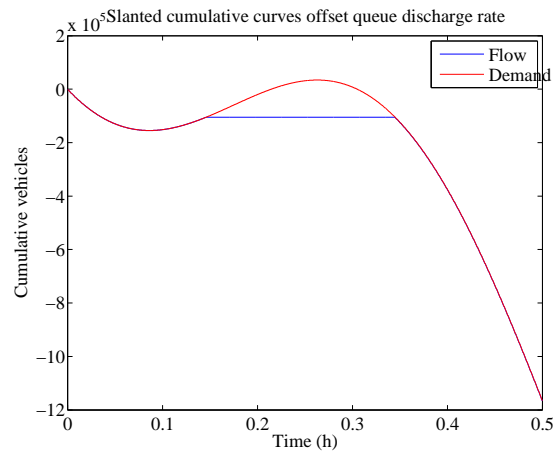




67

Points for the general shape (1) and for the correct times of flow change (1)

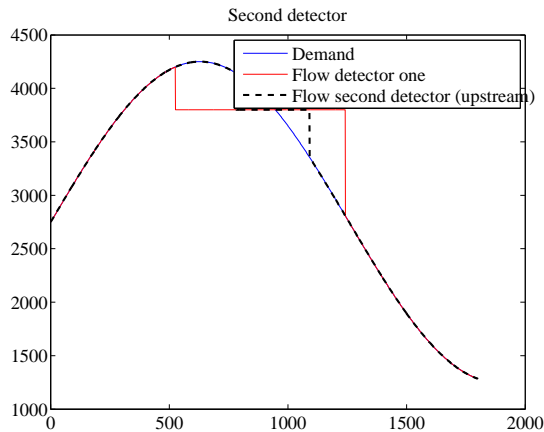
68 The most useful offset is the maximum flow of the road which is maintained for a while, i.e. the queue discharge rate (1 pt). (Alternative: the free flow capacity: 1/2)



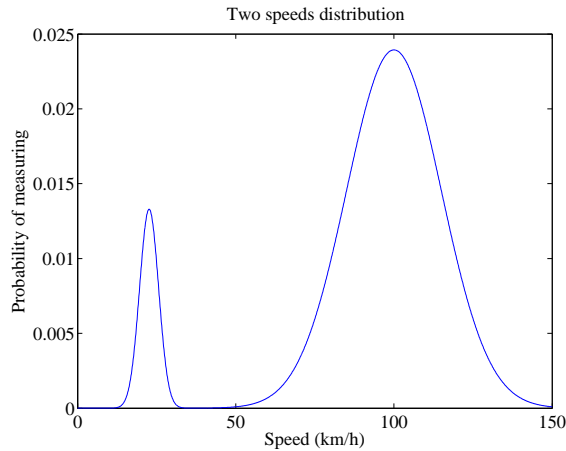
69

70 This is the area between the curves

71 It takes a while before the congestion spills back to the second detector. Similarly, congestion resolves from the tail, so the flow starts following the demand already earlier in time



72 If we do not relax the assumption of the fundamental diagram, there are only two speeds: the free flow speed and the speed for the state in the congested branch where the flow matches the queue discharge rate for the 2 lane stretch. (1) The frequency at which they are measured depends on the relative time of congestion (typically, 2 peaks at each 1 hour of congestion, so approximately 10% of the time congestion) (0.5). Relaxing the assumption of the fundamental diagram now, we do not find two exact values of the speed, but a distribution centered around two values:



(0.5)

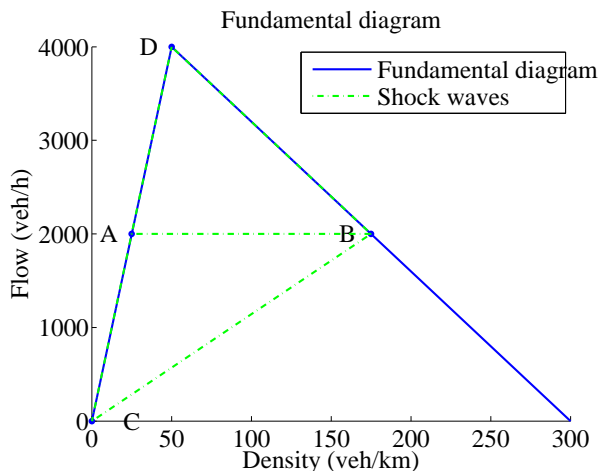
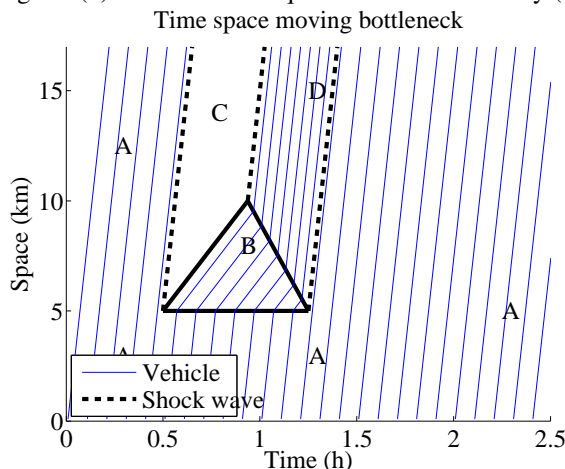
73 Capacity is maximum flow, $q = k u = 25 \times 80 = 2000$ veh/h/lane. For a two lane section, this is 4000 veh/h. (1 for points) plus 1 for graph

74 Since the tail is at the same place, the flow in the queue should be equal to the inflow (1), so 2000 veh/h.

75 The fundamental diagram is described by $q = C(1 - ((k - k_c)/(k_j - k_c)))$; use $k_j = 300$; $C = 4000$; $k_c = 50$; (1) Use the fundamental diagram to find the density at $q = 2000$ veh/h. (0.5) Solving $q = 1000$ veh/h gives $k = 175$ veh/km (0.5)

76 The speed of the vehicle is equal to the speed in the congested state (1). Using $q = k u$ (0.5), this gives $v = 2000/175 = 11,4$ km/h (0.5)

77 The truck drives at 11,4 km/h, and forms the moving bottleneck for 5 km. This can be plotted in the space time diagram (1). The tail of the queue remains stationary (1).



For the solution of the traffic jam, construct the line in the FD between the jam point and the capacity point (1). Finishing the figure: 1 point.

78 The queue has at maximum a length of 5 km, and the density is 175 veh/km – so $5 \times 175 = 875$ veh.

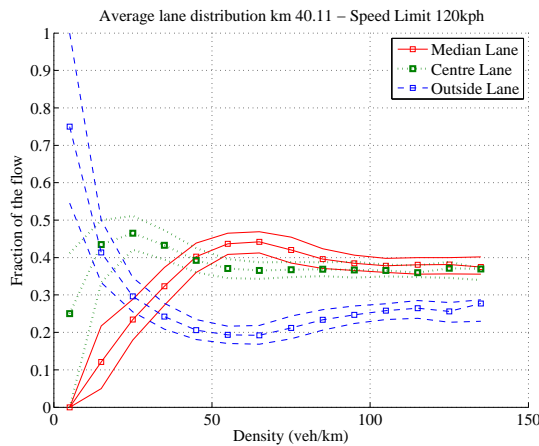
79 Two-pipe regime and one-pipe regime

80 Two-pipe regime (1). Trucks drive in one lane, and passenger cars in the other, at higher speeds (based on the density) (1).

81 The speed of the passenger cars is higher, so they will pass the stationary detectors more “often” (1). Hence, the fraction of the flow will be higher (1).

82 Requested is the fraction of the flow of passenger cars, (class 1): $\rho = q_1/q_{tot} = q_1/(q_1 + q_2) = (k_1 v_1)/(k_1 v_1 + k_2 v_2)$. (1 point for $q = kv$ per class).

From the image we know $k_2 = 4/7 * k_1$ (0.5 point), so $\rho = (k_1 v_1)/(k_1 v_1 + 4/7 k_1 v_2) = v_1/(v_1 + 4/7 v_2)$ (0.5 point) in which v indicates the speeds. Assuming $v_1 = 120$ km/h and $v_2 = 80$ km/h (1 point – assuming equal speeds maximizes the nr of points for this question to 1), we find: $\rho = 120/(120 + 4/7 * 80) = \dots$ (1)



83 If it is really quiet on the road, people keep right (hence blue is right). When it gets busier, more people go towards the middle lane, and then towards the left lane. (0.5 for the right reasoning, 0.5 for drawing the right conclusions; no points for only conclusions; 0.5 if middle and median lane exchanged.)

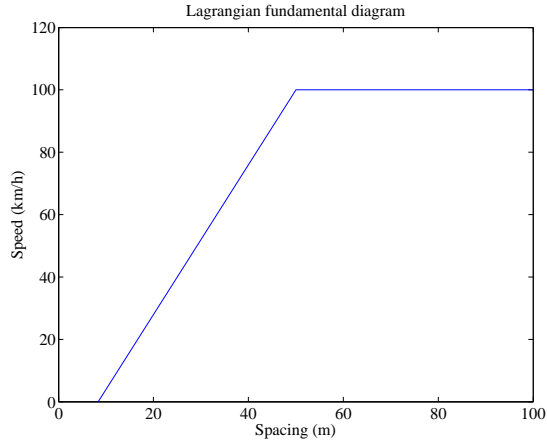
84 Slugs stay always in the right lane (1) Rabbits choose the fastest lane (1) Free speed of rabbits is higher than the free speed of slugs (1)

85 Near capacity, the left lanes travel still faster then the right lane (1). All rabbits are hence in the left lane, leaving gaps in the right lane (0.5) which hence has a lower flow (0.5)

86 It averages the flow and densities (0.5) *for an area* (by which it differs from the regular FD) (1) and relates them to each other (0.5)

87 The average flow decreases for the same average density if the traffic is distributed less homogeneously over the network.

88 The speed is increasing with increasing spacing (0.5). There is a minimum spacing (0.5) and a maximum speed (0.5). Plot: 0.5



89 Vehicles have a desired speed v^* which is determined by the distance to their leader (1). The acceleration is proportional to the difference between their speed and the desired speed.

90 Traffic must be stationary and homogeneous

91 If traffic is stationary, the acceleration is 0 (1), so $v = v^*$ (1). Realising that $k = 1/\Delta x$ (0.5), or correcting for the units (density is in veh/km!) we find $k = 1000/\Delta x$ (0.5), leading to:

$$v = 16.8(\tanh(0.086((1/k) - 25) + 0.913)) \quad (\text{B.9})$$

(0.5) This is the speed in m/s, which should be translated into km/h, so:

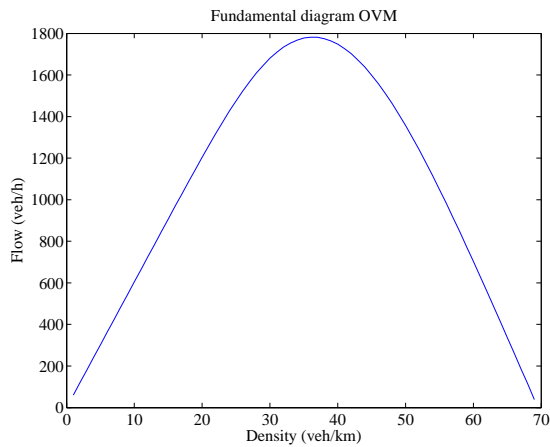
$$v = 3.616.8(\tanh(0.086((1/k) - 25) + 0.913)) \quad (\text{B.10})$$

(0.5) Now applying $q=ku=kv$ (0.5), we find

$$q = k3.616.8(\tanh(0.086((1/k) - 25) + 0.913)) \quad (\text{B.11})$$

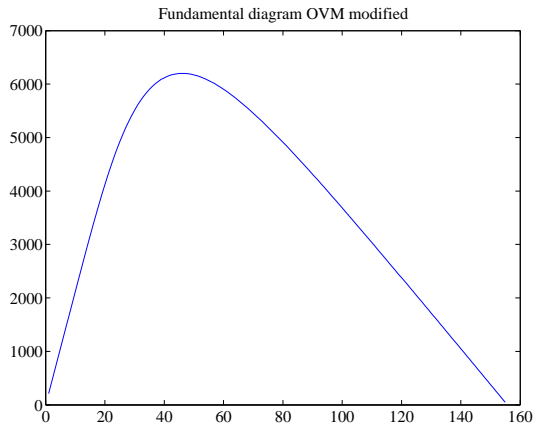
(0.5)

92 The fundamental diagram is shown below:



From this, we read a capacity of approximately 1750 veh/h, the free flow speed is approximately 60 km/h and a critical density of approximately 70 veh/km(1).

93 A free speed of 60 km/h could match a provincial road. However, the capacity for a provincial road is usually not so high. For sure, the jam density would be more in line with the jam density of motorways, i.e. well over 100 veh/km. Therefore, the fundamental diagram is not very accurate. It would be better to have a higher jam density, so scale the graph on the horizontal axis, meaning the number 0.086 should be lower (by about a factor $125/75=1.75$ – increasing the jam density to 140). Then, the speed drops even further, so that should be corrected (increase a factor 1.75), and then once more increased by a factor of almost 2 to get a motorway speed. This means increasing 16.8 to $1.75 \times 2 \times 16.8=...$ While this would give a proper free speed and jam density, the capacity increases to extreme values (1), so a proper parameter set is not possible



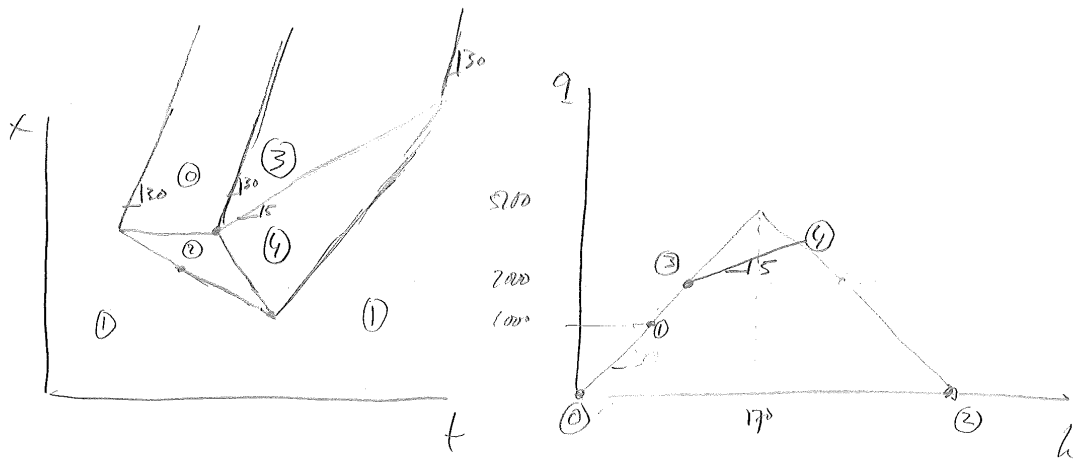
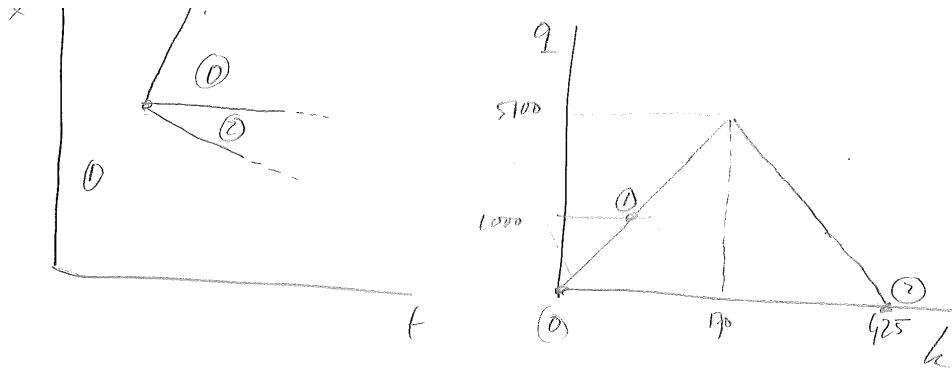
94 Drivers are expected to change lanes whenever it is beneficial for them (measured in terms of acceleration) (1). They do take the other drivers' benefit into account, but less than their own (at factor p) (1).

95 It can be expected that drivers take other drivers into account ($p>0$), but value their benefits less than their own ($p<1$).

96 No, it does not. The drivers are all at the left lanes. There is no more acceleration in the left lane, so the model does not give higher utility to the left lane.

97 Once the trucks come to a complete stop, upstream a congested area at jam density will be created (0.5); downstream, there will be an empty road (0.5). There are three shock waves. One with the free speed (30 km/h) separating the empty road with from the initial state (1). One at the location of the stopped trucks, separating the empty road from the jam state, at 0 km/h (1). Finally, there is a wave at the tail of the queue, propagating at a speed of $\Delta q/\Delta k=1000/((1000/30)-425)=-2.5$ km/h (upstream). (1 point)

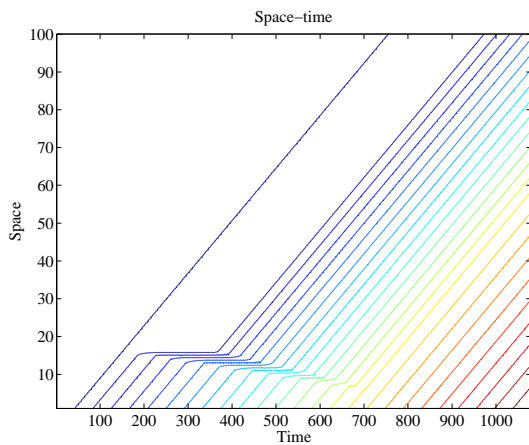
98 The start is the same as described in b. Then, at the head of the queue, vehicles are freed. The fastest vehicles, passing the moving bottleneck, will drive at a free flow speed of 30 km/h (1, including drawing in xt). The snow plows will form a moving bottleneck driving at 5 km/h (1, including drawing in xt). Downstream of this moving bottleneck there will be a free flow (0.5) traffic state with a flow of 2000 veh/h (given, 0.5) – this is state 3. The plows will form a moving bottleneck, and hence the separation of two traffic states, a congested upstream (state 4, unknown yet) and an uncongested downstream (state 3). (0.5 point). Plotting: 0.5 point. State 4 can be found by plotting the shock wave in the fundamental diagram, from state 3 upwards with a slope of 5 km/h (1). The shock wave speeds between 4 and 1, as well as between 3 and 1 can be found by the slope of the lines connecting these states in the FD (1).



99 The inflow is constant (constant raise of N at $x=4 - 1$ point), but the outflow is temporarily zero (no extra vehicles temporarily in the graph (1)). Hence, there is a temporal blocking (0.5) completely blocking the flow. (0.5)

100 The total delay can be derived from the area between the cumulative curves (1). In this case, we compare the cumulative curves where there is no delay (at $x=4\text{km}$) and that where the delay is maximum (near $x=25\text{ km}$) (1). The surface between the lines is (calculate: 1 point).

101 There is a temporal blocking, so the general pattern is as follows:



(1)

The head of the queue, and thus the location of the blocking is between location 16 and 20 (1). The tail is between km 8 and 12, since there is no delay (1)

102 The capacity is the derivative of cumulative curve during the outflow (0.5), here 2000 veh/h (0.5). The jam density can be derived from the number of vehicles between the cumulative curves in standstill: here 120 veh/km (480 veh in 4 km) (1). The slope of the congested branch can be determined by the speed at which the head of the queue (0.5) moves backward, e.g. at 16 km at $t=0.6$ and 12 km at $t=0.8$, i.e. 4 km in $0.2h = 20 \text{ km/h}$ (0.5). The critical density then is the jam density minus the capacity divided by the shock wave speed ($120-2000/20=120-100=20\text{veh/km} - 0.5 \text{ pt}$). The free speed then is the capacity divided by the critical density, i.e. $2000/20=100 \text{ km/h}$.

103 The limiting point for the flow is not the amount of space in the room, but the visitors watching the piece of art (1). Because then there are more visitors that can have a look at the art at the same time, because they do not stand crowded around a single object but have a large circumference to stand around (1).

104 I assume every visitor wants to be in the front row (1 point) for the assumed watching time of 30 seconds per person (10 s - 2 minutes: 1 point). Finally, I assume the width of a pedestrian to be 75 cm (50-110 cm: 1 point). The circumference of the show case is $2 \times 3 + 2 \times 1 = 8$ meter, which means $8/0.75 = 10 \frac{2}{3}$ visitors can stand at the circumference. (Both rounding to an integer number of visitors, as continuing with the real number is OK – arguing that the spots are not predefined, but dynamically filled). The capacity is 10 visitors per 30 seconds = 20 visitors per minute.(1)

105 When stepping on the moving walkway, visitors keep a gross distance headway of approximately 75 cm (50-110 cm: 1 point; net=gross-20cm); assume a single lane of visitors (for the best view) per walkway. The walkway moves with an assumed 0.5 m/s (0.2-1.5: 1 point). The flow is then $1/0.75 \times 0.5 = 2/3$ visitor per second = 40 visitors per minute. (0.5) Since there are walkways at both sides, the capacity is increased to 80 visitors per minute. (0.5)

106 The figure shows the size of the square approximately $500 \times 500 / 2 = 12,500$ square meters(0.5) The maximum density for pedestrians is approximately 5 ped/square meter (3-10: 0.5 pt). So, at times square at maximum 75,00 people can stand (0.5). The claim cannot be strictly right.(0.5)

107 Speeds in both lanes are equal(1). Alternatives with speeds etc: 0.5 points

108 Sketch showing the areas in more or less the right place (0.5), with appropriate names (0.5). Note that synchronized flow is an area (1)

109 There is no capacity(0.5), since there is a probability of breakdown from free flow to synchronised flow(0.5). This is an increasing function with flow. (Remarks on the area in synchronize flow: no points)

110 The coordinates move with the traffic, rather than that they are fixed at a certain location

111 No numerical diffusion, so more accurate results

112 Traffic is flowing from bottom because the congested patterns propagate in the opposite direction.

113 Bottleneck at km 14 (0.5), creating congestion and instability (1 point for this causality) leads to wide moving jams (0.5 for name)

114 Local: a change of speed of the vehicle cause oscillations with increasing amplitude in speeds with the direct follower (or not)

String: the amplitude of speed disturbances grows (or not) over a platoon,

Traffic: the disturbances within a platoon are propagated (or not) to the next platoon

(one point for the names, one point for the explanation)

115 The stability of traffic is one of the levels of above – we only need to consider that level. We see wide moving jams (or stop and go waves) emerging from an area of congestion, so traffic is unstable in the congested branch. (1) That means traffic is also platoon unstable. (1). Traffic is in general locally stable (only instable in simulations)

116 In the two pipe traffic state (0.5) traffic has different speeds in each lane / slugs and rabbits are separated (0.5); in one pipe traffic state (0.5) slugs and rabbits mix and the speeds are the same (0.5)

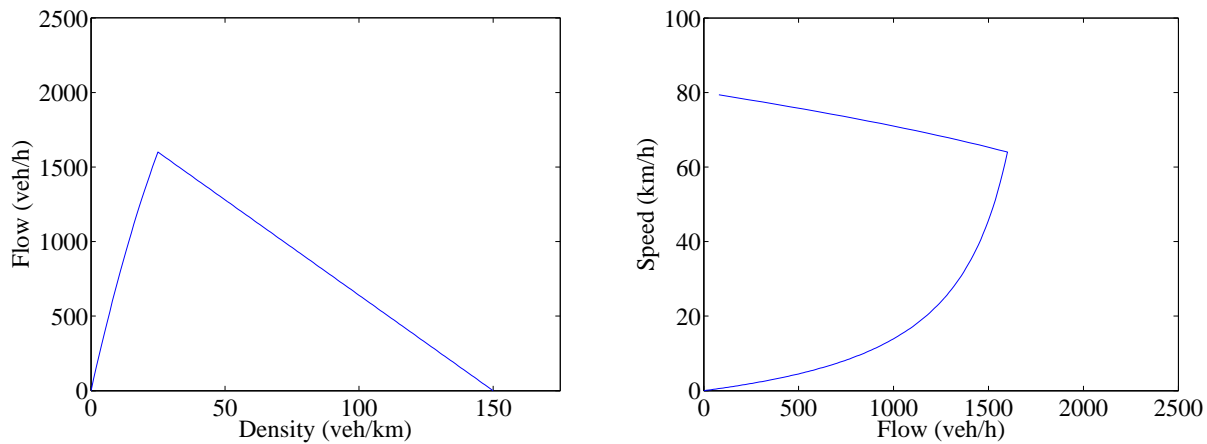
117 According to slugs and rabbits, the traffic is more present in the left lane (1), whereas for the Mobil lane change model there is a stronger tendency for drivers to take the right lane if there is no other vehicle.(1)

118 Stationary means that the traffic stream does not change over time (1). Homogeneous means that the traffic state does not change with space (the same at different locations) (1).

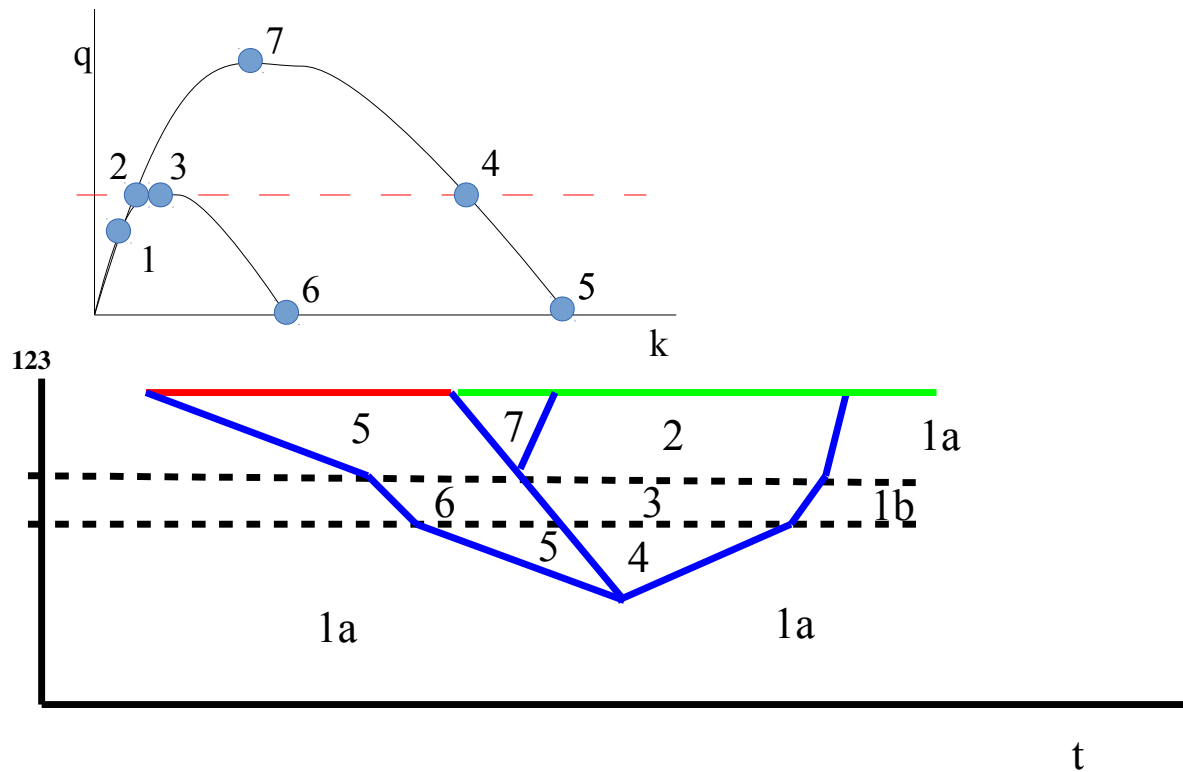
119 It cannot, since the FD gives the equilibrium conditions (1), and drivers have different ways to reach these equilibrium conditions. (1)

120 The right one is the triangular, since there is no influence of density in the speed in the free flow part

121 2 plots - for each one point. 1 point for the values

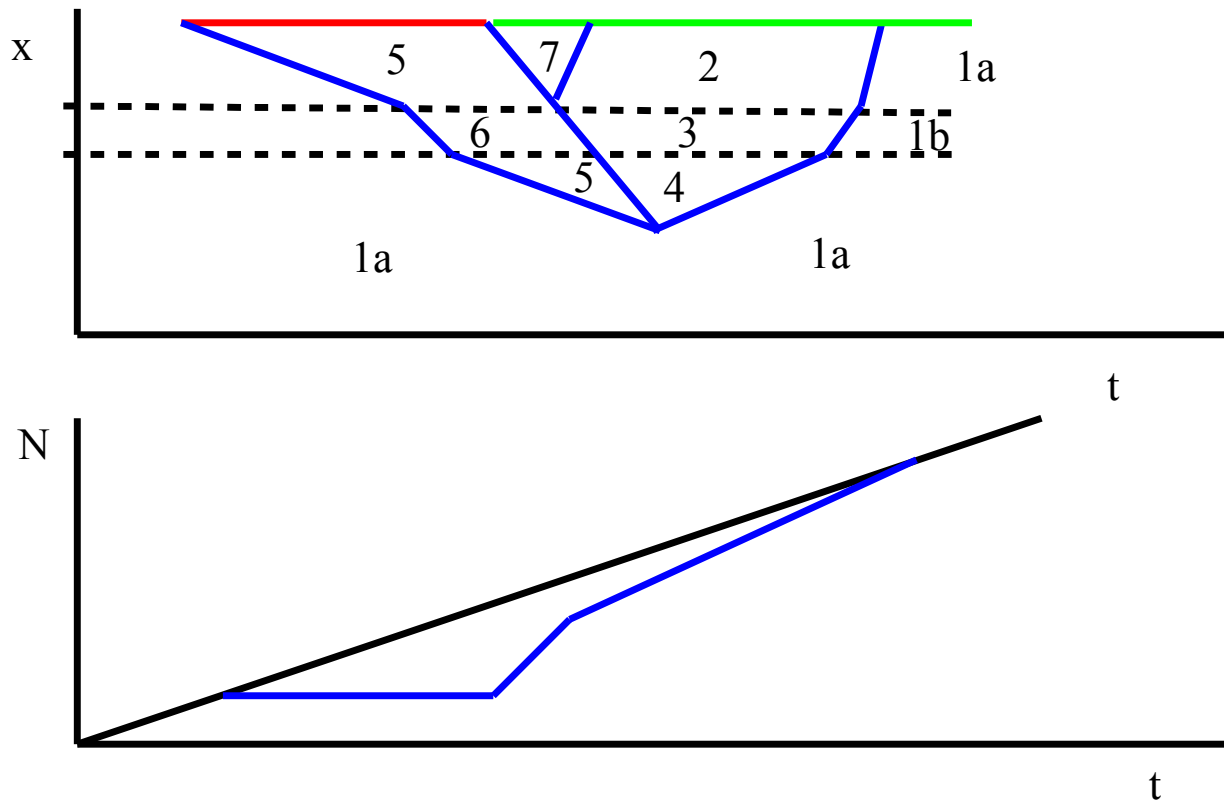


122 This is an urban area, so the free flow speed is around 50 km/h. (0.5). The jam density is hardly dependent on the conditions, so around 125 veh/km/lane (0.5) The capacity is a bit lower than in motorway conditions, at around 1200 veh/h/lane (1000-2000 veh/h/lane: 0.5 point). Draw this for a 4 and 1 lane part (0.5 point)



If during the green phase the queue completely dissipates, the inflow should be lower than the capacity for the one lane part (1). Starting with the traffic light in green/red: 1 point. During the red phase, the flow is zero, so we get jam density in the 3 lane part (0.5) and the 1 lane part (0.5). Once the traffic light turns green, there is capacity outflow (state 7 - 0.5 point). Once the backward shockwave reaches the part where the crane is, the flow in the part where the crane is, is now limited to the of one lane (0.5). In the downstream part, we now have the same flow in the free flow branch (0.5). A congested traffic state with the same flow occurs upstream of the crane area (1 point) (5.5 points for the traffic states). Now, connect all traffic states (2.5 points).

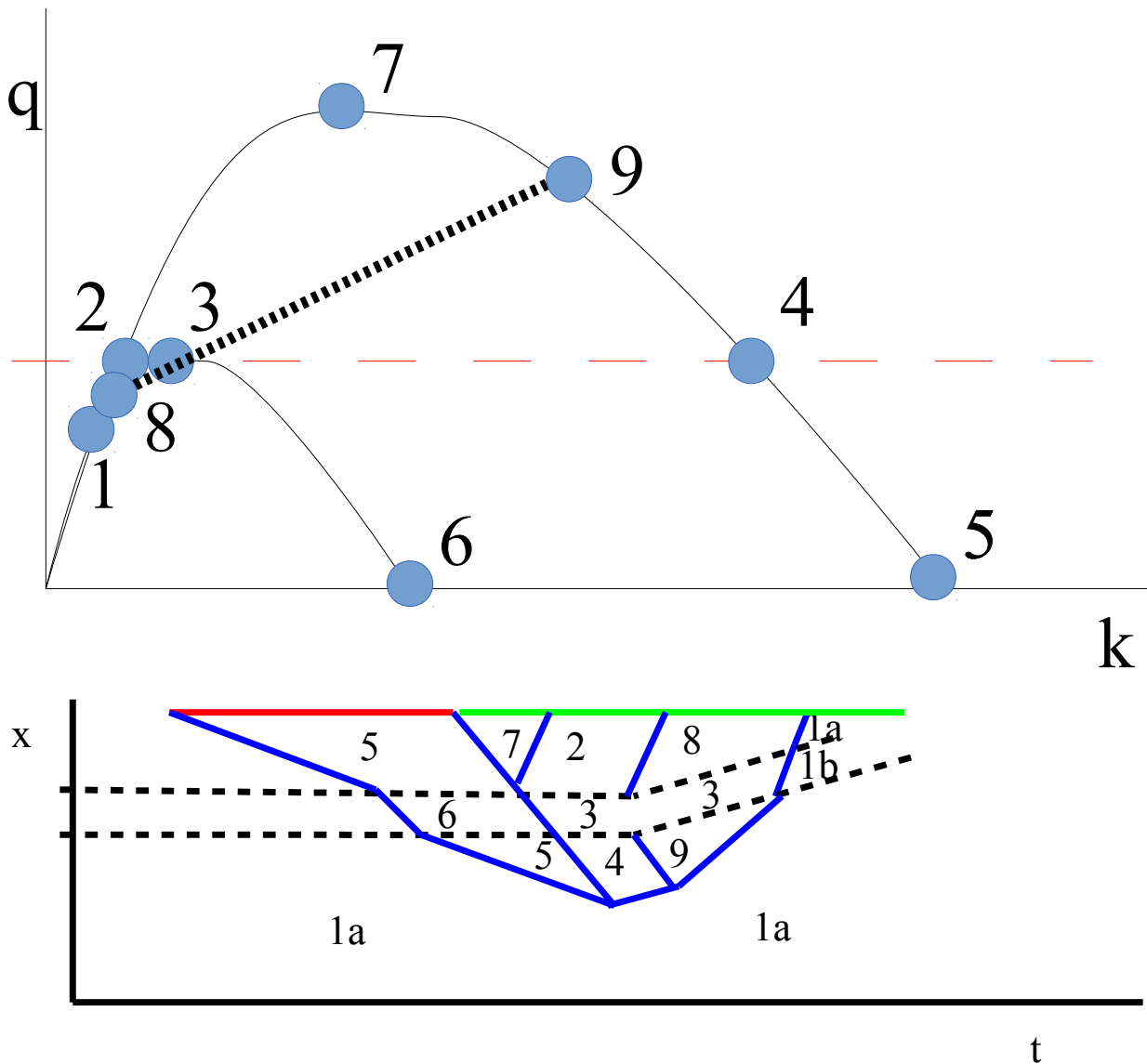
124 Upstream, the inflow is equal to the flow in 1 (0.5). Downstream, the flow is zero (during the red phase)(0.5), the flow of 7 (0.5), the flow of 2 and the flow of 1 once the queue has been dissolved. (0.5)



125 The delay is the area between the blue and the black line

126 If the crane is further from the intersection, state 7 lasts longer (1). Hence, the farther upstream the crane is, the longer the steep increase of the blue line (0.5) and the smaller the delay (0.5).

127 Still, the traffic operations next to the moving crane are at capacity conditions as long as there is a queue waiting. (0.5) Hence, we have point 3 (0.5). The crane forms a moving bottleneck and these are shocks which connect to the free flow and congested states on the fundamental diagram downstream and upstream (1 point for mentioning, 1 point for drawing correctly in FD). The remainder of the shocks can now be drawn (1 point for finishing)



128 The Network Fundamental Diagram describes the production (0.5) average flow (0.5) as function of the accumulation (0.5), i.e. the number of vehicles in a network (0.5). Also possible: the performance (0.5), i.e. the outflow (0.5), as function of the accumulation. Wrong combination of terms and meaning costs 1 point.

129 NFD plot with flattened top (top: 0,5 point).

130 The NFD goes up and down, just like the regular FD, but the top is flattened (1 pt, including graph). The flat top is caused by the fact that not all roads can be operating at capacity (1)

131 Once the roads get more congested, the blocking back causes the traffic to slow down.

132 See the course slides. If the inflow is limited, the production can be higher, and hence the outflow can be higher (1). Without control, the inflow into the protected network can be higher than the outflow out of the protected network(1), thereby steadily increasing the accumulation(1). The higher the accumulation, the lower the outflow, until finally a gridlock situation occurs.

133 A car-following model describes how the position, speed or acceleration of a follower depends on the movement of the leader

134 The relative amount of space (in time! -0.5 if not mentioned) that a non-passenger car vehicle occupies on the road

135 The road could handle 1 passenger car per unit of time (without loss of generality, choose time unit appropriately such that this is correct) or 0.5 truck (0.5 for this reasoning, or any other leading anywhere). Now, this would be 1.05 passenger car of $1.09 \cdot 0.5 = 0.545$ truck (1). To get the pce value, one has to divide the maximum truck flow over the passenger flow (1): $1.05 / 0.545 = 1.92$.

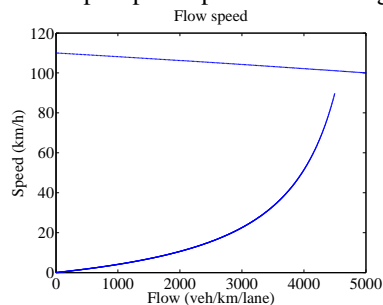
136 This means that the the solution is more exact; a platoon or stop-and-go wave will for instance spread in a Eulerian coordinate system, whereas this will stay together (resp the wave will remain sharp) in the Lagrangian coordinates.

137 Comfortable accelerations lie in the order of 1 m/s^2 , strong braking in the order of 6 m/s^2 . A threshold value to accelerate would hence be around 1 m/s^2 (0.3 to 2: 1 point)

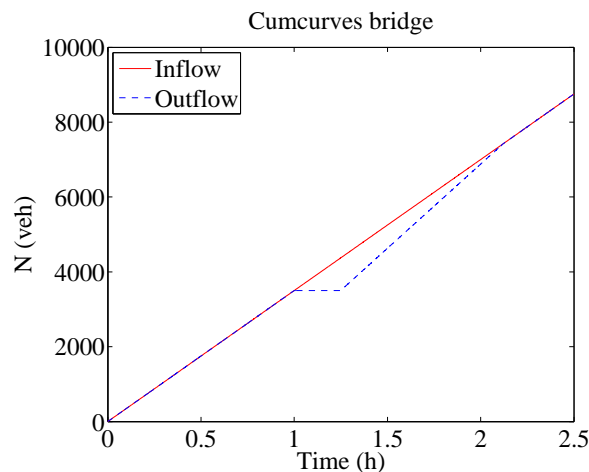
138 It is the politeness – how people value the acceleration of others. This can be assumed to be between irrelevant (value: 0) and just as important as themselves (value: 1)

139 Flow in ped/s/m (max: 0.6-2), density in ped/m² (max: 4-12 1 point) Base for instance the flow on a 1.5s headway per lane (similar to car traffic), leading to $1/1.5 = 0.67 \text{ ped/s/lane}$. In 1 meter, at 60cm width per ped, 1,67 fit next to each other (leading to 1 or two lanes). Being partly next to each other, the lane capacity is multiplied by 1.67: $\text{cap} = 0.97 \cdot 1.67 = 1.1 \text{ ped/m/s}$

140 Capdrop: 0.5 point. Decreasing speed): 0.5 point. General shape: 0.5



141 Free flow speed (100-120 km/h), critical speed(75-95 km/h), critical density(17-30 veh/km/lane), jam density (100-200 veh/km/lane). 1 point for the densities, 1 for the speeds. 1 point for matching numbers ($q=ku$) at capacity (free flow / critical)



142

143 In 15 minutes $3500/4=875$ vehicles arrive, which are in the queue. After the bridge opens, the queue length reduces (3500 veh/h in 4500 veh/h out)

144 See the cumulative curves. The total delay is the total area between the lines. (1) In this case, the congestion reduction phase lasts $875/(4500-3500)*60 = 52,5$ min, (1) so in total congestion lasts 67,5 minutes. (0.5). This is a triangle, which surface is being determined by the height times the width times divided by two. The surface then is $67,5 \text{ min} * 875 \text{ veh} / 2 / 60 (\text{min/hr}) = 492 \text{ veh h}$. (0.5)

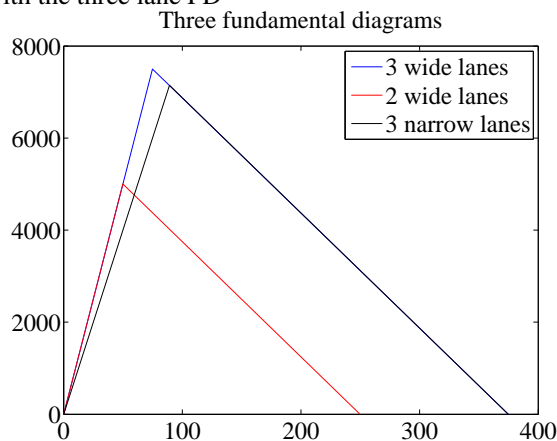
145 From one point different waves occur: a fast one to high speeds, and a backward moving one to lower speeds.

146 At the beginning there is no flow (the first vehicles need some time to arrive - 0.5) and it then gradually increases (0.5) to the capacity (1) which it will asymptotically reach (so no touching!) - 1.

147 This is downstream. The fastest wave travels at free flow speed (0.5). This is derived from the fundamental diagram (0.5). The Greenshields fundamental diagram is a parabola (0.5). To find the parameter (1 pt): the speed decreases linearly with the density. The capacity is found halfway the density range, so at 60 veh/km. The speed there can be determined by $v=q/k=5000/60=83 \text{ km/h}$. Since the speed-density relation is linear, the speed at $k=0$ is twice as high: $v_0=83*2=166 \text{ km/h}$ Other possibility: for the sake of calculation, flip the parabola to a form upside down, and move it to such that the top at (0,0) and increasing flow. The parameters are found by $a(60)^2 = 5000$ (0.5), so $a = 5000/3600 = 1.39 \text{ veh/h}/(\text{veh/km})^2 = 1.39 \text{ km}^2/\text{veh/h}$ (0.5). The speed is the derivative (0.5), i.e. $2ax$ at $x=60$. That means $v=2*1.39*60 = 167 \text{ km/h}$. (0.5) Note that it is unlikely that a wave will travel that fast in Dutch motorways. So the wave arrives at 200 m downstream $500/(167/3.6)=11$ seconds after the bridge closes.

Because this is a hard question, the final points are divided by 2.

148 For each of the FDs one point. Note the congested branch is uninfluenced for the congested part, so is overlapping with the three lane FD

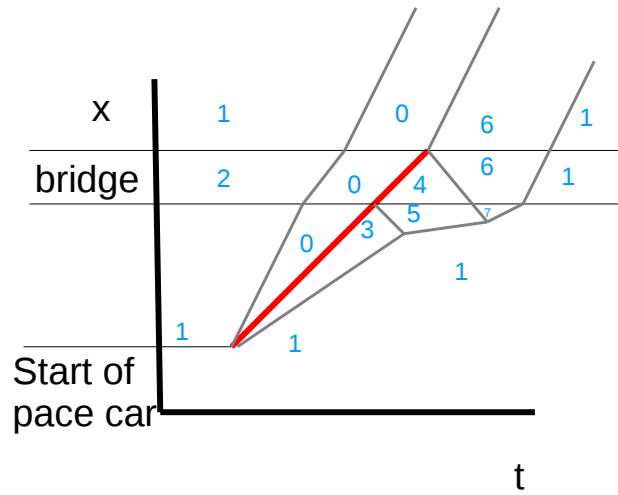
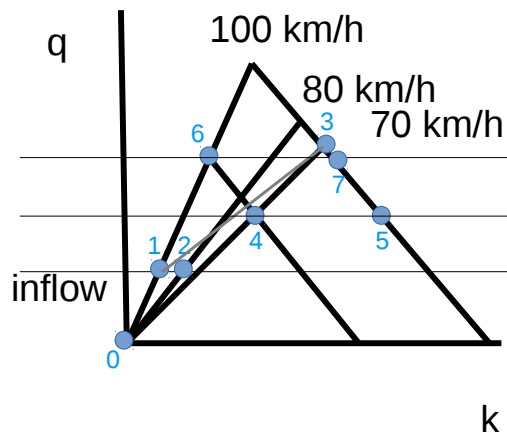


149 The question relates to: where do the free flow line for 80 kms/h and the congested line cross. (0.5) The free flow line is: $q=80k$ (0.5). The congested line is $q=100*25-25*(k-25)$. (0.5) Setting q equal gives $kc=29.8 \text{ veh/km/lane}$ and $q=2381 \text{ veh/h/lane}$. (0.5) For three lanes this gives 7129 veh/h. (0.5)

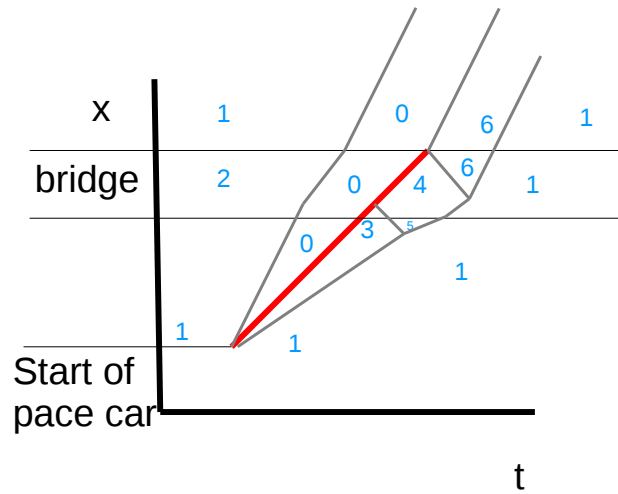
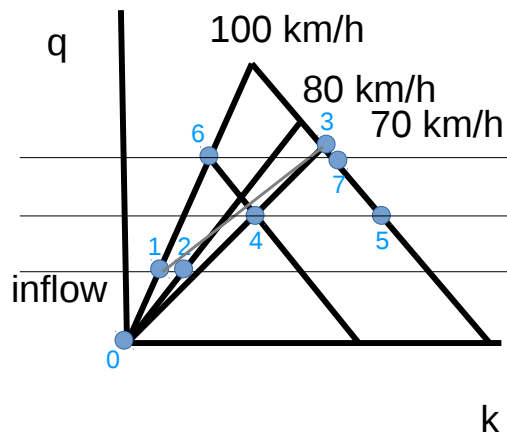
150 In busy conditions, the increased capacity causes less queuing, and hence a lower travel time (0.5). In free flow conditions, the higher speed causes lower travel times. (0.5)

151 The last vehicle downstream of the pace car needs to travel 1000 meters, where the pace car travels 700 meters. Upstream, the traffic has a speed of 100 km/h (0.5), so the time is $1000/(100/3.6)=10*3.6=36$ seconds (0.5). The pace car hence has to drive 700 meter in 36 seconds (0.5), hence the speed is $700/36 * 3.6 = 70 \text{ km/h}$. (0.5) (the factor 3.6 is for unit conversion to km/h.

152 Traffic is in free flow conditions (0.5), at a flow of 3000 veh/h (0.5), giving a state in high speeds (state 1) (0.5) and at 80 km/h in the narrow lane section (state 2) (0.5 – lower speeds). At a certain moment, the pace car enters, driving at 70 km/h leaving a gap in front (state 0) (0.5) Upstream there will be a congested state at the fundamental diagram for three wide lanes (0.5) at 70 km/h (0.5) (state 3). The capacity for the two lane part at 70 km/h (the pace car still determines the speed) is point 4 (0.5). This is lower than the local demand, state 3. Hence, there will a congested state upstream (state 5 - 1 pt) with the same flow as the congested state in the two lane section. Once the pace car leaves the road, a flow equal to the capacity of the two lane section exits the congested state 4. The head of this tail is moving backward (just like a head of a queue once the traffic light turns green). Downstream in the 3 lane section, the same flow (capacity flow of the two lane section) is found. Then, two possibilities arise (based on your sketch – no need for exact computation): (1) backward wave gets to the end of the bridge before the forward bridge reaches it. Then, in the three lane section a congested state with the same flow as the capacity in the two lane section is arises. Possibility (2) is that the forward wave is earlier, and in that case the congestion solves from the tail. Drawing the space time diagram: 2 points: (cumulative: 9.5, divide points by 1.5 because it is a hard question)



Solution 1: backward wave gets to the end of the bridge before the forward bridge reaches it

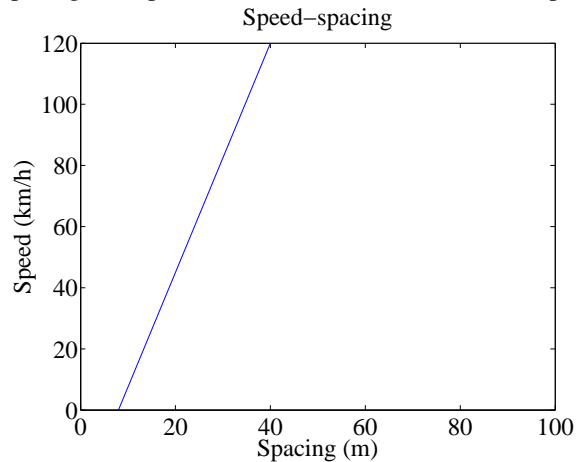


Solution 2: backward wave gets to the end of the bridge after the forward bridge reaches it

153 Synchronized flow

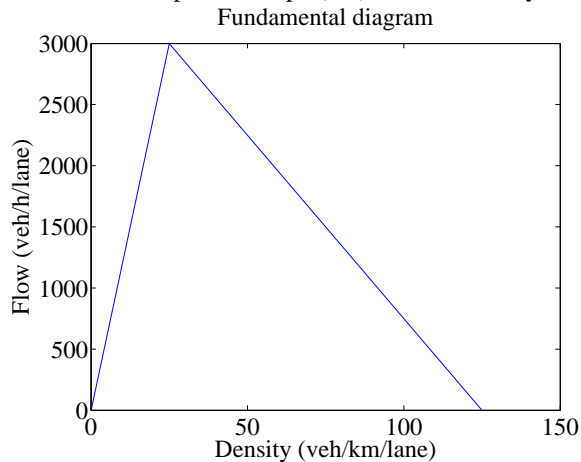
154 Wiedeman states that drivers will not react to minor speed differences if they are below a certain threshold (1). That is similar to the synchronize flow area (0.5) which states that drivers are willing to accept various time headways at different speeds (0.5)

155 Speed increases with increasing spacing (0.5). No values for smaller spacings than a critical value, and for higher spacings the speed is constant (0.5) (at the desired speed).



(1 for graph)

156 Free flow speed is slope (0.5), critical density is 1/critical spacing (0.5), jam density = 1/min spacing. (0.5)

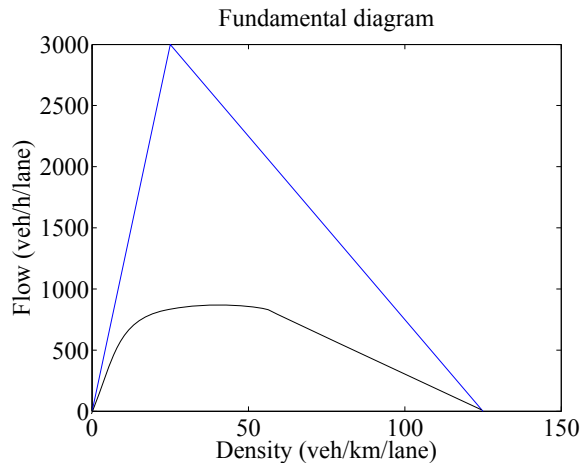


A piecewise linear speed-spacing diagram leads to a triangular fundamental diagram (0.5 – not asked in wording, but a wrong shape will get a reduction in points).

157 Production

158 Accumulation

159 (it is lower and it has a flattened top. (1) Plotting: (1). The right part is mainly theoretical, since one cannot reach that state (not needed for points).



Good reasoning as well: in a network, the speeds are lower, so the overall NFD is lower.

160 The controlled intersection causes headways to be more spread (1). In this case, the negative binomial (1) function is a good way to describe arrivals.

161 If the platoon is stable, it means traffic disturbances damp out within the platoon (1). That means that they cannot grow from platoon to platoon, which is the definition for traffic instability (1)

162 $N(x,t)$ indicates how many vehicles have passed location x at time t

163 With calibration, one finds the best parameter settings for a model (1), whereas in validation, one checks how good this (optimized) model works for another situation (1)

164 An MFD indicates the relation between the outflow out of (or internal flows in) *an area* to the number of vehicles in that area

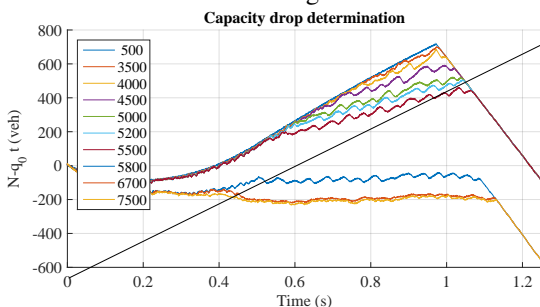
165 Capacity is given in ped/m/s

166 The capacity indicates the number of pedestrians per unit of time per unit of width.

167 (1) One has to estimate the number of vehicles in the road section at the start, (2) there is a increasing error from miscounts (3 – less of an issue) one does not have observations from the vehicles leaving or entering the road section (one has not here in this case either – therefore 0.5 point)

168 The queue starts at the bottleneck, since there is delay between $x=6700$ and $x=5800$ (there is a distance between the moved slanted cumulative curves of 6700 and 5800) (1). The delay spills back to approximately 3500m (there is still a little delay between 3500 and 4000m) (1). The congestion solves by a lower demand, seen from the demand curve (only that: 0.5 pt) and the fact that the delay at the more upstream locations solves earlier (add that: 0.5).

169 The most accurate reading is from the slanted curves.



Before congestion it has a slope of approximately $(650 - 400)/(1.2 - 0.2) = 1050$ veh/h (1). This should be added to the offset to get the flow (0.5): $1050 + 3900 = 5050$ veh/h (0.5) – reading from the non slanted curves 1 pt. Reading the maximum flow from the highest value on the three lane section: 0.5 point (it is a flow, but not related to the capacity)

170 The difference between the flow before congestion sets in and after it has set in is the capacity drop (1). After congestion has set in, the slope is approximately 0 (0.5) (or equalling a flow of 3900 veh/h). The flow 1050 veh/h lower than before congestion, which is the value for the capacity drop (0.5)

171 Yes, the delay would differ since the delay of the vehicles leaving at the offramp would not be taken into account (1). Hence, the delay computed with a vertical queuing model would be less (1)

172 The partial densities can be calculated by $k = q/v$ per class (1), leading to $k_1 = 500/120 = 4.2$ veh/km and $k_2 = 500/90 = 5.6$ veh/km (1). The total density is the sum of these two (0.5), 9.7 veh/km (0.5)

173 For the space mean speed, one can (a) average the paces or (b) Put weight on the speed values the speeds using the densities (either method: 1 point). (a) The result is $1/((1/90 + 1/120)/2)$ (0.5) = 102.8 km/h (0.5) (b) The result is $4.2 * 120 + 5.6 * 90 / (4.2 + 5.6)$ (0.5 point) = 102.8 km/h

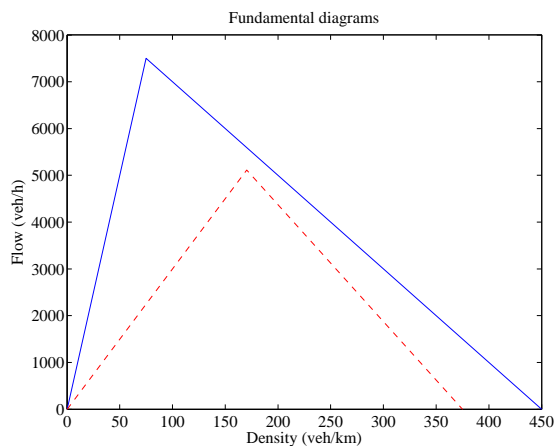
174 (i) For the time mean speed, one observes as many slow as fast vehicles (equal flows). (1) Hence, the mean speed is $(90 + 120)/2$ (0.5 pt) = 105 km/h (0.5 pt). If b is the correct answer to c and c the correct answer to b: 1 point total.

175 $k_{\text{Edie}} = \frac{\text{Total time spent}}{\text{Area in space-time}}$ (1 point)

176 Use the equation $q_{\text{rel}} = k_{\text{fast}} * v_{\text{rel}}$ (1). $k_{\text{fast}} = 4.2$ veh/km (0.5) and $v_{\text{rel}} = 120 - 60 = 60$ km/h (1). Therefore, $q_{\text{rel}} = 4.2 * 60 = 250$ veh/h

177 Calculate – in the same way as above – the flow of the slow moving vehicles: $q_{\text{slow}} = 5.6 * 20 = 113$ veh/h (2). Now, average the speeds: $v_{\text{mean}} = (q_{\text{slow}} * 80 + q_{\text{fast}} * 120) / (q_{\text{fast}} + q_{\text{slow}})$ (1 point) = 107.6 (0.5)

178 The flows passing a fixed observer are equal, and relative speed difference with the fast vehicles is larger. (1) Hence, using $q_{\text{rel}} = k * v_{\text{rel}}$, the flow of the fast vehicles becomes relative larger (1).



179
1 point for each line

180 1 since the capacities of both vehicle classes are equal

181 Newell's car-following model is described by the equation

$$x_i(t) = x_{i-1}(t - \tau) - s_{\text{jam}} \quad (\text{B.12})$$

(1 point) τ can be found as $1/\text{capacity}$ (1) $1/2000$ (h), or $3600/2000 = 1.8$ s (0.5). s_{jam} can be found as $1/\text{jam density}$ (1), or $1/125$ (/km), or $1000/125 = 8$ m (0.5)

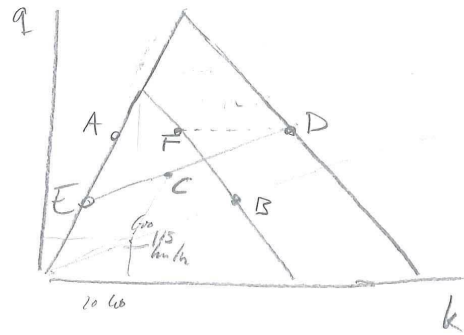
182 Slugs and Rabbits

183 Synchronised flow

184 Answer left to students

185 Only the two lane part is relevant here, so draw that fundamental diagram (1 point for the FD with the correct axes (per roadway, rather than lane). The initial conditions (A) can be indicated in the FD (0.5). Now, the traffic upstream of the truck is driving at 15 km/h (0.5), hence we get a congested state at the line $q=15 \cdot k$, leading to B (0.5 point). The trajectory of the truck can be put in x_t , driving at 15 km/h (1 point). The congested state B spills backwards with a speed of which the slope equals the slope of A-B in the fundamental diagram (1 point). Downstream of the truck, there is an empty road (0.5) and the matching shockwave between that and state A (0.5)

186 Draw the fundamental diagrams (1 point), and the capacity point C (0.5). The truck forms a bottleneck, and hence moving at 15 km/h, (0.5) through point C, there is a line with a slope of 15 km/h (0.5), connecting downstream point E (0.5) and upstream point D (0.5). Shockwaves O-E (0.5) and ED (0.5) can now be drawn. In the two lane section, state is at the two-lane fundamental diagram: a congested state at the same flow of D – point F (1 point). Shock wave BF at the speed of the line BF in the FD (0.5 point).



187 Exponential

188 Binomial distribution

189

$$f_i = \frac{q_i}{q} = \frac{q_i}{\sum_{\text{all lanes}} q_i} = \frac{1/\langle h_i \rangle}{\sum_{\text{all lanes}} 1/\langle h_i \rangle} \quad (\text{B.13})$$

(The step at each equal sign is 1 point)

190 Passenger car equivalent

191 The demands are equal, hence the flows of slugs and rabbits are equal (0.5). They are separated in free flow conditions (1), so the flow in both lanes is equal (0.5)

192 If a platoon is unstable (0.5) a small disturbance can grow over the platoon (0.5). If the disturbance also grows beyond the platoon into the next platoon (0.5) this is called platoon instability (0.5). A small disturbance hence can grow until vehicles come to a complete stop (0.5).

193 Breakdowns occur stochastically, and with a higher flow, the probability of a breakdown is higher. Then, there is not a single value for capacity.

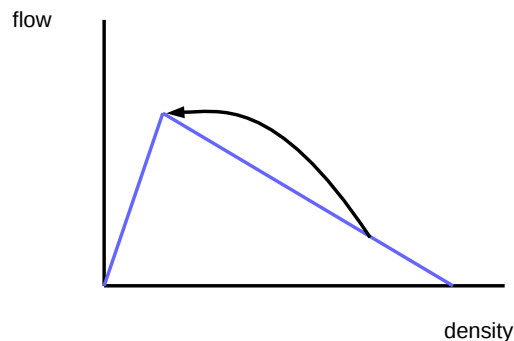
194 It means that the predicted traffic states are not exact; shock waves get spread out over space if time progresses (1)

195 Traffic must be stationary and homogeneous

196 Traffic characteristics move with the slope of the fundamental diagram. (1 pt, word characteristics not needed) Simplifying to a triangular fundamental diagram, they move either forward with the free flow speed or backward with the wave speed. A parallelogram with slopes free speed and wave speeds (1) aggregates hence a more homogeneous traffic states.

197 Edie's (generalised) definitions

198 Due to this multi-anticipation, drivers will accelerate earlier out of the congested state (1) (even before the density will go down as much as usual – i.e., the FD). Hence, the speed and thus the flow go up faster than normal (1). The end situation (capacity) is the same(1). We hence get a transition line above the congested branch (1: sketch).



199 The flow through the bottleneck is equal to the flow in the jam (1). This is found by $q=ku$ (1). $k=1000/11*3=273$ (0.5 + 0.5 for the *3 part) and $u=8$ (0.5). Hence, $q=273*8=2182$ veh/h (0.5)

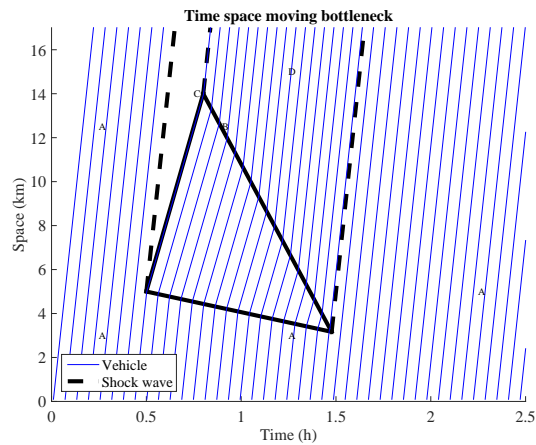
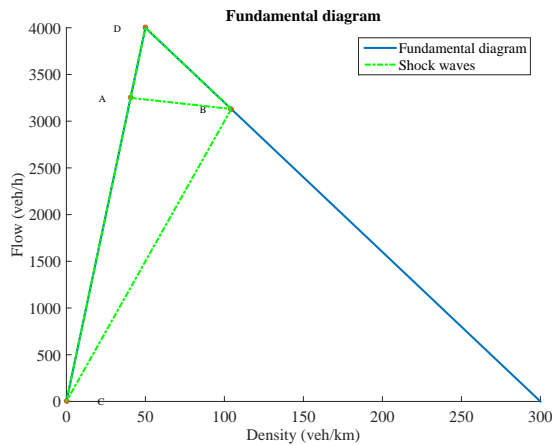
200 The capacity point for the three lane part is three times the capacity of the one lane part (0.5), which is the flow through the bottleneck (0.5). So the capacity is $3*2182=6545$ veh/h (0.5). The critical density is hence $6545/c_{\text{free}}=65$ veh/km (1). The wave speed can be found by realising the point $q=2182$ and $k=272$ lied on the FD (0.5). Now, the jam density can be found in various ways. For instance: the wave speed is dq/dk , with $dq=-(6545-2182)=-4364$ and $dk=272-65=207$ $w=-21$ km/h. $k_j=k_c+C/w=67+3*2182/21=375$ veh/km (1)

201 This question relates to the flow in the two lane section in a congested state (0.5) for a flow of 2182 (0.5). The density is exactly between the critical density ($2/3 \cdot 65 = 44$ veh/km) and the jam density ($2/3 \cdot 375 = 250$ veh/km), so at $294/2 = 150 - 3 = 147$ veh/km. (1) The speed then is $u = q/k = 2182/147 = 15$ km/h (1).

202 Since the traffic state is stationary, the shock waves must have slope zero, so the flows must be equal. (1)

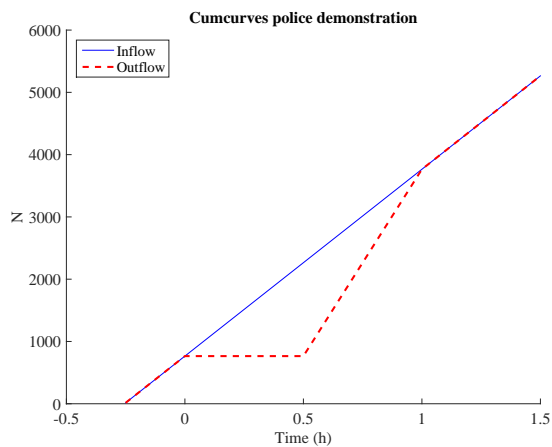
203 For all stationary states, the flow is the same for all locations. Hence, the average flow is the same as the outflow. (1) This increases as in the FD up to the critical density, and then remains at that maximum (1).

204 Sketch the FD (1). Draw a line with slope - speed - 30 km/h from the origin (0.5). This is the line where the congested state must lie, i.e. at the intersection of this line and the FD – indicate in FD (1). The original traffic situation is at a demand level higher than this flow (given) at the free flow branch (0.5). After the police cars speed up, the state returns to capacity (1). Indicate the connections in the FD (1) and in space-time (1)



205 Calculate the intersection point of the line with slope v_0 and the FD (1) Description of the congested FD: $q = C - C \cdot (k - k_c) / (k_j - k_c)$ (1). Fill in values, and solve:
 $C - C \cdot (k - k_c) / (k_j - k_c) = v_0 k$
 $k = 104$ veh/km (1) $q = v_0 k$ (0.5) $= 30 \cdot 104 = 3130$ veh/h (0.5)

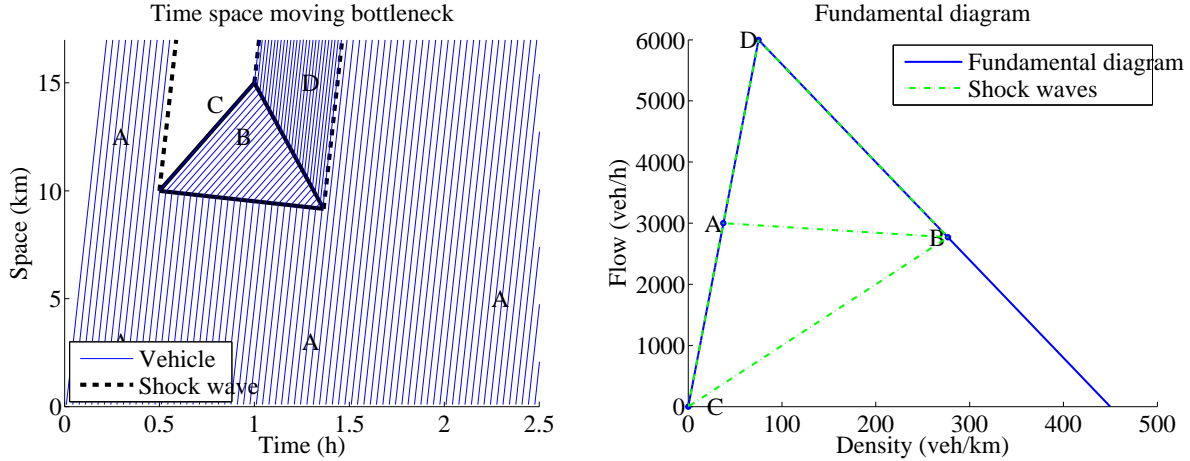
206 Inflow is constant (0.5), so a straight line with slope of demand (0.5). Outflow is equal to the inflow until the moment that the police cars enter (0.5). From that moment in time, the outflow hence slope is 0 (1). After they leave, the flow is the capacity (not asked), so steeper outflow (0.5), up to the moment they are at the same vehicle level (0.5), after which they are at the same line (0.5)



207 The delay is given by the area between the two lines in the graph above (1). The max nr of vehicles in the queue (N_{\max}) is $d * q_{in}$. The time to solve is then $t_{\text{solve}} = N_{\max} / (C - q_{in}) = d * q_{in} / (C - q_{in})$ (1). The area is $1/2 * N_{\max} * (d + t_{\text{solve}})$ (0.5). Replacing the terms gives $D = d * q_{in} * (d + d * q_{in} / (C - q_{in}))$. Further simplification (proof) leads to

208 The delay approaches infinity if the demand approaches the capacity. (1). That is because the jam will never solve if the demand is equal to the outflow (1), and all following vehicles will get a delay (1).

209 This is basically the same as the question b, with the difference that the demand is above the congested flow on the free flow branch of the FD (0.5). The segment connecting this point to the congested traffic state hence goes down (0.5), and this means the tail of the queue moves back (0.5). In graphs:



210 It does – it is based on the flows and the gaps, and they remain the same.

211 See the cumulative curves: the area is the delay (no points - awarded earlier). This increases proportional with both the number of vehicles in the queue, as well as with the delay for the first vehicle (1), which are both proportional to the duration of the demonstration (1), so in total that means a quadratic relationship (1)

212 Expected headway: 5 seconds. (1). Flow per lane: $3600/5$ peds/h. (1) Flow total: $3600/5 * 2 = 1440$ ped/h. (1)

213 In total the number of cyclists is the area under the graph (1), calculated by $\int_0^t 2 \text{ points } q(t) dt$, by geometry, leading to: $2 \text{ (min)} * q_0 * 1/2 = q_0$ [cyclist/min] (1). This equals 300 cyclists (0.5). Therefore, $q_0 = 300$ cyclist/min

214 The queue grows as long as q is larger than C (0.5), hence we need to find the number of cyclists that have passed at the moment q reduces to a value lower than C (0.5). It is $(1 - (C/q_0))$ minutes (0.5) after the peak of the flow (0.5) at one minute, so $t_E = (1 - (C/q_0)) + 1 = 2 - C/q_0$. The amount of cyclist which then have passed is $N_E = \int_0^{t_E} q(t) dt$, (1) which equals (or from geometry)

$$N_E = 1/2 * q_0 + (t_E - 1) * C + 1/2 * (t_E - 1) * (q_0 - C) \quad (\text{B.14})$$

$$= 1/2 * q_0 + (1 - C/q_0) * C + 1/2 * (1 - C/q_0) * (q_0 - C) \quad (\text{B.15})$$

$$= 1/2 * q_0 + (1 - C/q_0)(C + 1/2(q_0 - C)) \quad (\text{B.16})$$

(1)

215 Production

216 Yes, we can. The critical density for the Greenshields fundamental diagram is halfway the density range (0.5), hence at 50 veh/km (0.5). The speed at that density is half the free flow speed (linear relationship, 0.5 pt), being 40 km/h (0.5 pt). The capacity hence is $q = ku$ (0.5 pt) = $40 * 50 = 2000$ veh/h (0.5 pt)

217 An acceleration fan occurs at the head of a jam. Since characteristics of the lowest density move fastest, and characteristics of highest density move slowest, the sharp shock at the head of the queue (1) will spread out (1).

218 The density should be derived from the quotient of the flow and the space mean speed (1). The time mean speed overestimates the space mean speed (1), hence the density is underestimated (1)

219 Locally stable traffic means a vehicle will reduce the amplitude of its speed variation over time; from vehicle to vehicle, the amplitude can still grow, so platoons can be unstable.

220 In a stochastic simulation package (1 point), the traffic situation is depending on a random draw. You should do multiple simulations to check to which extent the results depend on the random draw.

221 FD holds in equilibrium, hence Δv equals 0, and a equals zero. This means (first equation) that $s = s^*$. (1). The second equation gives a relation between speed and density. We can rewrite this to

$$v = (s - x_0)/T \quad (\text{B.17})$$

(1 pt) Now substituting $s=1/k$ gives:

$$v = (1/k - x_0)/T \quad (\text{B.18})$$

(1 pt) Multiplying both sides with k gives the relation $q=q(k)$

$$vk = q = k(1/k - x_0)/T = 1/T - kx_0/T \quad (\text{B.19})$$

(1 pt)

222 After validation, it is known to which extent the model can be applied in other conditions and what its quality is

223 Since in the congested branch (equation above) q decreases with k , the capacity is found at the intersection of the congested branch and the free flow speed. We hence have to solve

$$v = q/k = k(1/k - x_0)/T/k = v_f = (1/k - x_0)/T \quad (\text{B.20})$$

(1) Solving this to k gives

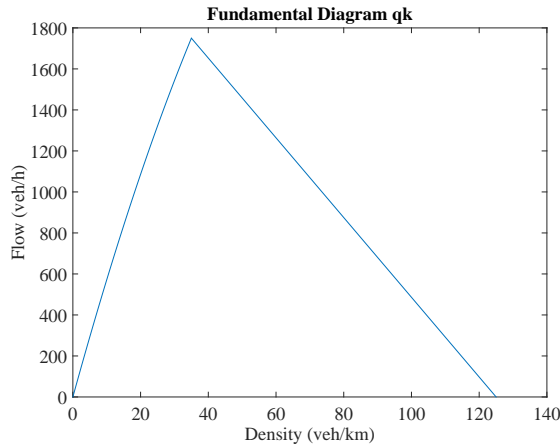
$$k = 1/(Tv_f + x_0) \quad (\text{B.21})$$

(1) Using the parameters, we find $k=1/(1*30+20)=1/50$ veh/m. (0.5) Computing q from this gives $q=kv=1/50 * 30 = 30/50 = 3/5$ veh/s (1) = 2160 veh/h (0.5)

224 Consider the FD in speed-density. Its form does not change, only the distance changes hence the values at the density axis are halved (0.5 pt). Moreover, the speed reduces to half, hence the values on the speed axis are also halved (0.5 pt). The effect on capacity is that the product of density and speed (1 point) is half times half = 1 quarter of the original capacity (1 point). The capacity is hence $2160/4=1080/2=540$ veh/h

225 Smulders fundamental diagram

226 Capacity is at the point where the congested branch starts (0.5); reading out the graph gives 35 veh/km and 50 km/h (0.5), so a capacity of ($q=ku$, 0.5 point), $35*50 = 1750$ veh/h



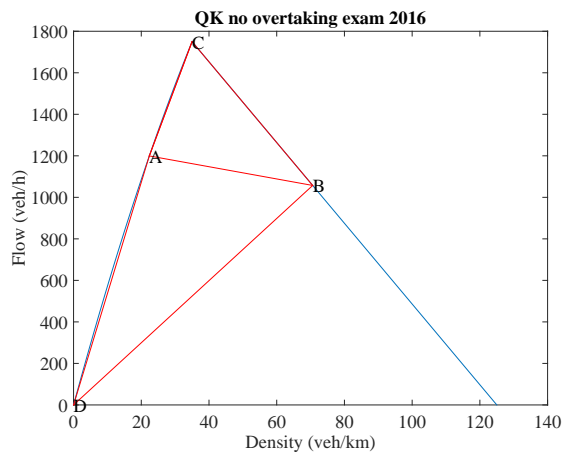
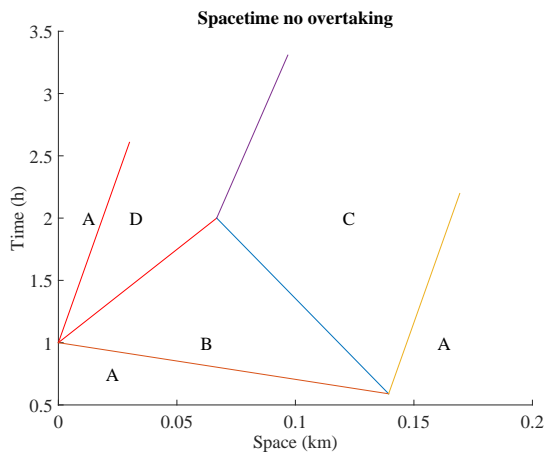
227

There is a slight curvature in the free flow branch, and a straight congested branch

228 This is the traffic state at 15 km/h (0.5), for which the FDs can be used (0.5). Hence, read out the FD at 15 km/h (0.5), yielding a density of approximately 70,5 veh/km (0.5). Using $q=ku$ (0.5), this gives a flow of approximately 1060 veh/h

229 First, find the traffic state upstream of the moving bottleneck, which is found by constructing the intersection point of the line $q=15k$ and the fundamental diagram (1 point, point B). Downstream of the MB is an empty road (state D, 1 point). Inflow point is at the free flow branch (0.5 point), and after the MB leaves the road, the state is at capacity (1 point).

Constructing the space time: start with the MB (1 point), construct AB, AC and CB (1 point), finishing 0.5 point.



230 A driver will change lanes whenever the utility for changing lanes is higher than staying in the current lane (1). The utility consists of the accelerations (no points, mentioned), for the driver itself and for the vehicles directly influenced (n and o) (1), where the latter two are discounted using a politeness factor \mathcal{P} (1)

231 The values are accelerations so should be given in m/s^2 (1 point). a_{bias} should be higher than a_{th} , otherwise no lane change to the right. Accelerations in the order of 1 m/s^2 are sizeable (i.e., quite some throttle opening), so values should be in the order of one tenth of that. Values between 0.01 and 1 are given 1 point (Treiber and Kesting propose 0.3 and 0.1 m/s^2 for a_{bias} and a_{th} respectively.)

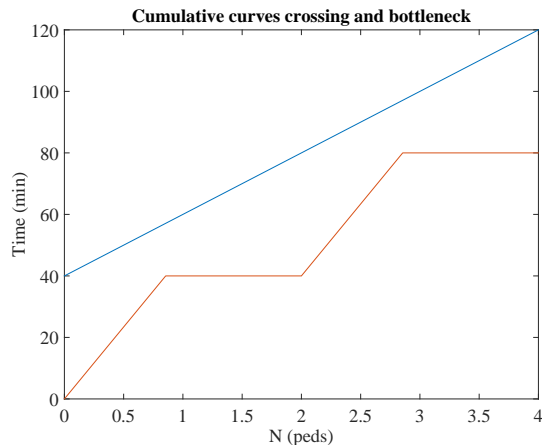
232 Poisson

233 $1200 \text{ peds/h} = 1200/60 \text{ peds/min} = 20 \text{ peds/min}$. In 120 seconds = 2 mins $2 \cdot 20 = 40$ peds arrive (and cross) (1 point for flow times cycle time, 0.5 point for unit conversions, 0.5 point for end answer)

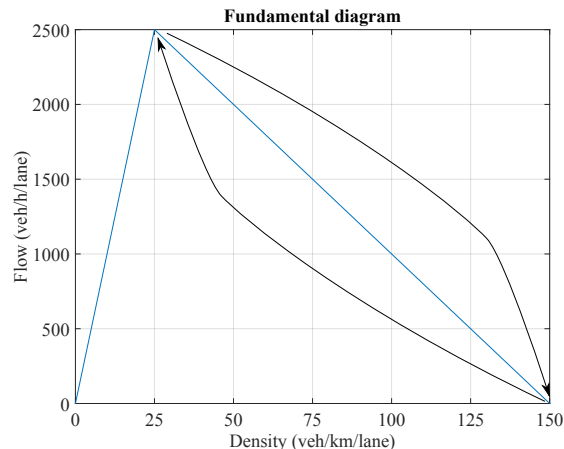
234 Flow in peds/m/s and density in peds/m² (1 point for each)

235 The capacity (read from graph) is 1.22 peds/m/s (1 point for using the capacity value), so the capacity for the bottleneck is $0.6 \times 1.22 = 0.732$ peds/s. (1). It will hence take $40 \text{ peds} / 0.732 \text{ peds/s} (0.5) = 54$ seconds (0.5) to pass the bottleneck.

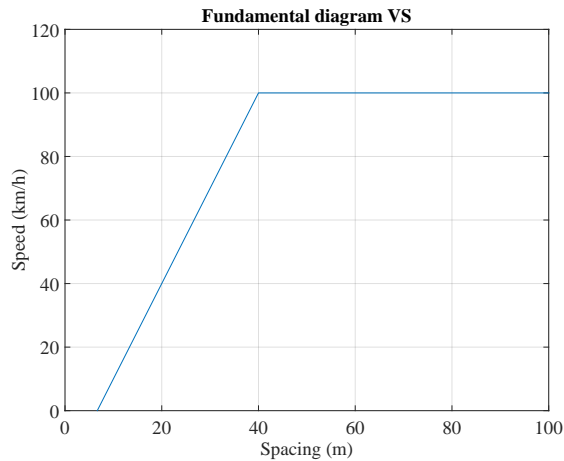
236 Starting with the hint: at the start, 40 pedestrians have crossed A and not B (see question b). (0.5) So start the curves with 40 pedestrians difference (0.5). Then, the inflow steadily increases with 1200 peds/h, or 40 peds/cycle (1). For the outflow, the queue discharges at 0.732 peds/s up to the moment that 40 pedestrians have exited, and remains constant then (1). (Indeed, by that time other pedestrians are waiting at the traffic light again, so the lines do not touch.



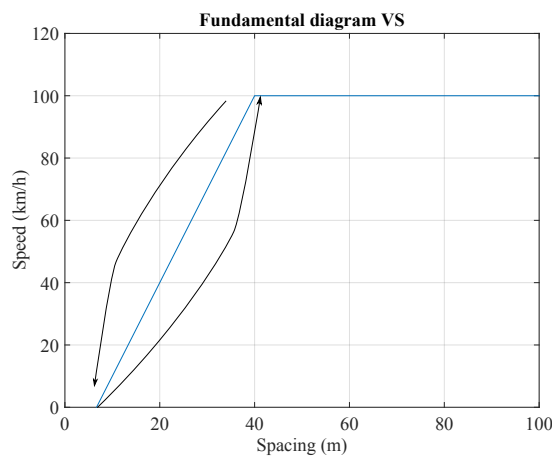
237 Consider for instance an acceleration from low speeds to high speeds. Traffic starts right bottom, and then the density decreases. However, since the speed of the vehicle is not adapted, it is still low, so it curves counter-clockwise to the top. (1) The other way round, under deceleration, consider a point near the top. Then, first the density increases (traffic state moves to the right), and the speed is still higher than for the newly increased density. Hence, the traffic state moves counter-clockwise down. (0.5 for a second reasoning)



238 Triangular, so the free flow speed is fixed (at $2500/25=100$ km/h). Straight line in congested branch means q and k are linear, say form $q=1/r-wk$. Divide both sides by k , and use substitution $s=1/k$: $q/k=v=1/k \cdot 1/r-w = 1/r \cdot s - w$, so also v and s are linear. From the fundamental diagram, find $1/r=3000$ veh/h (point where the congested line would intersect the y-axis) and $w=2500/125=20$ km/h. (Also accepted: triangular fundamental diagram in qk leads to a piecewise linear fundamental diagram in vs , with $s_{\min}=1/k_{\text{jam}}$, $s_{\text{crit}}=1/k_{\text{crit}}$ and $v_{\max}=q_{\text{crit}}/k_{\text{crit}}$). Plotting the minimum of congested speed and free flow speed gives:



(1pt)



239

240 Poisson distribution

241 Every truck counts for two vehicles in determining the capacity.

242 If we relate it to time headways (1) of a passenger car without queue warning systems, we get for cars a $pce = 1/1.05$ and for trucks $2/1.09$. (1). The new pce value is the ratio of the two (0.5): $2/1.09 / (1/1.05) = 1.05/1.09 * 2 = 1.92$ (0.5)

243 It means that the edge of a traffic jam flattens (contrary to predicted with shockwave theory)(1)

244 It means that after a braking manoeuvre of a leader, a follower will not find the same speed, but keeps continuing adjusting speed (0.5) in an increasing amplitude, i.e. going to higher and lower speed for every iteration (0.5).

245 Yes, if the inflow is equal to the flow in the queue behind the moving bottleneck, the tail remains stationary

246 This is not possible. For Greenshields, the critical density is half the jam density (1). Since this is not the case here, we cannot draw. (1)

A linear FD in VK is awarded 1/2 point.

247 Stop-and-go waves travel in the opposite direction of traffic, so traffic is moving top-down. No point rewarded if the tail of the queue of the accident is indicated.

248 Given one specific traffic jam and its slope (choose one, 1 point), we find the length of the shown road is around the distance travelled in 2/3 of an hour. Since stop-and-go waves travel with approximately 18 km/h, this equals or 12 km (1).

249 The capacity drop would be visible at location "1", downstream of the fixed bottleneck (0.5). There, the flow would be higher after congestion has set in than before (1). In the current graph, this is not visible. (0.5)

250 Rabbits take the lane where the speed is the highest.

251 The density is equal (from question, 0.5), and the flow is proportional to density times speed (0.5), i.e. a normalized flow of 80 of slugs and 100 of rabbits (0.5). That means $100/180 = 5/9$ of the flow is rabbits (0.5).

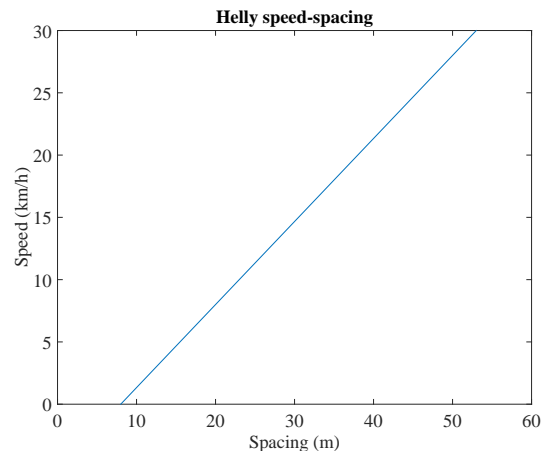
252 Weighted average speed proportional to the flows (1): $5/9 \cdot 100 + 4/9 \cdot 80 = 91$ km/h.
Computing space mean speed, or assuming flows are equal gives no points.

253 Edie's generalised definitions suggest that the speed is the total distance covered divided by the total time spent. TTD is the sum of all distance covered by all vehicles within a predefined area in space-time; TTS is the sum of all time spent of all vehicles within a predefined area in space-time.
Only the equations do not give any points.

254 The model prescribes an acceleration based on a speed difference (first term, sensitivity α) (1) and a difference between the spacing ($x_{i-1}(t - \tau) - x_i(t - \tau)$) and a desired spacing ($s_0 + T v_i(t - \tau)$) (second term, sensitivity β).
(1) The desired spacing is linearly increasing with the speed of the vehicle.

255 FD is homogeneous and stationary conditions (0.5), meaning $v_i = v_{i-1} = u$ (homogeneous, 0.5), and $a=0$ (stationary: 0.5). Hence, $x_{i-1}(t - \tau) - x_i(t - \tau) = s_0 - T u$ (0.5 - 2 points up to now). Spacing can be obtained by $s(t - \tau) = x_{i-1}(t - \tau) - x_i(t - \tau)$ (0.5) and stationarity $s(t) = s(t - \tau) = s$ (0.5). Then, $a = 0 = 0 + \beta (s - s_0 - T u)$, or $u = (s - s_0)/T$. (1) Plotting gives a linear increase of u as function of spacing

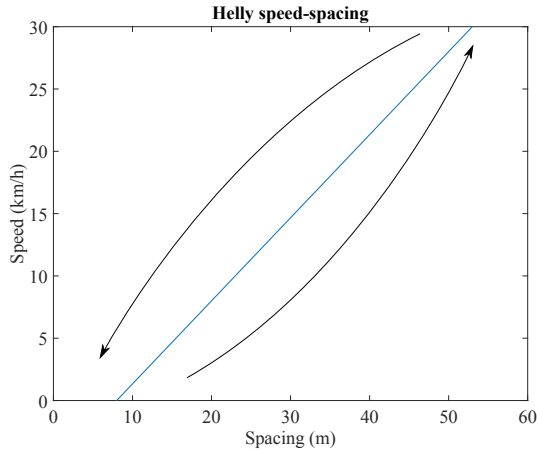
Explicitly making the assumptions is essential. A non-motivated sketch in vt gives no points; starting from $u =$



$(s - s_0)/T$ and plotting that will provide 1 point in total.

256 The delay τ causes a delayed reaction. If the leader accelerates (going right in the spacing), the follower goes later up in speed (1); similar reasoning for decelerating (0.5), so we obtain a anti-clockwise hysteresis loop (0.5).

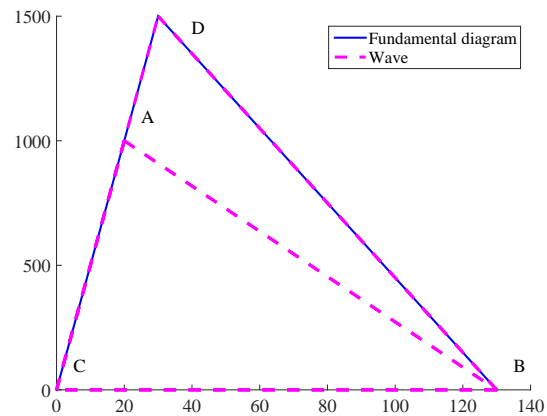
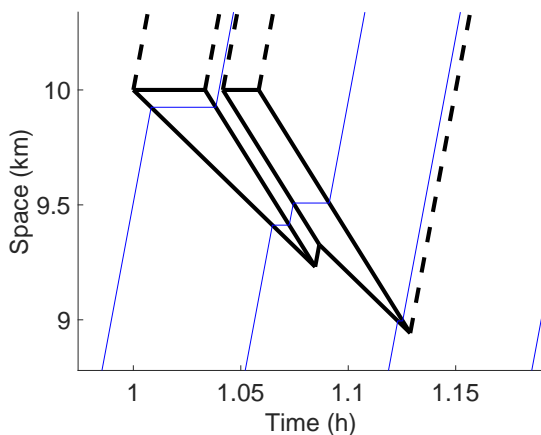
Plotting arrows based on an assumption delayed/anticipation, or providing both will give 1 point.



257 Starting from $s = s_0 + Tu$, we apply $s = 1/k$ (0.5) and $u = q/k$ (0.5). We obtain $1/k = s_0 + Tq/k$, rewritten to $1 = ks_0 + Tq$, or $q = (1 - ks_0)/T$ (1).

259 The critical density is $1500/50=30\text{veh/km}$ (0.5); The jam density is $1500/15=100\text{ veh/km}$ higher than the critical density (1), hence the jam density is $30+100=130\text{ veh/km}$ (0.5)

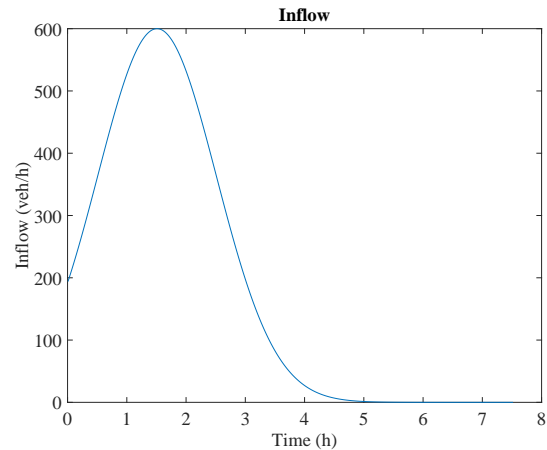
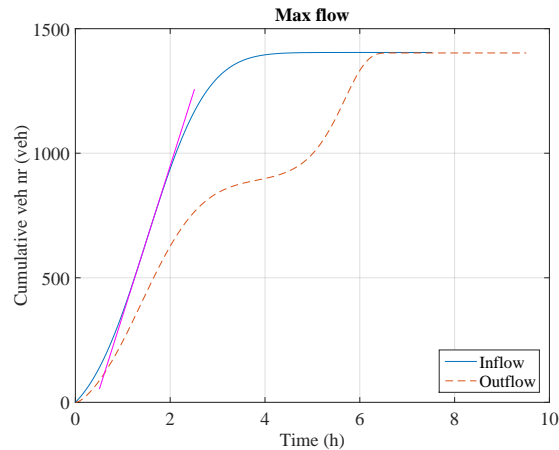
260 Indicate the inflow state in FD (A, 0.5). Then, the first light causes an empty congested state downstream (state C, 0.5) and a state at jam density upstream (B, 0.5). This creates three waves: AB, AC, BC (0.5 each; 1.5 total). When the traffic light turns green, a capacity state D (0.5) emerges, with shock waves CD and BD (0.5 point each – total so far: 4.5). The next red phase causes again states B (0.5) and C (0.5). However, this now gives waves BD (0.5) and CD (0.5). When waves AB and AD of the first traffic light join, wave AD emerges, up to the moment that this intersects with BD (0.5). Then, a wave AB continues (1). Finishing goes in the same way as finishing the first red phase: state D, waves CD, BD (0.5). When wave DB intersects with AD, the wave AD occurs and moves forward (0.5).



For this answer, the graphs have been constructed automatically. In your answer, provide the reasoning as above. Moreover, place letters in within the space-time diagram. The dotted shock waves should be drawn just as the others. Trajectories are not needed (not part of the question)

261 The flow is the slope of the cumulative inflow, which first increases (0.5) and then decreases, see graph above (0.5). The maximum flow is the highest slope, estimated at 600 veh/h (0.5).

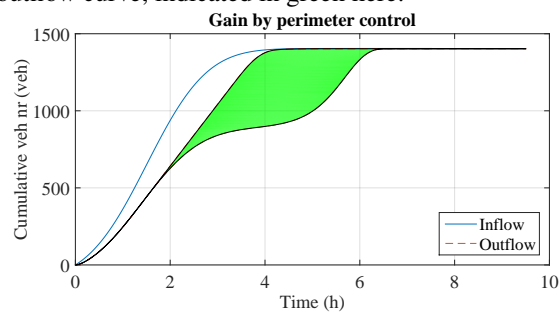
Half a point reduction if the line does not increase at the beginning.



262 The outflow curve increases when traffic starts to accumulate (1). The slope of the line is the outflow, given by the accumulation. If the accumulation increases to values over capacity, the outflow decreases, yielding a flatter outflow curve (1). Only when the inflow reduces to values under the low outflow, the accumulation decreases and the outflow increases again (1).

263 By limiting the inflow and not exceeding the critical accumulation, an outflow of 600 veh can be maintained (1); the remaining queuing is outside the network (1).

264 Whenever there are too many vehicles in the network, we assume they can be queued outside the network (perimeter control), and the outflow will be 400 veh/h, i.e. the capacity outflow from the MFD (0.5). The cumulative outflow under perimeter control hence keeps increasing with 400 veh/h whenever there is an excess number of vehicles between cumulative inflow and outflow(0.5). The amount of travel time gained is the area between the old and new outflow curve, indicated in green here.



265 No, he can be moving in the y-direction

266 The SFM describes for individual pedestrians (hence, microscopic, 1) how they move. A "force" changes their direction: they are attracted by their destination (1), and repelled by obstacles (0.5) and other pedestrians (0.5).

Appendix C

Matlab code for creating (slanted) cumulative curves

```
1 function cumcurves()
2 %This function will give the cumulative curves for a flow which
3 %has (in time) three values, and one bottleneck halfway
4 q0=[3600;5000;2000];%the three demands
5 Tchange=[60;90];%times in minutes at which the demands change
6 c=4000;%capacity
7 T=0:200;%minutes
8 dt=1/60;%time steps (in hours: time step is 1 min)
9 dem=q0(end)*ones(size(T));%pre-allocate demand function to the last demand value
10 for (i=numel(Tchange):-1:1)
11     dem(T<Tchange(i))=q0(i);%adapt the demand function
12 end
13
14 figure;
15 plot(dem,'linewidth',2)
16 hold on
17 plot(repmat(c,size(dem)),'r--','linewidth',3)
18 ylim([0 6000])
19 legend('Demand','Capacity','location','Northeast')
20 ylabel('Flow (veh/h)')
21 xlabel('Time (min)')
22 exportfig('Demand')
23 %%
24
25 Nin=dt*cumsum(dem);
26 qout=zeros(size(Nin));
27 qout(1)=dem(1);%in veh/h
28 queued=zeros(size(dem));
29 for (t=2:numel(T))
30     qout(t)=1/dt*min(dt*c, dt*dem(t)+queued(t-1));
31     queued(t)=queued(t-1)+dt*dem(t)-dt*qout(t);
32 end
33 Nout=dt*cumsum(qout);
34 figure;plot(Nin,'linewidth',2,'color',[0.5 0.5 1]);hold on;plot(Nout,'r--','linewidth',3)
35 legend('N_{in}','N_{out}','location','Northwest')
36 ylabel('Cumulative flow')
37 xlabel('Time (min)')
38 exportfig('Cumulative curves')
39 %%
40
41 %compute total delay:
42 TotalD=dt*sum(queued)%then the total delay in hours
```

```

43 NrVeh=Nin(end);
44 AvgDelay=TotalD/NrVeh;%then the total delay in hours
45 AvgDelayMin=60*AvgDelay;%then the total delay in hours
46
47 %%
48 Tin=interp1(Nin,T,1:NrVeh);%time to enter for each vehicle -- interpolation
49 Tout=interp1(Nout,T,1:NrVeh);%time to exit for each vehicle -- interpolation
50 DT=Tout-Tin;%additional travel time
51 figure;
52 plot(1:NrVeh,DT,'linewidth',2)
53 xlabel('Vehicle number')
54 ylabel('Delay (min)')
55 exportfig('Delay per vehicle')
56
57 figure;
58 plot(Tin,DT,'linewidth',2)
59 xlabel('Entry time (min)')
60 ylabel('Delay (min)')
61 exportfig('Delay as function of time')

```